

PRODUCTION DATA SHEET

DESCRIPTION

plug or the battery.

The controller also includes status indicators which show when the controller is powered by an in progress, and charge completed.

The USB input is current limited at

The LX2205 is a complete single two logically selectable levels (100mA cell Lithium Ion or Lithium Polymer and 500mA). When powered by a USB battery charger and power source input, the battery is charged with the manager. In addition to battery excess USB current that is not charging, power flow control is consumed by the system load. If the provided from up to three sources: a load exceeds the USB current limit, the wall adapter, a standard USB power battery will discharge to assist the USB power source to power the load. The The battery charge current and controller can logically suspend the termination current are independently USB power to allow the system to operate from the battery without loading the USB.

When a wall adapter is applied, it external adapter in addition to charge takes precedent over the USB power input and disables the USB input to prevent current flow from the adapter to the USB port.

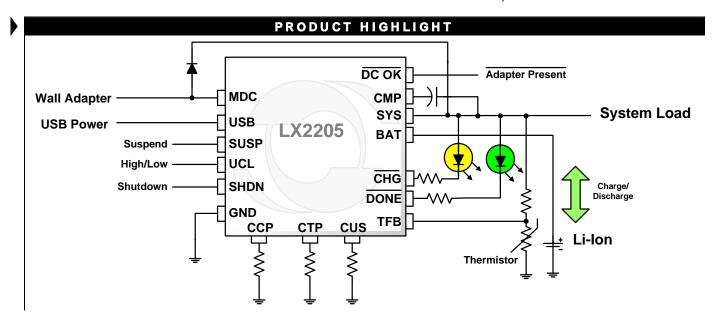
IMPORTANT: For the most current data, consult MICROSEMI's website: http://www.microsemi.com Patents Pending.

KEY FEATURES

- Single Cell Li-Ion Battery Charger
- **Power Source Management**
- Up to 1A Charging Current
- Integrated Power MOSFET
- **USB Current Compliance**
- 25µA Quiescent Current in Discharge Mode
- **Taper Current Termination**
- **Protection features:**
- **USB Reverse Current Blocking**
- Unsafe Battery Temp Lockout
- Internal IC Temperature Limiter
- **USB Current Limiter**

APPLICATIONS

- **Navigation Devices**
- Portable USB Devices
- Multi-Media Player
- **PDA Phones**
- **Digital Cameras**





Note: Available in Tape & Reel. Append the letters "TR" to the part number. (i.e. LX2205ILQ-TR)



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ABSOLUTE MAXIMUM RATINGS

Supply Voltages (MDC, SYS, USB) Battery Voltage (BAT) All Other Pins USB Current BAT Discharge Current Operating Ambient Temperature Range (T _A) Maximum Operating Junction Temperature (T _J) Storage Temperature Range	0.3V to 6V -0.3V to V _{SUPPLY}
	65°C to 150°C 300°C

Note: Exceeding these ratings could cause damage to the device. All voltages are with respect to ground. Currents are positive into, negative out of specified terminal.

THERMAL DATA

LQ Plastic 4 x 4mm 16-Pin

THERMAL RESISTANCE-JUNCTION TO AMBIENT, θ_{JA}

28°C/W*

Junction Temperature Calculation: $T_J = T_A + (P_D \times \theta_{JA})$.

*The θ_{JA} numbers are guidelines for the thermal performance of the device/pc-board system. All of the above assume no ambient airflow. See layout guidelines section for important details.

PACKAGE PIN OUT DONE 땡 CMP CTP **BAT** CCP SYS GND Connect Bottom **USB** Pad to GND CUS SUSP SHDN LQ PACKAGE

RoHS / Pb-free 100% Matte Tin Pin Finish

	FUNCTIONAL PIN DESCRIPTION					
Name	Name Pin Description					
BAT	BAT 2 Battery Connection - This pin is wired to the positive terminal of a single cell lithium ion/polymer battery.					
CCP Charge Current Programming Pin - A resistor (R _{CCP}) is connected between this pin and GND. The constant charging current is determined by the following relationship: $R_{CCP} = 50.648 \text{ x I}_{CCL}^{-1.0855}$ with R_{CCP} in kΩ and R_{CCP} in amps.						
CHG	THE CHG 14 Charge Indicator - This pin is a logic low level when the battery is being charged, provided V _{SYS} is ≥ 4.4V. It is capable of driving the series combination of an LED and resistor that is powered from the SYS pin.					
CMP	1	Compensation – Connect a 0.1µF capacitor from CMP to SYS.				
СТР	Charge Termination Programming Pin – A resistor (R _{CTP}) is connected between this pin and GND. The charge termination taper current is determined by the following relationship: R _{CTP} =0.7354 x I _{TERM} ^{-1.0876} with R _{CTP} in kΩ and I _{TERM} in amps.					
CUS	9	USB Current Limit Programming Pin – A resistor (R _{CUS}) is connected between this pin and GND. The high level USB charge current is determined by the following relationship: I _{USB} = 1050 / R _{CUS} .				
DCOK	13	Main DC Present – A low level on this logic output indicates that the Main DC power source (typically the wall adapter) is applied.				
DONE	15	Done Indicator - This pin is a logic low level when the battery charge cycle is complete. It is capable of driving the series combination of an LED and resistor that is powered from the SYS pin.				
GND	10	Common Ground – Used as chip ground and as a reference for the battery return.				

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	FUNCTIONAL PIN DESCRIPTION (CONTINUED)						
Name	Name Pin Description						
MDC	5	Main DC Input – This input is a voltage monitoring input (and not a high current input). Its purpose is to determine the presence of the main DC input to provide lockout for the USB power input.					
SHDN	6	Shutdown – Pulling this pin high will disable the entire device including the battery discharge path and place the device in a low power sleep mode. This pin has an internal pull-down.					
SUSP	7	Suspend (USB) – Pulling this pin high will prevent current from being drawn from the USB input pin. The rest of the chip functions are unaffected. This pin has an internal pull-down.					
SYS	3	System Power Node – This pin provides power to user system. SYS voltage provided will range from the battery voltage to the wall adapter and/or USB voltage.					
TFB	16	Temperature Feedback – Charging is suspended when the TFB pin falls below 29% (typ) of V _{SYS} or rises above 74% (typ) of V _{SYS} . CHG and DONE pins remain in their prior state during a TFB event. Connecting the TFB pin to GND disables the TFB function.					
USB	4	USB Power Input – USB compliant input.					
UCL	8	USB Current Limit – A high logic level will select the high USB current level determined by the programming of the CUS pin. A low logic level will select a level that is 20% of the high USB current level. This pin has an internal pull-down.					



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ELECTRICAL CHARACTERISTICS

Unless otherwise specified, the following specifications apply over the operating temperature -40°C \leq T_A \leq 85 °C and the following test conditions: V_{MDC} = V_{USB} = 5V, V_{SYS} =Open, V_{SUSP} = V_{SHDN} = Low, V_{UCL} = High, V_{BAT} = 3.9V, R_{CCP} = 49.9k, R_{CUS} = 2.26k, R_{CTP} = 20k

Parameter	Symbol Test Conditions		LX2205			Units		
Farameter	Symbol	rest Conditions	Min	Тур	Max	Unit		
MAIN CIRCUITRY								
Input Voltage	V _{SUPPLY}	USB or SYS	4.35		6			
Under Voltage Charging Lockout	V _{SYS} (_{UVLO)}	Rising input; V _{BAT} = 3.2V	3.55	3.7	3.95	V		
SYS UVLO Hysteresis		Guaranteed by design		140		mV		
USB UVLO	V _{USB} (_{UVLO)}	Rising input; V _{BAT} = 3.2V	4.25	4.30	4.34	V		
CVC Input Cumply Current		$V_{BAT} = V_{CVL}$; (battery charged), $V_{SYS} = 5.0V$		1.5	2.5	mA		
SYS Input Supply Current	I _{SYS}	SHDN = High (Shutdown Mode), V _{SYS} = 5.0V		25		μA		
		$V_{BAT} = V_{CVL}$; (battery charged), , $V_{MDC} = 0V$		2		mA		
LICD Input Cumply Current		SUSP = High (Suspend Mode), , V _{MDC} = 0V			25	μΑ		
USB Input Supply Current	I _{USB}	SHDN = High (Shutdown Mode), , V _{MDC} = 0V			25	μA		
		V _{MDC} = 0V, V _{USB} = 0V		-1.5	-6	μA		
Battery Drain Current	I _{BAT}	V _{BAT} = V _{CVL} ; (battery charged)		0.5	10	μA		
		V _{MDC} =0V; SUSP = High (Suspend Mode)		25	50	μA		
		SHDN = High (Shutdown Mode)		0.5	10	μA		
		V _{USB} = 0V; V _{MDC} = 0V; Discharge with no load		25	50	μΑ		
BATTERY CHARGER								
Constant Voltage Charge Voltage	V _{CVL}		4.16	4.2	4.24	V		
CTP Bias Voltage	V _{CTP}	I _{BAT} > 100mA		1.30		V		
CCP Bias Voltage	V _{CCP}			1.25		V		
	I _{CCL}	V _{SYS} = 5.0V	0.85	0.98	1.10	Α		
May Pattory Charge Current	I _{BAT}	V _{MDC} =0V		465		mA		
Max Battery Charge Current		V _{MDC} =0V; I _{SYS} = 200mA (out of pin)		261		mA		
		V _{MDC} =0V; UCL = Low		92		mA		
Conditioning Current	I _{COND}	V _{BAT} =2.5V, as a % of I _{CCL}	2.5	5	7.5	%		
Conditioning Current Threshold Voltage	V _{CCT}		2.55	2.7	2.9	V		
Charge Termination Current	I _{BAT}		40	50	60	mA		
Top Off Charge Droop Threshold	V_{DRP}	Expressed as a % of V _{CVL}	96	97	98	%		



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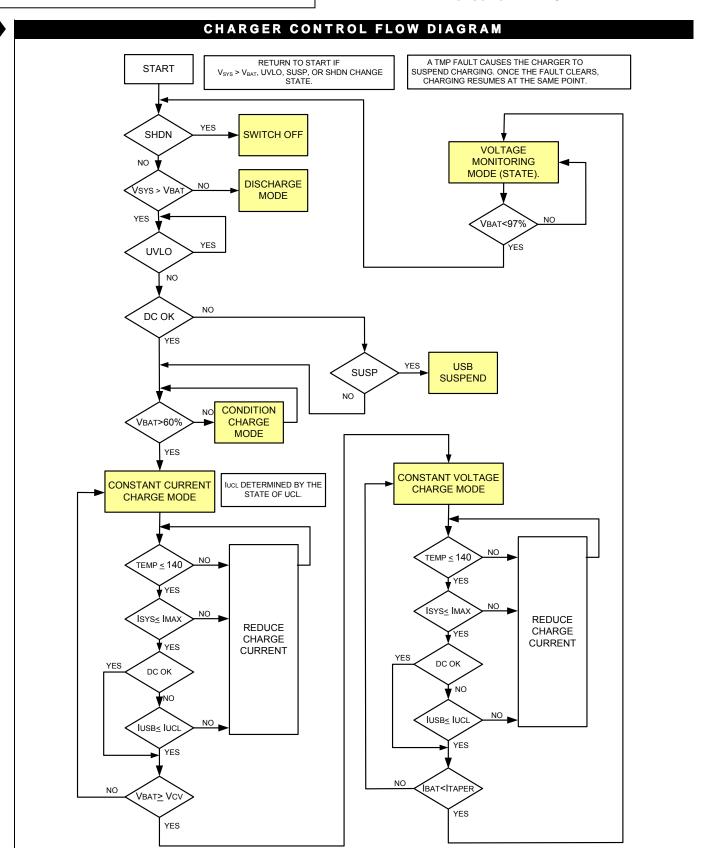
ELECTRICAL CHARACTERISTICS (CONTINUED)

Unless otherwise specified, the following specifications apply over the operating temperature -40°C \leq T_A \leq 85 °C and the following test conditions: $V_{MDC} = V_{USB} = 5V$, $V_{SYS} = 0$ pen, $V_{SUSP} = V_{SHDN} = 1$ Low, $V_{UCL} = 1$ High, $V_{BAT} = 3.9V$, $V_{CCP} = 49.9k$, $V_{CUS} = 2.26k$, $V_{CCP} = 2.20k$

Parameter	Symbol	Test Conditions	LX2205			Units			
Parameter	Symbol	rest Conditions	Min	Тур	Мах	Units			
USB CURRENT LIMIT									
USB Low Current Limit	I _{USB}	V _{MDC} = 0V, UCL = Low	85	93	100	mA			
USB High Current Limit	I _{USB}	V _{MDC} = 0V	425	463	500	mA			
Reverse Leakage Current	I _{LEAK}	V _{USB} = 0V		2	10	μΑ			
CUS Bias Voltage	V _{cus}			2.5		V			
LOGIC									
CHG, DONE Logic High Output	V_{OH}	V _{SYS} = 5.0V, I _{OH} = -25uA	4.0	4.5		V			
CHG, DONE Logic Low Output	V_{OL}	$V_{SYS} = 5.0V, I_{OL} = 5mA$			0.4	V			
Input Logic : UCL, SUSP, SHDN	$V_{LOG(IN)}$	Logic Hi,	1.2			V			
input Logic . OCL, 303F, 3HDN	V LOG(IN)	Logic Lo			0.4	V			
Input Logic Current : UCL, SUSP,		Logic Hi, V _{LOG} = 2V	0	2	4				
SHDN	I _{LOG(IN)}	Logic Lo, V _{LOG} = 0V	-2	0	2	μA			
Outset Levie v BOOK	1	Logic Hi, 10K to 3.3V	3.2						
Output Logic: DC OK	$V_{LOG(OUT)}$	Logic Lo, I _{LOG} = 100μA			0.4	V			
THERMAL DIE PROTECTION	•		•		•				
Battery Charger Thermal Limiter	T _{CTL}			140		°C			
BI-DIRECTIONAL PASS ELEMENT	CONTROL								
Discharge Switch On Resistance	R _{DS(ON)}	I _{BAT} = -1A		275		mΩ			
Charging Threshold	V_{CHG}	V _{SYS} – V _{BAT}		40		mV			
Discharging Threshold	V _{DCH}	V _{BAT} – V _{SYS}		40		mV			
Pass Element Switch Mode Delay	t _{sw}	Charge-To-Discharge or Discharge-To-Charge		2.5		μs			
Charging headroom		V _{SYS} – V _{BAT} , I _{BAT} = 5mA		80		mV			
Discharging headroom		V _{BAT} – V _{SYS} , I _{BAT} = -20mA		80		mV			
MDC INPUT	•		•						
DC OK Voltage Threshold	V_{MDC}	Rising	4.0	4.15	4.3	V			
Hysteresis	V _{MDC(HYS)}			35		mV			
MDC Input current	I _{MDC}			15	35	μA			
BATTERY TEMPERATURE MONIT	OR	'	•						
		Rising Threshold ; as % of V _{SYS}	73	75	77	%			
Cold Temp Fault Threshold	$V_{TFB(COLD)}$	Falling Threshold; as % of V _{SYS}	71	73	75	%			
		Falling Threshold; as % of V _{SYS}	27	28.5	30	%			
Hot Temp Fault Threshold	$V_{TFB(HOT)}$	Rising Threshold; as % of V _{SYS}	28	29.5	31	%			
TFB Disable Voltage Threshold	V _{TFB(DIS)}		70	100	150	mV			



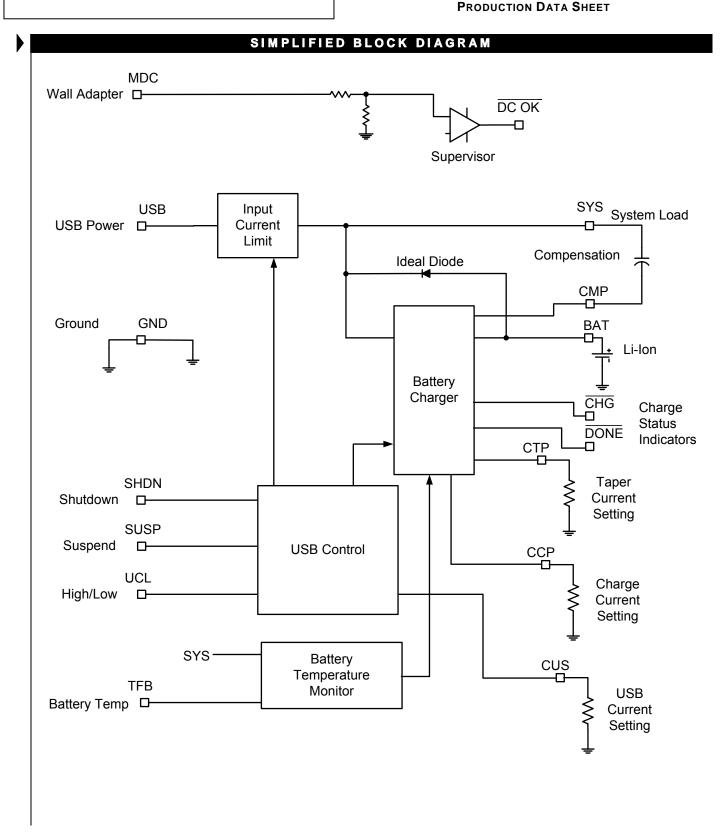
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APPLICATION CIRCUITS

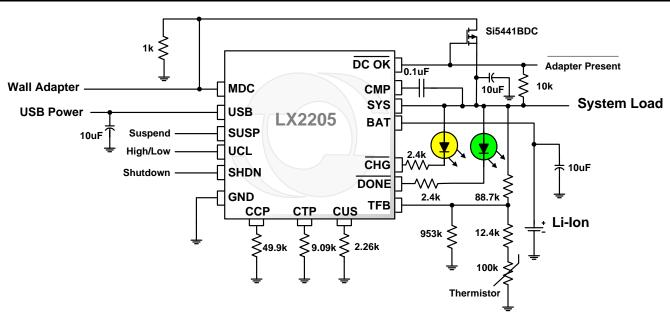


Figure 3 – AC Adapter and USB Supply (Charge and Discharge Modes) with 1A charging and 100mA termination current. In this application, the wall adapter voltage is not well regulated and can dip to less than 4.7V. For this case, a reverse blocking MOSFET is used instead of the reverse blocking diode, shown in the Product Highlight. This extends the operating range of the LX2205 because the drop across the MOSFET is minimal. It also increases efficiency by eliminating the power loss of the schottky diode.

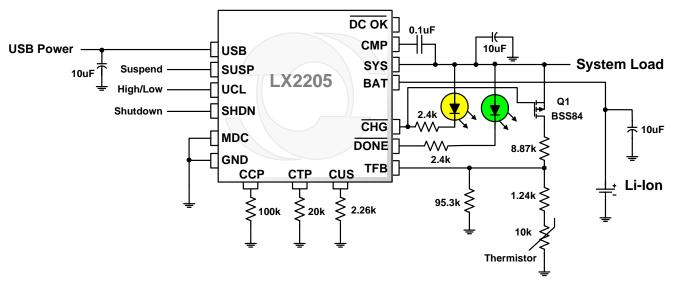


Figure 4 – This application uses only a USB input with 500mA and 100mA maximum current limit levels and a 50mA termination current level. MOSFET Q1 turns off the TFB resistor string when not in charge mode to prevent battery drain; this is particularly helpful when using a small thermistor resistance value in the battery pack.



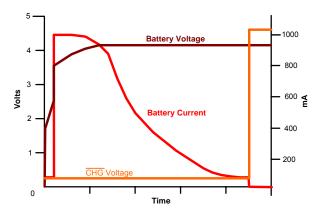
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THEORY OF OPERATION

BATTERY CHARGER GENERAL DESCRIPTION

The LX2205 is designed to charge a single cell Lithium Ion or Lithium Polymer battery using two steps: a constant current step followed by a constant voltage step. The basic charger function uses the SYS pin as an input and BAT pin as the output. The LX2205 charger has a programmable maximum current (programmable by the resistor value between the CCP pin and GND) which is the maximum charging current during the Constant Current Mode of the charging profile. The charger will terminate constant voltage charging once the current drops below the taper current setting (programmable by the resistor value between CTP pin and GND).

Two step charger profile:



CONDITIONING CURRENT CHARGE MODE

A conditioning current is applied to a battery that is deeply discharged and has a terminal voltage less than 60% of the constant voltage level. The conditioning current is 5% of the CCP programmable constant current level. Once the battery terminal voltage exceeds the 60% level, the full constant current level is applied (unless charging current is limited by one of the other charger control loops).

CHARGE TERMINATION MODE

To increase system battery life and avoid float charging, the LX2205 disconnects the charger once the battery has been fully charged. The charge termination state occurs at the end of constant voltage mode. The charge status indicators change state when charging is completed.

STATES	CHG	DONE
Charge in process	ON	OFF
Charge completed	OFF	ON
Input power removed	OFF	OFF

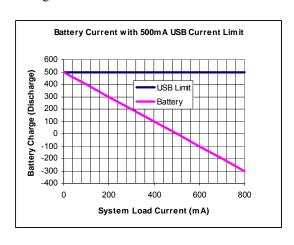
Using the taper current to terminate the charge cycle is particularly advantageous in an isolated battery topology such as the LX2205, because when an external power source is applied to the appliance with the appliance turned on, the power to the appliance and the power to the battery take separate paths. This separate path allows the battery charge current to be monitored accurately. Compared with charger controllers that rely on a fixed timeout period terminating by taper current allow for the shortest possible battery charge time.

TOP OFF CHARGE MODE

Once the charger has completed a charge cycle, if power remains applied, the LX2205 enters a voltage monitoring mode. In this mode the LX2205 monitors the battery terminal voltage and applies a top off charge if the battery voltage drops by more than 3% of $V_{\rm CVL}$. This feature is especially important for charging systems in equipment where usage is infrequent.

USB CHARGE MODE AND CURRENT LIMIT

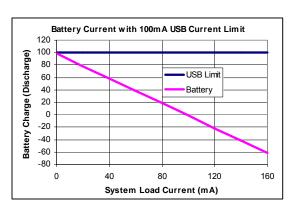
The LX2205 is fully compliant with, and supports, the USB specifications – the Low Power Peripheral (100mA) and High Power Peripheral (500mA). The UCL logic input selects the USB charge current level. The LX2205 senses the current flowing from the USB terminal to the SYS terminal. The LX2205 will first try to reduce the combined USB load by scaling back the battery charging current. Once the charger has scaled back the charge current to zero, if the load demands more current than the USB bus can supply the $V_{\rm SYS}$ voltage will drop down to the battery voltage level and the battery will supply the additional current demand. This is illustrated in the following two charts.





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THEORY OF OPERATION



REDUCED USB CHARGE TIME

The isolated battery topology reduces charge time from the USB port when the appliance is turned on while also charging. Because the system power rail can be a higher voltage than the battery voltage, the system will require less power from the USB source which leaves more power available to charge the battery quickly. For example, if the system draws 1W, and the USB input is 5V, the system draws 1W/5V = 200mA from the USB source; this leaves 300mA to charge the battery. In a topology where the load connects directly to the battery (as is done with conventional non-isolated linear chargers), if the average battery voltage is 3.7V, the system will draw 1W/3.7V = 270mA from the USB source, this leaves only 230mA to charge the battery. In this case the LX2205 will charge the battery 30% faster.

USB SUSPEND

When the SUSP pin is pulled high, less than $25\mu A$ is pulled from the USB port. The rest of the LX2205, however, continues to function normally. If an adapter is applied, the effect of SUSP is negligible. If the system is running off both USB and the battery and SUSP is logic high, the system load will be transferred 100% to the battery.

SHDN

When SHDN is logic high, the LX2205 is placed in a total shutdown mode; no current will flow between SYS, USB and BAT. Quiescent current is $25\mu A$ during shutdown. \overline{CHG} and \overline{DONE} are high impedance (off) in SHDN mode.

UCL

The UCL pin is used to select the current limit level for the USB input. When the UCL pin is a logic high the maximum current level as determined by the CUS resistor is selected; when the UCL pin is a logic low, the current limit is set to 20% of the maximum level.

POWER OR-ING (SYS TO BAT AND BAT TO SYS)

When the power is removed from both MDC and USB, the battery current flows from BAT to SYS and thus provides power to the load without the need for any external switches or monitoring circuits. There is a circuit equivalent of an ideal diode (patent-pending bi-directional MOSFET) in the LX2205 between the BAT pin and SYS pin. This ideal diode appears as a low impedance to high forward current and presents a high impedance to low discharge currents or potentially reverse charge currents. For small forward currents, the ideal diode regulates a small forward voltage. This small voltage allows the power sense circuitry to determine whether an input power source is present even if the current through the ideal diode is less than 1mA. This feature makes it virtually impossible to charge the battery (unregulated) in reverse through the ideal diode and also enables the battery to assist a current limited input power source without chattering even if only a few mA of battery current are required.



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THEORY OF OPERATION / APPLICATION NOTE

MDC, USB OR-ING, UVLO AND DC OK

The power path from the USB input to the SYS pin consists of a current limiter and a bidirectional switch (capable of blocking current in either direction). The USB input is switched off when at least one of the following conditions exists:

- 1. VUSB < VUSBUVLO
- 2. USB Suspend pin is asserted.
- 3. $V_{MDC} > V_{USB}$
- 4. $VMDC > V\overline{DCOK}$ _THRESHOLD

The MDC input is a monitoring input only, it is not a high current input. When the voltage at SYS exceeds the UVLO level, (typically 3.7V), the charger portion of the circuit is activated. The DCOK output is pulled low when both of the following conditions are true:

- 1. $VMDC > V\overline{DCOK}$ THRESHOLD
- 2. VSYS > VBAT

Therefore when using a current limited wall adapter it is possible to charge the battery and not assert the \overline{DCOK} output.

PROTECTION FEATURES

<u>Conditioning Current Mode</u> – If the battery terminal voltage is less than 2.7V, the battery charger will reduce the charge current to 5% of full scale. This also protects the appliance from overheating by trying to drive the full charging current into a short circuited battery.

<u>Under Voltage Lockout</u> – The charger remains inactive until the under voltage lockout threshold is exceeded at the SYS pin.

<u>Thermal Control Loop</u> – The power dissipation of the charger is limited by reducing the charge current with a control loop to prevent the die temperature from exceeded approximately 140°C.

<u>Reverse Current Blocking</u> – Current will not flow out of the USB pin.

<u>Shutdown Mode</u> – If the SHDN pin is logic high, the charger enters a shutdown mode to prevent draining the battery.

<u>Battery Temperature Lockout</u> – If an unsafe temperature is sensed by the TFB input window comparator, battery charging is suspended.

LAYOUT GUIDELINES

- It is important when laying out the LX2205 to place 10μF ceramic capacitors as close to the SYS, USB and VBAT IC terminals as possible to filter switching transients.
- It is important to provide a low thermal impedance path from the thermal pad on the bottom of the LX2205 package to the ground plane of the circuit board to maximize heat dissipation. Generally this is accomplished by the use of multiple thermal vias.
- The compensation capacitor should be placed close to the CMP pin and connected with a short trace.

CHARGE CURRENT PROGRAMMING

The CCP, CTP, and CUS programming pins are used to program the constant charge current, termination current, and USB current, respectively. These pins utilize regulated output voltages that produce a program current across an external resistor to GND.

The following tables are guidelines for selecting the proper resistor values:

Constant Charge Current (in mA)	R_{CCP}
50	1270k
100	604k
200	294k
300	187k
400	137k
500	107k
600	88.7k
700	75.0k
800	63.4k
900	56.2k
1000	49.9k*
* R _{CCP} mir	nimum value

тестр пп	minum varac
Termination Current (in mA)	R _{CTP}
5	237k
10	105k
20	51.1k
40	24.9k
60	15.8k
80	11.8k
100	9.09k
120	7.50k
140	6.34k
160	5.49k
180	4.75k
200	4.22k

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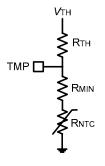
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APPLICATION NOTE

BATTERY TEMPERATURE MONITOR

The LX2205 has an input to monitor the battery temperature during battery charging. The SYS voltage must be used to bias this circuitry. During the occurrence of a TMP fault, the charge cycle is suspended; however the status indicators state remains unchanged.

A typical Lithium Ion battery should only be charged within a temperature range of 0°C to 60°C. For this calculation example, a Vishay NTHS0402N01N1003J thermistor was used. This thermistor has the value of $327k\Omega$ at 0°C, $100k\Omega$ at 25°C and $24.9k\Omega$ at 60°C. The thermistor must be biased with a Thevenin voltage source and series resistance to achieve the proper TMP thresholds. A fixed value resistor is added in series with the thermistor to prevent it from becoming too low impedance at high temperatures and causing the TMP input to default to off.



Using a value of R_{MIN} that is $\frac{1}{2}$ the thermistor high temperature trip resistance value works well; therefore, for this example, set the value of R_{MIN} to:

$$12.4k = R_{MIN} = \frac{R_{T=60^{\circ}C}}{2} .$$

This has the effect of adding a fixed 12.4k to the thermistor resistance values so it becomes $339k\Omega$ at 0° C, $112k\Omega$ at 25° C and $37.3k\Omega$ at 60° C.

The equations for R_{TH} and V_{TH} are, using Cold Temperature Fault Threshold average of 74% and the Hot Temperature Fault Threshold average of 29% of V_{SYS} :

$$\begin{split} & \frac{V_{TH}}{V_{SYS}} = \frac{0.29 \times 0.74 \times \left(R_{T=0^{\circ}C} - R_{T=60^{\circ}C}\right)}{\left(0.29 \times R_{T=0^{\circ}C}\right) - \left(0.74 \times R_{T=60^{\circ}C}\right)} \\ & = K = 0.916 \end{split}$$

$$R_{TH} = \left(\frac{K}{0.74} - 1\right) \times R_{T=0^{\circ}C} = 80.6k$$

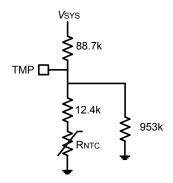
To finish the design it is necessary to create the Thevenin Voltage and resistance using a voltage divider from the SYS pin.

The values of R1 and R2 can be calculated as:

$$R_1 = \frac{R_{TH}}{K} = 88k$$

$$R_2 = \frac{R_1 \times R_{TH}}{R_1 - R_{TH}} = 958k$$

Actual standard 1% resistor values are: 953k and 88.7k. The final circuit for this example is:



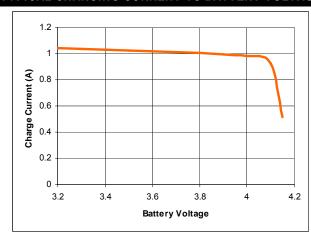
The TMP voltages with this circuit are:

	TEMP (°C)	RNTC	VTMP (% VSYS)
-	-20	971k	85%
	0	327k	74%
ĺ	25	100k	53%
	60	24.9k	29%
	80	12.6k	22%

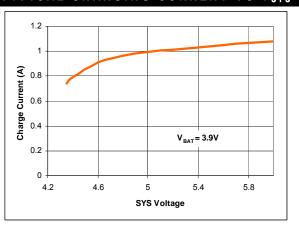


1A Li-lon Battery Charger with Power Source Management **PRODUCTION DATA SHEET**

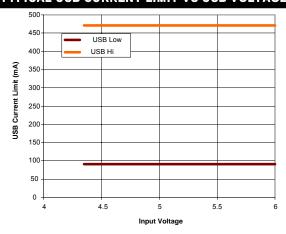
TYPICAL CHARGING CURRENT VS BATTERY VOLTAGE



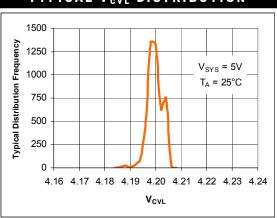
TYPICAL CHARGING CURRENT VS V_{sys}



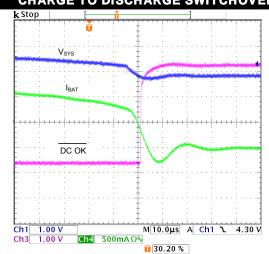
TYPICAL USB CURRENT LIMIT VS USB VOLTAGE



TYPICAL VCVL DISTRIBUTION



CHARGE TO DISCHARGE SWITCHOVER



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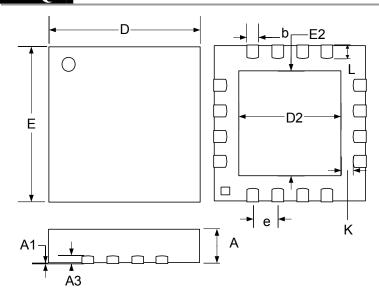
Microsemi



PRODUCTION DATA SHEET

PACKAGE DIMENSIONS

16-Pin MLPQ Plastic (4x4mm EP / 114x114Cu Exposed Pad)



	MILLIMETERS		MILLIMETERS INCH		HES
Dim	MIN	MAX	MIN	MAX	
Α	0.80	1.00	0.031	0.039	
A1	0	0.05	0	0.002	
A3	0.18	0.30	0.007	0.012	
b	0.23	0.38	0.009	0.015	
D	4.00 BSC 0.157 E			BSC	
E	4.00	BSC	0.157	BSC	
е	0.65 BSC		0.026 BSC		
D2	2.55	2.80	0.100	0.110	
E2	2.55	2.80	0.100	0.110	
K	0.20	-	0.008	-	
L	0.30	0.50	0.012	0.020	

Note:

 Dimensions do not include mold flash or protrusions; these shall not exceed 0.155mm(.006") on any side. Lead dimension shall not include solder coverage.

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