## Isolated Switching Regulator With Integrated Feedback

## Data Sheet

## FEATURES

## Isolated PWM feedback with built in compensation

 Primary side transformer driver for up to $\mathbf{2 . 5} \mathbf{W}$ output power with 5 V input voltageRegulated adjustable output: 3.3 V to 24 V
Up to 80\% efficiency
200 kHz to 1 MHz adjustable oscillator
Soft start function at power-up
Pulse-by-pulse overcurrent protection
Thermal shutdown
2500 V rms isolation
High common-mode transient immunity: > $\mathbf{2 5} \mathbf{~ k V / \mu s}$
16-lead QSOP package
High temperature operation: $105^{\circ} \mathrm{C}$

## APPLICATIONS

## Power supply startup bias and gate drives

Isolated sensor interfaces
Process controls

## GENERAL DESCRIPTION

The ADuM3070 ${ }^{1}$ isolator is a regulated dc-to-dc isolated power supply controller with an internal MOSFET driver. The dc-todc controller has an internal isolated PWM feedback from the secondary side based on the $i$ Coupler ${ }^{\circ}$ chip scale transformer technology and complete loop compensation. This eliminates the need to use an optocoupler for feedback and compensates the loop for stability.

FUNCTIONAL BLOCK DIAGRAM


NOTES

1. $\mathrm{V}_{\text {DD1 }}$ IS THE POWER SUPPLY FOR THE PUSH-PULL TRANSFORMER.
2. VDDA IS THE POWER SUPPLY OF SIDE 1 OF THE ADuM3070.

Figure 1.

The ADuM3070 isolator provides a more stable output voltage and higher efficiency compared to unregulated isolated dc-to-dc power supplies. The fully integrated feedback and loop compensation in a small QSOP package provides a smaller form factor than any discrete solution. The regulated feedback provides a relatively flat efficiency curve over the full output power range. The ADuM3070 enables a dc-to-dc converter with a 3.3 V to 24 V isolated output voltage range from either a 5.0 V or a 3.3 V input voltage, with an output power of up to 2.5 W .

## ADuM3070

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## REVISION HISTORY

## 5/12—Revision 0: Initial Version

## SPECIFICATIONS

## ELECTRICAL CHARACTERISTICS-5 V PRIMARY INPUT SUPPLY/5 V SECONDARY ISOLATED SUPPLY

$4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD} 1}=\mathrm{V}_{\mathrm{DDA}} \leq 5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=\mathrm{V}_{\mathrm{REG}}=\mathrm{V}_{\mathrm{ISO}}=5.0 \mathrm{~V}$, $\mathrm{f}_{\mathrm{SW}}=500 \mathrm{kHz}$, all voltages are relative to their respective grounds, see the application schematic in Figure 31. All minimum/maximum specifications apply over the entire recommended operating range, unless otherwise noted. All typical specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{DD1}}=\mathrm{V}_{\mathrm{DDA}}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=\mathrm{V}_{\text {REG }}=\mathrm{V}_{\text {ISO }}=5.0 \mathrm{~V}$.

Table 1. DC-to-DC Converter Static Specifications

| Parameter | Symbol | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC-TO-DC CONVERTER SUPPLY |  |  |  |  |  |  |
| Isolated Output Voltage | Viso | 4.5 | 5.0 | 5.5 | V | $\mathrm{I}_{\text {SOO }}=0 \mathrm{~mA}, \mathrm{~V}_{\text {ISO }}=\mathrm{V}_{F B} \times(\mathrm{R} 1+\mathrm{R} 2) / \mathrm{R} 2$ |
| Feedback Voltage Setpoint | $V_{\text {fb }}$ | 1.15 | 1.25 | 1.37 | V | liso $=0 \mathrm{~mA}$ |
| Line Regulation | $V_{\text {ISO (LINE) }}$ |  | 1 | 10 | $\mathrm{mV} / \mathrm{V}$ | $\mathrm{I}_{\text {SO }}=50 \mathrm{~mA}, \mathrm{~V}_{\mathrm{DDI}}{ }^{1}=\mathrm{V}_{\text {DDA }}{ }^{2}=4.5 \mathrm{~V}$ to 5.5 V |
| Load Regulation | VISO (LOAD) |  | 1 | 2 | \% | $\mathrm{I}_{\text {so }}=50 \mathrm{~mA}$ to 200 mA |
| Output Ripple | $\mathrm{V}_{\text {ISO (R1P) }}$ |  | 50 |  | mV p-p | 20 MHz bandwidth, Cout $=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, l Iso $=100 \mathrm{~mA}$ |
| Output Noise | $V_{\text {ISO (NOISE) }}$ |  | 100 |  | mV p-p | 20 MHz bandwidth, $\mathrm{C}_{\text {out }}=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, $\mathrm{I}_{\text {so }}=100 \mathrm{~mA}$ |
| Switching Frequency | fsw |  | 1000 |  | kHz | $\mathrm{Roc}=50 \mathrm{k} \Omega$ |
|  |  |  | 200 |  | kHz | $\mathrm{Roc}=270 \mathrm{k} \Omega$ |
|  |  | 192 | 318 | 515 | kHz | $\mathrm{V}_{\text {OC }}=\mathrm{V}_{\text {DD2 }}$ (open-loop) |
| IdDA Quiescent | IDDA (Q) |  |  | 5 | mA |  |
| Switch On Resistance | Ron |  | 0.5 |  | $\Omega$ |  |
| Maximum Output Supply Current | IISO (max) | 400 | 500 |  | mA | $\mathrm{f} \leq 1 \mathrm{MHz}, \mathrm{V}_{\text {ISO }}=5.0 \mathrm{~V}$ |
| Efficiency at Maximum Output Current |  |  | 70 |  | \% | $\mathrm{I}_{\text {ISO }}=\mathrm{I}_{\text {ISO (MAX) }}, \mathrm{f} \leq 1 \mathrm{MHz}$ |

${ }^{1} V_{D D 1}$ is the power supply for the push-pull transformer.
${ }^{2} V_{\text {DDA }}$ is the power supply of Side 1 of the ADuM3070.

## ELECTRICAL CHARACTERISTICS—3.3 V PRIMARY INPUT SUPPLY/3.3 V SECONDARY ISOLATED SUPPLY

$3.0 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD} 1}=\mathrm{V}_{\mathrm{DDA}} \leq 3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=\mathrm{V}_{\mathrm{REG}}=\mathrm{V}_{\mathrm{ISO}}=3.3 \mathrm{~V}$, $\mathrm{f}_{\mathrm{SW}}=500 \mathrm{kHz}$, all voltages are relative to their respective grounds, see the application schematic in Figure 31. All minimum/maximum specifications apply over the entire recommended operating range, unless otherwise noted. All typical specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{DD1}}=\mathrm{V}_{\mathrm{DDA}}=3.3 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=\mathrm{V}_{\mathrm{REG}}=\mathrm{V}_{\mathrm{ISO}}=3.3 \mathrm{~V}$.

Table 2. DC-to-DC Converter Static Specifications

| Parameter | Symbol | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC-TO-DC CONVERTER SUPPLY |  |  |  |  |  |  |
| Isolated Output Voltage | $V_{\text {ISO }}$ | 3.0 | 3.3 | 3.63 | V | $\mathrm{I}_{\text {SO }}=0 \mathrm{~mA}, \mathrm{~V}_{\text {ISO }}=\mathrm{V}_{\text {FB }} \times(\mathrm{R} 1+\mathrm{R} 2) / \mathrm{R} 2$ |
| Feedback Voltage Setpoint | $V_{\text {Fb }}$ | 1.15 | 1.25 | 1.37 | V | $\mathrm{I}_{\text {so }}=0 \mathrm{~mA}$ |
| Line Regulation | $V_{\text {ISO (LINE) }}$ |  | 1 | 10 | $\mathrm{mV} / \mathrm{V}$ | $\mathrm{I}_{\text {So }}=50 \mathrm{~mA}, \mathrm{~V}_{\mathrm{DD} 1}{ }^{1}=\mathrm{V}_{\text {DDA }}{ }^{2}=3.0 \mathrm{~V}$ to 3.6 V |
| Load Regulation | VISO (LOAD) |  | 1 | 2 | \% | liso $=50 \mathrm{~mA}$ to 200 mA |
| Output Ripple | $V_{\text {ISO (RIP) }}$ |  | 50 |  | mVp-p | 20 MHz bandwidth, Cout $=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, liso $=100 \mathrm{~mA}$ |
| Output Noise | VISO (NOISE) |  | 100 |  | mVp-p | 20 MHz bandwidth, Cout $=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, liso $=100 \mathrm{~mA}$ |
| Switching Frequency | fsw |  | 1000 |  | kHz | $\mathrm{Roc}=50 \mathrm{k} \Omega$ |
|  |  |  | 200 |  | kHz | $\mathrm{Roc}=270 \mathrm{k} \Omega$ |
|  |  | 192 | 318 | 515 | kHz | $\mathrm{V}_{\mathrm{OC}}=\mathrm{V}_{\text {DD2 }}$ (open-loop) |
| IdDA Quiescent | IdDA (Q) |  | 2 | 3.5 | mA |  |
| Switch On Resistance | Ron |  | 0.6 |  | $\Omega$ |  |
| Maximum Output Supply Current | IISO (max) | 250 | 350 |  | mA | $\mathrm{f} \leq 1 \mathrm{MHz}, \mathrm{V}_{\text {ISO }}=3.3 \mathrm{~V}$ |
| Efficiency at Maximum Output Current |  |  | 70 |  | \% | $\mathrm{l}_{\text {ISO }}=\mathrm{I}_{\text {ISO ( }}^{\text {(Max }}$, $\mathrm{f} \leq 1 \mathrm{MHz}$ |

[^0]
## ELECTRICAL CHARACTERISTICS—5 V PRIMARY INPUT SUPPLY/3.3 V SECONDARY ISOLATED SUPPLY

$4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD} 1}=\mathrm{V}_{\mathrm{DDA}} \leq 5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=\mathrm{V}_{\mathrm{REG}}=\mathrm{V}_{\mathrm{ISO}}=3.3 \mathrm{~V}, \mathrm{f}_{\mathrm{SW}}=500 \mathrm{kHz}$, all voltages are relative to their respective grounds, see the application schematic in Figure 31. All minimum/maximum specifications apply over the entire recommended operating range, unless otherwise noted. All typical specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{DD} 1}=\mathrm{V}_{\mathrm{DDA}}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=\mathrm{V}_{\mathrm{REG}}=\mathrm{V}_{\mathrm{ISO}}=3.3 \mathrm{~V}$.

Table 3. DC-to-DC Converter Static Specifications

| Parameter | Symbol | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC-TO-DC CONVERT |  |  |  |  |  |  |
| Isolated Output Voltage | Viso | 3.0 | 3.3 | 3.63 | V | $\mathrm{I}_{\text {SOO }}=0 \mathrm{~mA}, \mathrm{~V}_{1 S O}=\mathrm{V}_{F B} \times(\mathrm{R} 1+\mathrm{R} 2) / \mathrm{R} 2$ |
| Feedback Voltage Setpoint | $V_{\text {fb }}$ | 1.15 | 1.25 | 1.37 | V | liso $=0 \mathrm{~mA}$ |
| Line Regulation | $V_{\text {ISO (LINE) }}$ |  | 1 | 10 | $\mathrm{mV} / \mathrm{V}$ | $\mathrm{I}_{150}=50 \mathrm{~mA}, \mathrm{~V}_{\mathrm{DDI}}{ }^{1}=\mathrm{V}_{\text {DDA }}{ }^{2}=4.5 \mathrm{~V}$ to 5.5 V |
| Load Regulation | VISO (LOAD) |  | 1 | 2 | \% | $\mathrm{I}_{\text {so }}=50 \mathrm{~mA}$ to 200 mA |
| Output Ripple | $V_{\text {ISO (RIP) }}$ |  | 50 |  | mV p-p | 20 MHz bandwidth, Cout $=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, liso $=100 \mathrm{~mA}$ |
| Output Noise | VISO (NOISE) |  | 100 |  | mV p-p | 20 MHz bandwidth, Cout $=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, liso $=100 \mathrm{~mA}$ |
| Switching Frequency | $\mathrm{f}_{\text {sw }}$ |  | 1000 |  | kHz | $\mathrm{R}_{\mathrm{oc}}=50 \mathrm{k} \Omega$ |
|  |  |  | 200 |  | kHz | $\mathrm{Roc}=270 \mathrm{k} \Omega$ |
|  |  | 209 | 318 | 515 | kHz | V OC $=\mathrm{V}_{\text {DD2 }}$ (open-loop) |
| IddA Quiescent | Idda (Q) |  |  | 5 | mA |  |
| Switch On Resistance | Ron |  | 0.5 |  | $\Omega$ |  |
| Maximum Output Supply Current | Iso (max) | 400 | 500 |  | mA | $\mathrm{f} \leq 1 \mathrm{MHz}$, $\mathrm{V}_{\text {ISO }}=3.3 \mathrm{~V}$ |
| Efficiency at Maximum Output Current |  |  | 70 |  | \% |  |

${ }^{1} V_{D D 1}$ is the power supply for the push-pull transformer.
${ }^{2} \mathrm{~V}_{\text {DDA }}$ is the power supply of Side 1 of the ADuM3070.

## ELECTRICAL CHARACTERISTICS—5 V PRIMARY INPUT SUPPLY/15 V SECONDARY ISOLATED SUPPLY

$4.5 \mathrm{~V} \leq \mathrm{V}_{\mathrm{DD} 1}=\mathrm{V}_{\mathrm{DDA}} \leq 5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{REG}}=\mathrm{V}_{\mathrm{ISO}}=15 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=5.0 \mathrm{~V}, \mathrm{f}_{\mathrm{SW}}=500 \mathrm{kHz}$, all voltages are relative to their respective grounds, see the application schematic in Figure 32. All minimum/maximum specifications apply over the entire recommended operating range, unless otherwise noted. All typical specifications are at $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{DD} 1}=\mathrm{V}_{\mathrm{DDA}}=5.0 \mathrm{~V}, \mathrm{~V}_{\mathrm{REG}}=\mathrm{V}_{\text {ISO }}=15 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD} 2}=5.0 \mathrm{~V}$.

Table 4. DC-to-DC Converter Static Specifications

| Parameter | Symbol | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC-TO-DC CONVERTER SUPPLY |  |  |  |  |  |  |
| Isolated Output Voltage | $V_{150}$ | 13.8 | 15.0 | 16.5 | V | $\mathrm{I}_{\text {SOO }}=0 \mathrm{~mA}, \mathrm{~V}_{\text {ISO }}=\mathrm{V}_{\text {FB }} \times(\mathrm{R} 1+\mathrm{R} 2) / \mathrm{R} 2$ |
| Feedback Voltage Setpoint | $V_{\text {fb }}$ | 1.15 | 1.25 | 1.37 | V | $\mathrm{l}_{\text {so }}=0 \mathrm{~mA}$ |
| $V_{\text {DD2 } 2}$ Linear Regulator Voltage | $V_{\text {DD2 }}$ | 4.5 | 5.0 | 5.48 | V | $\mathrm{V}_{\text {REG }}=7 \mathrm{~V}$ to 15 V , IDD2 200 mA to 50 mA |
| Dropout Voltage | V ${ }_{\text {DD2DO }}$ |  | 0.5 | 1.5 | V | $\mathrm{l}_{\mathrm{DD} 2}=50 \mathrm{~mA}$ |
| Line Regulation | VISO (LINE) |  | 1 | 10 | $\mathrm{mV} / \mathrm{V}$ | $\mathrm{I}_{\text {ISO }}=50 \mathrm{~mA}, \mathrm{~V}_{\mathrm{DD} 1^{1}}=\mathrm{V}_{\text {DDA }}{ }^{2}=4.5 \mathrm{~V}$ to 5.5 V |
| Load Regulation | VISO (LOAD) |  | 1 | 3 | \% | $\mathrm{I}_{\text {SO }}=20 \mathrm{~mA}$ to 100 mA |
| Output Ripple | $\mathrm{V}_{\text {ISO (RIP) }}$ |  | 200 |  | $m \vee p-p$ | 20 MHz bandwidth, Cout $=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, l so $=100 \mathrm{~mA}$ |
| Output Noise | VISO (NOISE) |  | 500 |  | $m \vee p-p$ | 20 MHz bandwidth, Cout $=0.1 \mu \mathrm{~F} \\| 47 \mu \mathrm{~F}$, l so $=100 \mathrm{~mA}$ |
| Switching Frequency | $\mathrm{f}_{\text {sw }}$ |  | 1000 |  | kHz | Roc $=50 \mathrm{k} \Omega$ |
|  |  |  | 200 |  | kHz | $\mathrm{Roc}=270 \mathrm{k} \Omega$ |
|  |  | 192 | 318 | 515 | kHz | $\mathrm{V}_{\mathrm{OC}}=\mathrm{V}_{\text {DD2 }}$ (open-loop) |
| Idod Quiescent | IdDA (Q) |  | 3.5 | 5 | mA |  |
| Switch On Resistance | Ron |  | 0.5 |  | $\Omega$ |  |
| Maximum Output Supply Current | IISO (max) | 100 | 140 |  | mA | $\mathrm{f} \leq 1 \mathrm{MHz}, \mathrm{V}_{\text {ISO }}=15.0 \mathrm{~V}$ |
| Efficiency at Maximum Output Current |  |  | 70 |  | \% | $\mathrm{liso}=\mathrm{l}_{\text {ISO (MAX) }}, \mathrm{f} \leq 1 \mathrm{MHz}$ |

[^1]
## PACKAGE CHARACTERISTICS

Table 5.

| Parameter | Symbol | Min | Typ | Max | Unit | Test Conditions/Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| RESISTANCE Input to Output ${ }^{1}$ | R-O |  | $10^{12}$ |  | $\Omega$ |  |
| CAPACITANCE Input to Output ${ }^{1}$ | $\mathrm{Cl}_{1-\mathrm{O}}$ |  | 2.2 |  | pF | $\mathrm{f}=1 \mathrm{MHz}$ |
| THERMAL <br> IC Junction-to-Ambient Thermal Resistance ${ }^{2}$ Thermal Shutdown <br> Threshold <br> Hysteresis | $\theta_{\mathrm{JA}}$ <br> TSsd <br> TSsd-Hys |  | $\begin{aligned} & 76 \\ & 150 \\ & 20 \end{aligned}$ |  | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ <br> ${ }^{\circ} \mathrm{C}$ <br> ${ }^{\circ} \mathrm{C}$ | TJ rising |

${ }^{1}$ The device is considered a 2-terminal device: Pin 1 to Pin 8 is shorted together, and Pin 9 to Pin 16 is shorted together.
${ }^{2}$ The thermocouple is located at the center of the package underside.

## REGULATORY APPROVALS (PENDING)

Table 6.

| UL | CSA | VDE |
| :--- | :--- | :--- |
| Recognized under the UL 1577 | Approved under CSA Component Acceptance Notice \#5A | Certified according to DIN VVDE V |
| Component Recognition Program ${ }^{1}$ |  | 0884-10 (VDE V 0884-10):2006-12² |
| Single Protection, 2500 V rms | Basic insulation per CSA 60950-1-03 and IEC 60950-1, | Reinforced insulation,560 V peak |
| Isolation Voltage | $400 \mathrm{~V} \mathrm{rms} \mathrm{(848} \mathrm{~V} \mathrm{peak)} \mathrm{maximum} \mathrm{working} \mathrm{voltage}$ |  |
| File E214100 | File 205078 | File 2471900-4880-0001 |

${ }^{1}$ In accordance with UL 1577, each ADuM3070 is proof tested by applying an insulation test voltage of $\geq 3000 \mathrm{~V} \mathrm{rms} \mathrm{for} 1$ sec (current leakage detection limit $=10 \mu \mathrm{~A}$ ).
${ }^{2}$ In accordance with DIN V VDE V 0884-10, each ADuM3070 is proof tested by applying an insulation test voltage of $\geq 1050 \mathrm{~V}$ peak for 1 sec (partial discharge detection limit $=5 \mathrm{pC}$ ). The asterisk ( ${ }^{*}$ ) marking branded on the component designates DIN V VDE V 0884-10 approval.

## INSULATION AND SAFETY RELATED SPECIFICATIONS

Table 7.

| Parameter | Symbol | Value | Unit | Test Conditions/Comments |
| :--- | :--- | :--- | :--- | :--- |
| Rated Dielectric Insulation Voltage | L(IO1) | 2500 | $>3.8$ | V rms |
| Minimum External Air Gap (Clearance) | L(I02) | $>3.1$ | mm | 1-minute duration <br> Measured from input terminals to output terminals <br> along the printed circuit board (PCB) seating plane <br> Measured from input terminals to output terminals, <br> shortest distance path along body |
| Minimum External Tracking (Creepage) | 0.017 min | mm | Distance through insulation <br> DIN IEC 112/VDE 0303 Part 1 <br> Minimum Internal Gap (Internal Clearance) | $>400$ | $\mathrm{~V} \quad$| Material Group (DIN VDE 0110, 1/89, Table 1) |
| :--- |

## ADuM3070

## DIN V VDE V 0884-10 (VDE V 0884-10) INSULATION CHARACTERISTICS

These isolators are suitable for reinforced electrical isolation only within the safety limit data. Protective circuits ensure maintenance of the safety data. The asterisk $\left(^{*}\right.$ ) marking on packages denotes DIN V VDE V 0884-10 approval.

Table 8.

| Parameter | Test Conditions/Comments | Symbol | Characteristic | Unit |
| :---: | :---: | :---: | :---: | :---: |
| Installation Classification per DIN VDE 0110 |  |  |  |  |
| For Rated Mains Voltage $\leq 150 \mathrm{~V}$ rms |  |  | I to IV |  |
| For Rated Mains Voltage $\leq 300 \mathrm{~V} \mathrm{rms}$ |  |  | I to III |  |
| For Rated Mains Voltage $\leq 400 \mathrm{~V}$ rms |  |  | I to Il |  |
| Climatic Classification |  |  | 40/105/21 |  |
| Pollution Degree per DIN VDE 0110, Table 1 |  |  | 2 |  |
| Maximum Working Insulation Voltage |  | VIorm | 560 | $V_{\text {peak }}$ |
| Input-to-Output Test Voltage, Method b1 | $V_{\text {IORM }} \times 1.875=V_{\text {pd }(m),} 100 \%$ production test, $\mathrm{t}_{\text {ini }}=\mathrm{t}_{\mathrm{m}}=1 \mathrm{sec}$, partial discharge $<5 \mathrm{pC}$ | $V_{\text {pd ( }}$ ( $)$ | 1050 | $\mathrm{V}_{\text {peak }}$ |
| Input-to-Output Test Voltage, Method a |  |  |  |  |
| After Environmental Tests Subgroup 1 | $\mathrm{V}_{\text {IORM }} \times 1.5=\mathrm{V}_{\mathrm{pd}(\mathrm{m})}, \mathrm{t}_{\text {ini }}=60 \mathrm{sec}, \mathrm{t}_{\mathrm{m}}=10 \mathrm{sec}$, partial discharge $<5 \mathrm{pC}$ | $V_{\text {pd ( }}$ ) | 840 | $\mathrm{V}_{\text {Peak }}$ |
| After Input and/or Safety Test Subgroup 2 and Subgroup 3 | $V_{\text {IORM }} \times 1.2=V_{\text {pd }(\mathrm{m})}, \mathrm{t}_{\text {ini }}=60 \mathrm{sec}, \mathrm{t}_{\mathrm{m}}=10 \mathrm{sec}$, partial discharge $<5 \mathrm{pC}$ | $V_{\text {pd ( } ~}^{\text {m }}$ ) | 672 | $\mathrm{V}_{\text {Peak }}$ |
| Highest Allowable Overvoltage |  | $V_{\text {IOTM }}$ | 3500 | $\mathrm{V}_{\text {peak }}$ |
| Withstand Isolation Voltage | 1 minute withstand rating | $V_{\text {ISO }}$ | 2500 | $V_{\text {RMS }}$ |
| Surge Isolation Voltage | $\mathrm{V}_{\text {PEAK }}=10 \mathrm{kV}, 1.2 \mu \mathrm{~s}$ rise time, $50 \mu \mathrm{~s}, 50 \%$ fall time | VIOSM | 6000 | $\mathrm{V}_{\text {peak }}$ |
| Safety Limiting Values | Maximum value allowed in the event of a failure (see Figure 2) |  |  |  |
| Case Temperature |  | Ts | 150 | ${ }^{\circ} \mathrm{C}$ |
| Side 1, Side 2 Pvdda, Pvreg Power Dissipation |  | Pvdda, Pvreg | 1.65 | W |
| Insulation Resistance at $\mathrm{T}_{\text {s }}$ | $\mathrm{V}_{10}=500 \mathrm{~V}$ | Rs | $>10^{9}$ | $\Omega$ |



Figure 2. Thermal Derating Curve, Dependence of Safety Limiting Values on Ambient Temperature, per DIN V VDE V 0884-10

## RECOMMENDED OPERATING CONDITIONS

Table 9.

| Parameter | Symbol | Min | Max | Unit |
| :--- | :--- | :--- | :--- | :--- |
| TEMPERATURE <br> Operating Temperature | $\mathrm{T}_{\mathrm{A}}$ | -40 | +105 | ${ }^{\circ} \mathrm{C}$ |
| LOAD    <br> $\quad$ Minimum Load $\mathrm{I}_{\text {SO }(\mathrm{MIN})}$ 10  |  |  |  |  |

## ABSOLUTE MAXIMUM RATINGS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 10.

| Parameter | Rating |
| :--- | :--- |
| Storage Temperature Range (TST) | $-55^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Ambient Operating Temperature | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ |
| Range ( $\mathrm{T}_{\mathrm{A}}$ ) |  |
| Supply Voltages | -0.5 V to +7.0 V |
| $\mathrm{~V}_{\text {DDA, }} \mathrm{V}_{\text {DD2 }}{ }^{1,2}$ | -0.5 V to +20.0 V |
| $\mathrm{~V}_{\text {REG }} \mathrm{X} 1, \mathrm{X}^{1}$ | $-100 \mathrm{kV} / \mu \mathrm{t}$ to $+100 \mathrm{kV} / \mu \mathrm{S}$ |
| Common-Mode Transients $^{3}$ |  |

${ }^{1}$ All voltages are relative to their respective ground.
${ }^{2} V_{D D 1}$ is the power supply for the push-pull transformer, and $V_{D D A}$ is the power supply of Side 1 of the ADuM3070.
${ }^{3}$ Refers to common-mode transients across the insulation barrier. Commonmode transients exceeding the absolute maximum ratings may cause latch-up or permanent damage.
Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Table 11. Maximum Continuous Working Voltage Supporting 50-Year Minimum Lifetime ${ }^{1}$

| Parameter | Max | Unit | Applicable <br> Certification |
| :---: | :--- | :--- | :--- |
| AC Voltage <br> Bipolar Waveform <br> Unipolar Waveform <br> Basic Insulation | 565 | V peak | 50-year minimum <br> lifetime, all <br> certifications |
| DC Voltage <br> Basic Insulation | 848 | V peak | Working voltage <br> per IEC 60950-1 |

${ }^{1}$ Refers to the continuous voltage magnitude imposed across the isolation barrier. See the Insulation Lifetime section for more information.

## ESD CAUTION



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Figure 3. Pin Configuration

See Application Note AN-1109 for specific layout guidelines.

Table 12. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 1 | X1 | Transformer Driver Output 1. |
| 2,8 | $\mathrm{GND}_{1}$ | Ground Reference for Primary Side. |
| 3,11, 12 | NC | No Connect. Do not connect to this pin. |
| 5,6 | TP | Test Point. Do not connect to this pin. |
| 4 | X2 | Transformer Driver Output 2. |
| 7 | $\mathrm{V}_{\text {DDA }}$ | Primary Supply Voltage 3.0 V to 5.5 V . Connect to $\mathrm{V}_{\mathrm{DDI}}$. Connect a $0.1 \mu \mathrm{~F}$ bypass capacitor from V $\mathrm{V}_{\text {dDA }}$ to $\mathrm{GND}_{1}$. |
| 9, 15 | $\mathrm{GND}_{2}$ | Ground Reference for Secondary Side. |
| 10 | OC | Oscillator Control Pin. When OC = logic high $=\mathrm{V}_{\mathrm{DD} 2}$, the secondary controller runs open-loop. To regulate the output voltage, connect a resistor between the OC pin and $\mathrm{GND}_{2}$, and the secondary controller runs at a frequency of 200 kHz to 1 MHz , as programmed by the resistor value. |
| 13 | FB | Feedback Input from the Secondary Output Voltage $V_{\text {iso. }}$. Use a resistor divider from $V_{\text {iso }}$ to the FB pin to make the $\mathrm{V}_{F B}$ voltage equal to the 1.25 V internal reference level using the $\mathrm{V}_{I S O}=\mathrm{V}_{F B} \times(\mathrm{R} 1+\mathrm{R} 2) / \mathrm{R} 2$ formula. The resistor divider is required even in open-loop mode to provide soft start. |
| 14 | VDD2 | Internal Supply Voltage Pin for the Secondary Side Controller. When a sufficient external voltage is supplied to $\mathrm{V}_{\mathrm{REG}}$, the internal regulator regulates the $\mathrm{V}_{\mathrm{DD} 2}$ pin to 5.0 V . Otherwise, $\mathrm{V}_{\mathrm{DD} 2}$ should be in the 3.0 V to 5.5 V range. Connect a $0.1 \mu \mathrm{~F}$ bypass capacitor from $\mathrm{V}_{\mathrm{DD} 2}$ to $\mathrm{GND}_{2}$. |
| 16 | $\mathrm{V}_{\text {REG }}$ | Input of the Internal Regulator to Power the Secondary Side Controller. $\mathrm{V}_{\text {REG }}$ should be in the 5.5 V to 15 V range to regulate the $\mathrm{V}_{\mathrm{DD} 2}$ output to 5.0 V . |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 4. Switching Frequency ( $f_{s w}$ ) vs. Roc Resistance


Figure 5. Typical Efficiency at 5 V In to 5 V Out at Various Switching Frequencies with 1:2 Coilcraft Transformer (JA4631-BL)


Figure 6. Typical Efficiency at 5 V In to 5 V Out at Various Switching Frequencies with 1:2 Halo Transformer (TGSAD-260V6LF)


Figure 7. 5 V In to 5 V Out Efficiency over Temperature with 1:2 Coilcraft Transformer (JA4631-BL) at $500 \mathrm{kHz} f_{s w}$


Figure 8. Single-Supply Efficiency with 1:2 Coilcraft Transformer (JA4631-BL) at $500 \mathrm{kHz} \mathrm{f}_{\mathrm{sw}}$


Figure 9. Typical Efficiency at 3.3 V In to 5 V Out at Various Switching Frequencies with 1:3 Halo Transformer (TGSAD-290V6LF)

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Figure 10. Typical Efficiency at 3.3 V In to 5 V Out over Temperature with 1:3 Halo Transformer (TGSAD-290V6LF) at $500 \mathrm{kHz} f_{s w}$


Figure 11.5 V In to 15 V Out Efficiency at Various Switching Frequencies with 1:3 Coilcraft Transformer (JA4650-BL)


Figure 12.5 V In to 15 V Out Efficiency at Various Switching Frequencies with 1:3 Halo Transformer (TGSAD-290V6LF)


Figure 13.5 V In to 15 V Out Efficiency over Temperature with 1:3 Coilcraft Transformer (JA4650-BL) at $500 \mathrm{kHz} f_{\text {sw }}$


Figure 14. Double-Supply Efficiency with 1:5 Coilcraft Transformer (KA4976-AL) at $500 \mathrm{kHz} \mathrm{f}_{\mathrm{sw}}$


Figure 15. Typical VIso Startup at 5 V In to 5 V Out with $10 \mathrm{~mA}, 50 \mathrm{~mA}$, and 500 mA Output Load


Figure 16. Typical VIso Startup at 5 V In to 3.3 V Out with $10 \mathrm{~mA}, 50 \mathrm{~mA}$, and 500 mA Output Load


Figure 17. Typical $V_{\text {Iso }}$ Startup at 3.3 V In to 3.3 V Out with $10 \mathrm{~mA}, 50 \mathrm{~mA}$, and 250 mA Output Load


Figure 18. Typical Viso Startup at 5 V In to 15 V Out with $10 \mathrm{~mA}, 20 \mathrm{~mA}$, and 100 mA Output Load


Figure 19. Typical Viso Load Transient Response, 5 V In to 5 V Out at $10 \%$ to $90 \%$ of 500 mA Load at $500 \mathrm{kHz} \mathrm{fsw}^{\text {sw }}$


Figure 20. Typical VIso Load Transient Response, 5 V In to 5 V Out at $10 \%$ to $90 \%$ of 500 mA Load at $500 \mathrm{kHz} f_{\text {sw }}$ with $0.1 \mu$ F Feedback Capacitor



Figure 21. Typical Viso Load Transient Load Response, 5 V In to 3.3 V Out at $10 \%$ to $90 \%$ Load of 500 mA Load at $500 \mathrm{kHz} \mathrm{f}_{\mathrm{sw}}$


Figure 22. Typical VIso Load Transient Load Response, 5 V In to 3.3 V Out at $10 \%$ to $90 \%$ Load of 500 mA Load at 500 kHz fsw with $0.1 \mu$ F Feedback Capacitor


Figure 23. Typical $V_{\text {Iso }}$ Load Transient Response, 3.3 V In to 3.3 V Out at $10 \%$ to $90 \%$ of 250 mA Load at $500 \mathrm{kHz} \mathrm{f}_{\mathrm{sw}}$


Figure 24. Typical Viso Load Transient Response, 3.3 V In to 3.3 V Out at $10 \%$ to $90 \%$ of 250 mA Load at $500 \mathrm{kHz} f_{s w}$ with $0.1 \mu$ F Feedback Capacitor


Figure 25. Typical Viso Load Transient Response, 5 V In to 15 V Out at $10 \%$ to $90 \%$ of 100 mA Load at $500 \mathrm{kHz} \mathrm{f}_{\mathrm{sw}}$


Figure 26. Typical VIso Load Transient Response, 5 V In to 15 V Out at $10 \%$ to $90 \%$ of 100 mA Load at $500 \mathrm{kHz} f_{\text {sw }}$ with $0.1 \mu$ F Feedback Capacitor


Figure 27. Typical Viso Output Ripple, 5 V In to 5 V Out at 500 mA Load at 500 kHz fsw



Figure 28. Typical VIso Output Ripple, 5 V In to 3.3 V Out at 500 mA Load at $500 \mathrm{kHz} \mathrm{fs}_{\mathrm{sw}}$



Figure 29. Typical VIIO Output Ripple, 3.3 V In to 3.3 V Out at 250 mA Load at 500 kHz fsw



Figure 30. Typical Viso Output Ripple, 5 V In to 15 V Out at 100 mA Load at 500 kHz fsw

## APPLICATIONS INFORMATION

The dc-to-dc converter section of the ADuM3070 uses a secondary side controller architecture with isolated pulse-width modulation (PWM) feedback. VDD1 power is supplied to an oscillating circuit that switches current to the primary side of an external power transformer using internal push-pull switches at the X1 and X2 pins. Power transferred to the secondary side of the transformer is full-wave rectified with external Schottky diodes (D1 and D2), filtered with the L1 inductor and Cout capacitor, and regulated to the isolated power supply voltage from 3.3 V to 15 V . The secondary ( $\mathrm{V}_{\text {ISO }}$ ) side controller regulates the output by using a feedback voltage $V_{F B}$ from a resistor divider on the output and creating a PWM control signal that is sent to the primary ( $\mathrm{V}_{\mathrm{CC}}$ ) side by a dedicated $i$ Coupler data channel labeled $V_{\text {Fb. }}$. The primary side PWM converter varies the duty cycle of the X1 and X2 switches to modulate the oscillator circuit and control the power being sent to the secondary side. This feedback allows for significantly higher power and efficiency.
The ADuM3070 implements undervoltage lockout (UVLO) with hysteresis on the VDD1 power input. This feature ensures that the converter does enter oscillation due to noisy input power or slow power-on ramp rates.
A minimum load current of 10 mA is recommended to ensure optimum load regulation. Smaller loads can generate excess noise on the output because of short or erratic PWM pulses. Excess noise generated from smaller loads can cause regulation problems, in some circumstances.

## APPLICATION SCHEMATICS

The ADuM3070 has three main application schematics, as shown in Figure 31 to Figure 33. Figure 31 has a center-tapped secondary and two Schottky diodes providing full wave rectification for a single output, typically for power supplies of $3.3 \mathrm{~V}, 5 \mathrm{~V}, 12 \mathrm{~V}$, and 15 V . For single supplies when $\mathrm{V}_{\text {ISO }}=3.3 \mathrm{~V}$ or $\mathrm{V}_{\text {ISO }}=5 \mathrm{~V}$, see the note in Figure 31 about connecting together $\mathrm{V}_{\text {reg }}, \mathrm{V}_{\mathrm{DD} 2}$, and $\mathrm{V}_{\text {ISo }}$. Figure 32 is a voltage doubling circuit that can be used for a single supply whose output exceeds 15 V , which is the largest supply that can be connected to the regulator input, $\mathrm{V}_{\mathrm{REG}}$ (Pin 16), of the part. With Figure 32, the output voltage can be as high as 24 V and the $\mathrm{V}_{\text {reg }}$ pin is only about 12 V . When using the circuit shown in Figure 32, to obtain an output voltage lower than 10 V (for example, $\mathrm{V}_{\text {DDI }}=3.3 \mathrm{~V}, \mathrm{~V}_{\text {ISO }}=5 \mathrm{~V}$ ), connect $\mathrm{V}_{\text {REG }}$ to $\mathrm{V}_{\text {ISO }}$ directly. Figure 33, which also uses a voltage doubling secondary circuit, is shown as an example of a coarsely regulated, positive power supply and an unregulated, negative power supply for outputs of approximately $\pm 5 \mathrm{~V}, \pm 12 \mathrm{~V}$, and $\pm 15 \mathrm{~V}$. For any circuit in Figure 31, Figure 32, or Figure 33, the isolated output voltage ( $\mathrm{V}_{\text {ISO }}$ ) can be set using the voltage dividers, R1 and R2 (values $1 \mathrm{k} \Omega$ to $100 \mathrm{k} \Omega$ ), using the following equation:

$$
V_{I S O}=V_{F B} \times \frac{R 1+R 2}{R 2}
$$

where $V_{F B}$ is the internal feedback voltage, which is approximately 1.25 V .


Figure 31. Single Power Supply


Figure 32. Doubling Power Supply


## TRANSFORMER DESIGN

Transformers have been designed for use in the circuits shown in Figure 31, Figure 32, and Figure 33 and are listed in Table 13. The design of a transformer for the ADuM3070 can differ from some isolated dc-to-dc converter designs that do not regulate the output voltage. The output voltage is regulated by a PWM controller in the ADuM 3070 that varies the duty cycle of the primary side switches in response to a secondary side feedback voltage, $\mathrm{V}_{\mathrm{FB}}$, received through an isolated digital channel. The internal controller has a limit of $40 \%$ maximum duty cycle.

## TRANSFORMER TURNS RATIO

To determine the transformer turns ratio, and taking into account the losses for the primary switches and the losses for the secondary diodes and inductors, the external transformer turns ratio for the ADuM 3070 can be calculated by

$$
\frac{N_{S}}{N_{P}}=\frac{V_{I S O}+V_{D}}{V_{D D I(M I N)} \times D \times 2}
$$

where:
$N_{S} / N_{P}$ is the primary to secondary turns ratio.
$V_{\text {ISO }}$ is the isolated output supply voltage.
$V_{D}$ is the Schottky diode voltage drop ( 0.5 V maximum).
$V_{D D 1 \text { (MIN) }}$ is the minimum input supply voltage.
$D$ is the duty cycle $=0.30$ for a $30 \%$ typical duty cycle, $40 \%$ is maximum, and a multiplier factor of 2 is used for the push-pull switching cycle.
For Figure 31, the 5 V to 5 V reference design in Table 13, with $\mathrm{V}_{\mathrm{DDI}}(\mathrm{MIN})=4.5 \mathrm{~V}$, the turns ratio is $\mathrm{N}_{\mathrm{S}} / \mathrm{N}_{\mathrm{P}}=2$.

For a similar 3.3 V input to 3.3 V output, isolated single power supply and with $\mathrm{V}_{\mathrm{DDI}(\mathrm{MIN})}=3.0 \mathrm{~V}$, the turns ratio is also $\mathrm{N}_{\mathrm{s}} / \mathrm{N}_{\mathrm{P}}=$ 2. Therefore, the same transformer turns ratio $\mathrm{N}_{\mathrm{S}} / \mathrm{N}_{\mathrm{P}}=2$ can be used for the three single power applications ( 5 V to $5 \mathrm{~V}, 5 \mathrm{~V}$ to 3.3 V , and 3.3 V to 3.3 V ).

For Figure 32, the circuit uses double windings and diode pairs to create a doubler circuit; therefore, half the output voltage, $\mathrm{V}_{\mathrm{ISO}} / 2$, is used in the equation.

$$
\frac{N_{S}}{N_{P}}=\frac{\frac{V_{I S O}}{2}+V_{D}}{V_{D D I(M I N)} \times D \times 2}
$$

$N_{S} / N_{P}$ is the primary to secondary turns ratio.
$V_{I S O} / 2$ is used in the equation because the circuit uses two pairs of diodes creating a doubler circuit.
$V_{D}$ is the Schottky diode voltage drop ( 0.5 V maximum).
$V_{D D 1 \text { (MIN) }}$ is the minimum input supply voltage.
$D$ is the duty cycle, which is 0.30 for a $30 \%$ typical duty cycle and 0.40 for a $40 \%$ maximum duty cycle, and a multiplier factor of two is used for the push-pull switching cycle.
For Figure 32, the 5 V to 15 V reference design in Table 13, with $\mathrm{V}_{\mathrm{DDI}(\mathrm{MIN})}=4.5 \mathrm{~V}$, results in a turns ratio of $\mathrm{N}_{\mathrm{S}} / \mathrm{N}_{\mathrm{P}}=3$.

For Figure 33, the circuit also uses double windings and diode pairs to create a doubler circuit; however, because a positive and negative output voltage is created, $V_{I S O}$ is used in the equation.

$$
\frac{N_{S}}{N_{P}}=\frac{V_{I S O}+V_{D}}{V_{D D I(M I N)} \times D \times 2}
$$

where:
$N_{S} / N_{P}$ is the primary to secondary turns ratio.
$V_{I S O}$ is the isolated output supply voltage and is used in the equation because the circuit uses two pairs of diodes creating a doubler circuit with a positive and negative output. $V_{D}$ is the Schottky diode voltage drop ( 0.5 V maximum).
$V_{D D I(M I N)}$ is the minimum input supply voltage, and a multiplier factor of 2 is used for the push-pull switching cycle.
$D$ is the duty cycle; in this case, a higher duty cycle of $D=0.35$ for a $35 \%$ typical duty cycle ( $40 \%$ maximum duty cycle) was used in the Figure 33 circuit to reduce the maximum voltages seen by the diodes for a $\pm 15 \mathrm{~V}$ supply.

For Figure 33, the +5 V to $\pm 15 \mathrm{~V}$ reference design in Table 13, with $\mathrm{V}_{\mathrm{DDI}(\mathrm{MIN})}=4.5 \mathrm{~V}$, results in a turns ratio of $\mathrm{N}_{\mathrm{S}} / \mathrm{N}_{\mathrm{P}}=5$.

## TRANSFORMER ET CONSTANT

The next transformer design factor to consider is the ET constant. This constant determines the minimum $V \times \mu \mathrm{s}$ constant of the transformer over the operating temperature. ET values of $14 \mathrm{~V} \times \mu \mathrm{s}$ and $18 \mathrm{~V} \times \mu \mathrm{s}$ were selected for the ADuM3070 designs listed in Table 13 using the following equation:

$$
E T(M I N)=\frac{V_{D D 1(M A X)}}{f_{S W(M I N)} \times 2}
$$

where:
$V_{D D I(M A X)}$ is the maximum input supply voltage.
$f_{S W(M I N)}$ is the minimum primary switching frequency $=300 \mathrm{kHz}$
in startup, and a multiplier factor of 2 is used for the push-pull switching cycle.

## TRANSFORMER PRIMARY INDUCTANCE AND RESISTANCE

Another important characteristic of the transformer for designs with the ADuM3070 is the primary inductance. Transformers for the ADuM3070 are recommended to have between $60 \mu \mathrm{H}$ to $100 \mu \mathrm{H}$ of inductance per primary winding. Values of primary inductance in this range are needed for smooth operation of the ADuM3070 pulse-by-pulse current-limit circuit, which can help protect against build up of saturation currents in the transformer. If the inductance is specified for the total of both primary windings, for example, as $400 \mu \mathrm{H}$, the inductance of one winding is $1 / 4$ of two equal windings, or $100 \mu \mathrm{H}$.

Another important characteristic of the transformer for designs with the ADuM3070 is primary resistance. Primary resistance as low as is practical (less than $1 \Omega$ ) helps reduce losses and improves efficiency. The total primary resistance can be measured and specified, and is shown for the transformers in Table 13.

## ADuM3070

Table 13. Transformer Reference Designs

| Part No. | Manufacturer | Turns Ratio, <br> PRI:SEC | ET Constant <br> $\mathbf{( V \times \mu \mathbf { M i n } )}$ | Total Primary <br> Inductance $(\boldsymbol{\mu H})$ | Total Primary <br> Resistance $(\boldsymbol{\Omega})$ | Isolation <br> Voltage $(\mathbf{r m s})$ | Isolation <br> Type | Reference |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

## TRANSFORMER ISOLATION VOLTAGE

Isolation voltage and isolation type should be determined for the requirements of the application and then specified. The transformers in Table 13 have been specified for 2500 V rms for supplemental or basic isolation and for 1500 V rms for functional isolation. Other isolation levels and isolation voltages can be specified and requested from the manufacturers that are listed in Table 13 or from other manufacturers.

## SWITCHING FREQUENCY

The ADuM3070 switching frequency can be adjusted from 200 kHz to 1 MHz by changing the value of the Roc resistor shown in Figure 31, Figure 32, and Figure 33. The value of the Roc resistor needed for the desired switching frequency can be determined from the switching frequency vs. Roc resistance curve shown in Figure 4. The output filter inductor value and output capacitor value for the ADuM 3070 application schematics have been designed to be stable over the switching frequency range from 500 kHz to 1 MHz , when loaded from $10 \%$ to $90 \%$ of the maximum load.

The ADuM3070 also has an open-loop mode where the output voltage is not regulated and is dependent on the transformer turns ratio, $\mathrm{N}_{\mathrm{S}} / \mathrm{N}_{\mathrm{P}}$, and the conditions of the output including output load current and the losses in the dc-to-dc converter circuit. This open-loop mode is selected when the OC pin is connected high to the $V_{\text {DD } 2}$ pin. In open-loop mode, the switching frequency is 318 kHz .

## TRANSIENT RESPONSE

The load transient response of the output voltage of the ADuM3070 for $10 \%$ to $90 \%$ of the full load is shown in Figure 19 to Figure 26 for the application schematics in Figure 31 and Figure 32. The response shown is slow but stable and can have more output change than desired for some applications. The output voltage change with load transient has been reduced, and the output has been shown to remain stable by adding more inductance to the output circuits, as shown in the second $\mathrm{V}_{\text {ISO }}$ output waveform in Figure 19 to Figure 26.

For additional improvement in transient response, add a $0.1 \mu \mathrm{~F}$ ceramic capacitor $\left(\mathrm{C}_{\mathrm{FB}}\right)$ in parallel with the high feedback resistor. As shown in Figure 19 to Figure 26, this value helps reduce the overshoot and undershoot during load transients.

## COMPONENT SELECTION

Power supply bypassing is required at the input and output supply pins. Note that a low ESR ceramic bypass capacitor of $0.1 \mu \mathrm{~F}$ is required on Side 1 between Pin 7 and Pin 8, and on Side 2 between Pin 14 and Pin 15, as close to the chip pads as possible.
The power supply section of the ADuM3070 uses a high oscillator frequency to efficiently pass power through the external power transformer. Bypass capacitors are required for several operating frequencies. Noise suppression requires a low inductance, high frequency capacitor; ripple suppression and proper regulation require a large value capacitor. To suppress noise and reduce ripple, large valued ceramic capacitors of X5R or X7R dielectric type are recommended. The recommended capacitor value is $10 \mu \mathrm{~F}$ for $\mathrm{V}_{\text {DDI }}$ and $47 \mu \mathrm{~F}$ for $\mathrm{V}_{\text {ISO }}$. These capacitors have a low ESR and are available in moderate 1206 or 1210 sizes for voltages up to 10 V . For output voltages larger than 10 V , two $22 \mu \mathrm{~F}$ ceramic capacitors can be used in parallel. See Table 14 for recommended components.
Inductors must be selected based on the value and supply current needed. Most applications with switching frequencies between 500 kHz and 1 MHz and load transients between $10 \%$ and $90 \%$ of full load are stable with the $47 \mu \mathrm{H}$ inductor value listed in Table 14. Values as large as $200 \mu \mathrm{H}$ can be used for power supply applications with a switching frequency as low as 200 kHz to help stabilize the output voltage or for improved load transient response (see Figure 19 to Figure 26). Inductors in a small 1212 or 1210 size are listed in Table 14 with a $47 \mu \mathrm{H}$ value and a 0.41 A current rating to handle the majority of applications below a 400 mA load, and with a $100 \mu \mathrm{H}$ value and a 0.34 A current rating to handle a load to 300 mA .
Schottky diodes are recommended for their low forward voltage to reduce losses and their high reverse voltage of up to 40 V to withstand the peak voltages available in the doubling circuit shown in Figure 32 and Figure 33.

Table 14. Recommended Components

| Part Number | Manufacturer | Value |
| :--- | :--- | :--- |
| GRM32ER71A476KE15L | Murata | $47 \mu \mathrm{~F}, 10 \mathrm{~V}, \mathrm{X7R}$, |
|  |  | 1210 |
| GRM32ER71C226KEA8L | Murata | $22 \mu \mathrm{~F}, 16 \mathrm{~V}, \mathrm{X} 7 \mathrm{R}$, |
|  |  | 1210 |
| GRM31CR71A106KA01L | Murata | $10 \mu \mathrm{~F}, 10 \mathrm{~V}, \mathrm{X7R}$, |
|  |  | 1206 |
| MBR0540T1/D | ON Semiconductor | $0.5 \mathrm{~A}, 40 \mathrm{~V}$, |
|  |  | Schottky, SOD-123 |
| LQH3NPN470MM0 | Murata | $47 \mu \mathrm{H}, 0.41 \mathrm{~A}$, |
|  |  |  |
| ME3220-104KL |  | 1212 |
|  |  | $100 \mu \mathrm{H}, 0.34 \mathrm{~A}$, |

## PRINTED CIRCUIT BOARD (PCB) LAYOUT

Note that the total lead length between the ends of the low ESR capacitor and the $\mathrm{V}_{\mathrm{DDx}}$ and $\mathrm{GND}_{\mathrm{x}}$ pins must not exceed 2 mm . See Figure 34 for the recommended PCB layout.


Figure 34. Recommended PCB Layout
In applications involving high common-mode transients, ensure that board coupling across the isolation barrier is minimized. Furthermore, design the board layout such that any coupling that does occur equally affects all pins on a given component side. Failure to ensure this can cause voltage differentials between pins, exceeding the absolute maximum ratings specified in Table 10, thereby leading to latch-up and/or permanent damage.
The ADuM3070 is a power device that dissipates about 1 W of power when fully loaded. Because it is not possible to apply a heat sink to an isolation device, the device primarily depends on heat dissipation into the PCB through the $\mathrm{GND}_{\mathrm{x}}$ pins. If the device is used at high ambient temperatures, care must be taken to provide a thermal path from the $\mathrm{GND}_{\mathrm{x}}$ pins to the PCB ground plane.

The board layout shows enlarged pads for the $\mathrm{GND}_{\mathrm{x}}$ pins (Pin 2 and Pin 8) on Side 1 and (Pin 9 and Pin 15) on Side 2. Implement large diameter vias from the pad to the ground planes and power planes to increase thermal conductivity and to reduce inductance. Multiple vias in the thermal pads can significantly reduce temperatures inside the chip. The dimensions of the expanded pads are left to the discretion of the designer and the available board space.

## THERMAL ANALYSIS

The ADuM3070 parts consist of two internal die attached to a split lead frame with two die attach paddles. For the purposes of thermal analysis, the die is treated as a thermal unit, with the highest junction temperature reflected in the $\theta_{\mathrm{JA}}$ from Table 5. The value of $\theta_{\text {JA }}$ is based on measurements taken with the devices mounted on a JEDEC standard, 4-layer board with fine width traces and still air. Under normal operating conditions, the ADuM3070 devices operate at full load across the full temperature range without derating the output current. However, following the recommendations in the Printed Circuit Board (PCB) Layout section decreases thermal resistance to the PCB, allowing increased thermal margins in high ambient temperatures. The ADuM3070 has a thermal shutdown circuit that shuts down the dc-to-dc converter of the ADuM 3070 when a die temperature of about $160^{\circ} \mathrm{C}$ is reached. When the die cools below about $140^{\circ} \mathrm{C}$, the ADuM3070 dc-to-dc converter turns on again.

## POWER CONSUMPTION

The total input supply current is equal to the sum of the IDDI primary transformer current and the ADuM3070 input current, $\mathrm{I}_{\mathrm{DDA}}$.
The following relationship allows the total $\mathrm{I}_{\text {IN }}$ current to be:

$$
\begin{equation*}
I_{I N}=\left(I_{I S O} \times V_{I S O}\right) /\left(E \times V_{D D I}\right) \tag{1}
\end{equation*}
$$

where:
$I_{I N}$ is the total supply input current.
IIso is the current drawn by the secondary side external load.
$E$ is the power supply efficiency at the given output load from
Figure 8 or Figure 14 at the $V_{I S O}$ and $V_{D D I}$ condition of interest.


NOTES

1. $\mathrm{V}_{\mathrm{DD} 1}$ IS THE POWER SUPPLY FOR THE PUSH-PULL TRANSFORMER.
2. VDDA IS THE POWER SUPPLY OF SIDE 1 OF THE ADuM3070.

## POWER CONSIDERATIONS

## Soft Start Mode and Current-Limit Protection

When the ADuM3070 first receives power from $V_{D D 1}$, it is in soft start mode, and the output voltage, $\mathrm{V}_{\text {ISO }}$, is increased gradually while it is below the startup threshold. In soft start mode, to limit the peak current during $\mathrm{V}_{\text {ISo }}$ power-up, the primary converter gradually increases the width of the PWM signal. When the output voltage is larger than the start-up threshold, the PWM signal can be transferred from the secondary controller to the primary converter, and the dc-to-dc converter switches from soft start mode to the normal PWM control mode. If a short circuit occurs, the push-pull converter shuts down for about 2 ms and then enters soft start mode. If, at the end of soft start, a short circuit still exists, the process is repeated, which is called hiccup mode. If the short circuit is cleared, the ADuM3070 enters normal operation.
The ADuM3070 has a pulse-by-pulse current limit, which is active at startup and during normal operation, that protects the primary switches, X1 and X2, from exceeding approximately 1.3 A peak, protecting the transformer windings.

## INSULATION LIFETIME

All insulation structures eventually break down when subjected to voltage stress over a sufficiently long period. The rate of insulation degradation is dependent on the characteristics of the voltage waveform applied across the insulation. Analog Devices, Inc., conducts an extensive set of evaluations to determine the lifetime of the insulation structure within the ADuM3070. Accelerated life testing is performed using voltage levels higher than the rated continuous working voltage. Acceleration factors for several operating conditions are determined, allowing calculation of the time to failure at the working voltage of interest. The values shown in Table 11 summarize the peak voltages for 50 years of service life in several operating conditions. In many cases, the working voltage approved by agency testing is higher than the 50 -year service life voltage. Operation at working voltages higher than the service life voltage listed leads to premature insulation failure.

The insulation lifetime of the ADuM3070 depends on the voltage waveform type imposed across the isolation barrier. The $i$ Coupler insulation structure degrades at different rates, depending on whether the waveform is bipolar ac, dc, or unipolar ac. Figure 36, Figure 37, and Figure 38 illustrate these different isolation voltage waveforms.

Bipolar ac voltage is the most stringent environment. A 50 -year operating lifetime under the bipolar ac condition determines the Analog Devices recommended maximum working voltage.
In the case of unipolar ac or dc voltage, the stress on the insulation is significantly lower. This allows operation at higher working voltages while still achieving a 50 -year service life. The working voltages listed in Table 11 can be applied while maintaining the 50 -year minimum lifetime, if the voltage conforms to either the unipolar ac or dc voltage cases. Treat any cross-insulation voltage waveform that does not conform to Figure 37 or Figure 38 as a bipolar ac waveform, and limit its peak voltage to the 50 -year lifetime voltage value listed in Table 11.

RATED PEAK VOLTAGE


Figure 37. DC Waveform

RATED PEAK VOLTAGE


NOTES

1. THE VOLTAGE IS SHOWN SINUSOIDAL FOR ILLUSTRATION PURPOSES ONLY. IT IS MEANT TO REPRESENT ANY VOLTAGE WAVEFORM VARYING BETWEEN O AND SOME LIMITING VALUE. THE LIMITING VALUE CAN BE POSITIVE OR NEGATIVE, BUT THE VOLTAGE
CANNOT CROSS OV.

Figure 38. Unipolar AC Waveform

## OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MO-137-AB
CONTROLLING DIMENSIONS ARE IN INCHES; MILLIMETER DIMENSIONS (IN PARENTHESES) ARE ROUNDED-OFF INCH EQUIVALENTS FOR REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

Figure 39. 16-Lead Shrink Small Outline Package [QSOP]
(RQ-16)
Dimension shown in inches and (millimeters)

## ORDERING GUIDE

| Model $^{1,2}$ | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| ADuM3070ARQZ | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | 16 -Lead Shrink Small Outline Package [QSOP] <br> Evaluation Board | RQ-16 |

[^2]
## ADuM3070

## NOTES


[^0]:    ${ }^{1} V_{\text {DDI }}$ is the power supply for the push-pull transformer.
    ${ }^{2} V_{\text {DDA }}$ is the power supply of Side 1 of the ADuM3070.

[^1]:    ${ }^{1} V_{D D 1}$ is the power supply for the push-pull transformer.
    ${ }^{2} \mathrm{~V}_{\text {DDA }}$ is the power supply of Side 1 of the ADuM3070.

[^2]:    ${ }^{1}$ Tape and reel are available. The addition of an -RL7 suffix designates a 7 " (1000 units) tape and reel option.
    ${ }^{2}$ Z = RoHS Compliant Part.

