

FEATURES

- RF frequency range of 2300 MHz to 2900 MHz
- IF frequency range of dc to 450 MHz
- Power conversion loss: 7.7 dB
- SSB noise figure of 7.6 dB
- Input IP3 of 31 dBm
- Typical LO drive of 0 dBm
- Single-ended, 50 Ω RF and LO input ports
- High isolation SPDT LO input switch
- Single-supply operation: 3.3 V to 5 V
- Exposed pad, 5 mm \times 5 mm 20-lead LFCSP
- 1500 V HBM/1250 V FICDM ESD performance

APPLICATIONS

- Cellular base station receivers
- Transmit observation receivers
- Radio link downconverters

GENERAL DESCRIPTION

The **ADL5363** uses a highly linear, doubly balanced passive mixer core along with integrated RF and local oscillator (LO) balancing circuitry to allow for single-ended operation. The **ADL5363** incorporates an RF balun to provide optimal performance over a 2300 MHz to 2900 MHz input frequency range. The balanced passive mixer arrangement provides good LO-to-RF leakage, typically better than -30 dBm, and excellent intermodulation performance. The balanced mixer core also provides extremely high input linearity, allowing the device to be used in demanding cellular applications where in-band blocking signals might otherwise result in the degradation of dynamic performance.

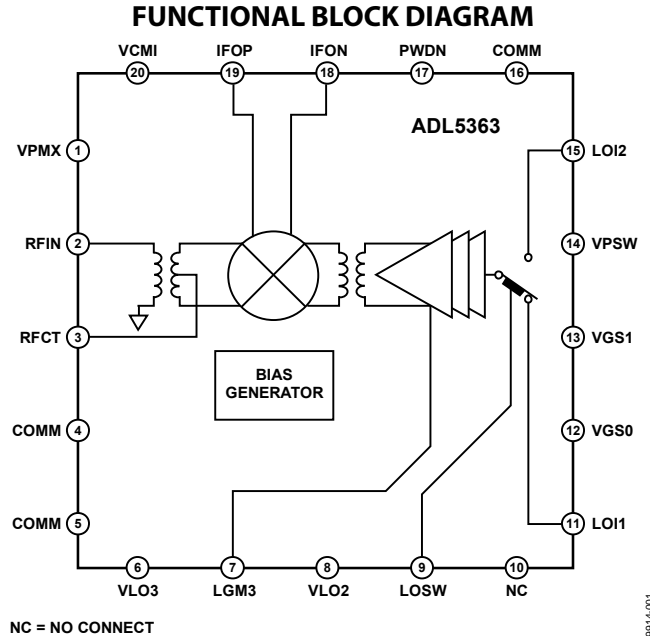


Figure 1.

The **ADL5363** provides two switched LO paths that can be used in TDD applications where it is desirable to rapidly switch between two local oscillators. LO current can be externally set using a resistor to minimize dc current commensurate with the desired level of performance. For low voltage applications, the **ADL5363** is capable of operation at voltages down to 3.3 V with substantially reduced current. For low voltage operation, an additional logic pin is provided to power down ($<200 \mu\text{A}$) the circuit when desired.

The **ADL5363** is fabricated using a BiCMOS high performance IC process. The device is available in a 5 mm \times 5 mm LFCSP and operates over a -40°C to $+85^\circ\text{C}$ temperature range. An evaluation board is also available.

Table 1. Passive Mixers

RF Frequency (MHz)	Single Mixer	Single Mixer and IF Amp	Dual Mixer and IF Amp
500 to 1700	ADL5367	ADL5357	ADL5358
1200 to 2500	ADL5365	ADL5355	ADL5356
2300 to 2900	ADL5363	ADL5353	ADL5354

Rev. 0

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REVISION HISTORY

7/11—Revision 0: Initial Version

SPECIFICATIONS

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $Z_O = 50\ \Omega$, unless otherwise noted.

Table 2.

Parameter	Test Conditions/Comments	Min	Typ	Max	Unit
RF INPUT INTERFACE					
Return Loss	Tunable to >20 dB over a limited bandwidth		16		dB
Input Impedance			50		Ω
RF Frequency Range		2300		2900	MHz
OUTPUT INTERFACE					
Output Impedance	Differential impedance, $f = 200\text{ MHz}$		33 -0.3		Ω pF
IF Frequency Range		dc		450	MHz
DC Bias Voltage ¹	Externally generated	3.3	5.0	5.5	V
LO INTERFACE					
LO Power		-6	0	+10	dBm
Return Loss			15		dB
Input Impedance			50		Ω
LO Frequency Range		2330		3350	MHz
POWER-DOWN (PWDN) INTERFACE ²					
PWDN Threshold			1.0		V
Logic 0 Level				0.4	V
Logic 1 Level		1.4			V
PWDN Response Time	Device enabled, IF output to 90% of its final level		160		ns
	Device disabled, supply current <5 mA		220		ns
PWDN Input Bias Current	Device enabled		0.0		μA
	Device disabled		70		μA

¹ Apply the supply voltage from the external circuit through the choke inductors.

² The PWDN function is intended for use with $V_S \leq 3.6\text{ V}$ only.

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5 V PERFORMANCE

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, VGS0 = VGS1 = 0 V, and $Z_O = 50\ \Omega$, unless otherwise noted.

Table 3.

Parameter	Test Conditions/Comments	Min	Typ	Max	Unit
DYNAMIC PERFORMANCE					
Power Conversion Loss	Including 1:1 IF port transformer and PCB loss		7.7		dB
SSB Noise Figure			7.6		dB
Input Third-Order Intercept (IIP3)	$f_{RF1} = 2534.5\text{ MHz}$, $f_{RF2} = 2535.5\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, each RF tone at 0 dBm		31		dBm
Input Second-Order Intercept (IIP2)	$f_{RF1} = 2535\text{ MHz}$, $f_{RF2} = 2585\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, each RF tone at 0 dBm		62		dBm
Input 1 dB Compression Point (IP1dB) ¹	Exceeding 20 dBm RF power results in damage to the device		25		dBm
LO-to-IF Leakage	Unfiltered IF output		-22		dBm
LO-to-RF Leakage			-32		dBm
RF-to-IF Isolation			-44		dBc
IF/2 Spurious	-10 dBm input power		-61		dBc
IF/3 Spurious	-10 dBm input power		-70		dBc
POWER SUPPLY					
Positive Supply Voltage		4.5	5	5.5	V
Quiescent Current	$V_S = 5\text{ V}$		100		mA

¹ Exceeding 20 dBm RF power results in damage to the device.

3.3 V PERFORMANCE

$V_S = 3.3\text{ V}$, $I_S = 60\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $R_9 = 226\ \Omega$, VGS0 = VGS1 = 0 V, and $Z_O = 50\ \Omega$, unless otherwise noted.

Table 4.

Parameter	Test Conditions/Comments	Min	Typ	Max	Unit
DYNAMIC PERFORMANCE					
Power Conversion Loss	Including 1:1 IF port transformer and PCB loss		7.4		dB
SSB Noise Figure			6.8		dB
Input Third-Order Intercept (IIP3)	$f_{RF1} = 2534.5\text{ MHz}$, $f_{RF2} = 2535.5\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, each RF tone at 0 dBm		26		dBm
Input Second-Order Intercept (IIP2)	$f_{RF1} = 2535\text{ MHz}$, $f_{RF2} = 2585\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, each RF tone at 0 dBm		56		dBm
POWER SUPPLY					
Positive Supply Voltage			3.3		V
Quiescent Current	$V_S = 5\text{ V}$		60		mA

ABSOLUTE MAXIMUM RATINGS

Table 5.

Parameter	Rating
Supply Voltage, V_S	5.5 V
RF Input Level	20 dBm
LO Input Level	13 dBm
IFOP, IFON Bias Voltage	6.0 V
VGS0, VGS1, LOSW, PWDN	5.5 V
Internal Power Dissipation	0.5 W
Thermal Resistance, θ_{JA}	25°C/W
Temperature	
Maximum Junction Temperature	150°C
Operating Temperature Range	-40°C to +85°C
Storage Temperature Range	-65°C to +150°C
Lead Temperature (Soldering, 60 sec)	260°C

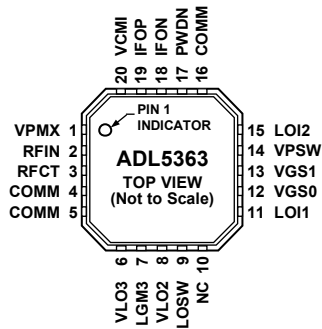
Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ESD CAUTION



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



- NOTES**
1. NC = NO CONNECT. DO NOT CONNECT TO THIS PIN.
 2. EXPOSED PAD. MUST BE SOLDERED TO GROUND.

09914-002

Figure 2. Pin Configuration

Table 6. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	VPMX	Positive Supply Voltage.
2	RFIN	RF Input. Must be ac-coupled.
3	RFCT	RF Balun Center Tap (AC Ground).
4, 5, 16	COMM	Device Common (DC Ground).
6, 8	VLO3, VLO2	Positive Supply Voltages for LO Amplifier.
7	LGM3	LO Amplifier Bias Control.
9	LOSW	LO Switch. LOI1 selected for 0 V, and LOI2 selected for 3 V.
10	NC	No Connect.
11, 15	LOI1, LOI2	LO Inputs. Must be ac-coupled.
12, 13	VGS0, VGS1	Mixer Gate Bias Controls. 3 V logic. Ground these pins for nominal setting.
14	VPSW	Positive Supply Voltage for LO Switch.
17	PWDN	Power Down. Connect this pin to ground for normal operation and connect this pin to 3.0 V for disable mode.
18, 19	IFON, IFOP	Differential IF Outputs.
20	VCM1	No Connect. This pin can be grounded.
	EPAD (EP)	Exposed pad. Must be soldered to ground.

TYPICAL PERFORMANCE CHARACTERISTICS

5 V PERFORMANCE

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, VGS0 = VGS1 = 0 V, and $Z_O = 50\ \Omega$, unless otherwise noted.

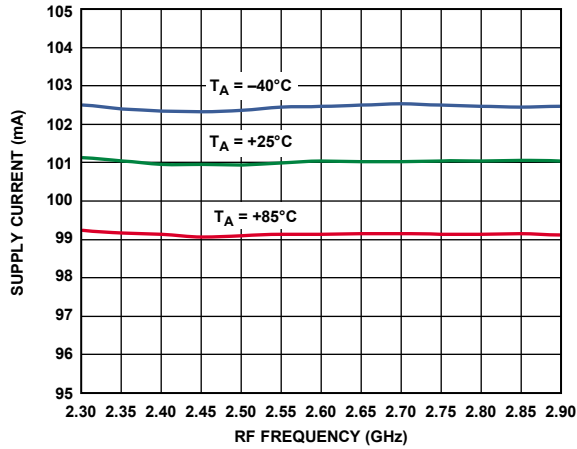


Figure 3. Supply Current vs. RF Frequency

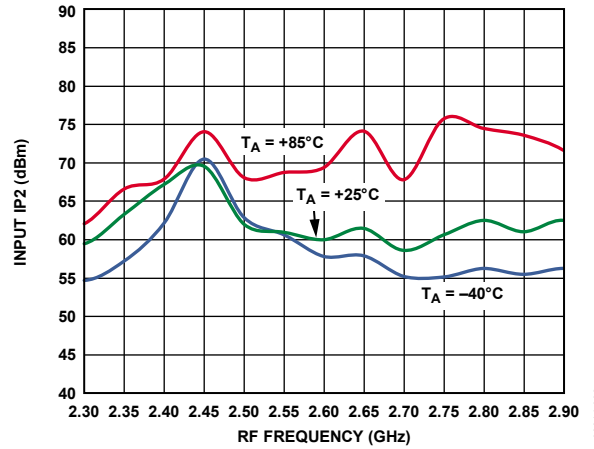


Figure 6. Input IP2 vs. RF Frequency

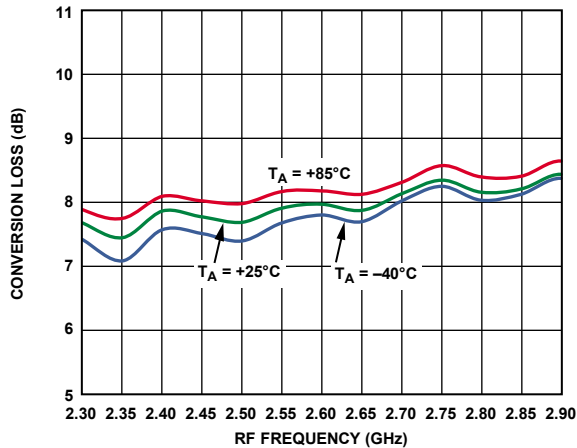


Figure 4. Power Conversion Loss vs. RF Frequency

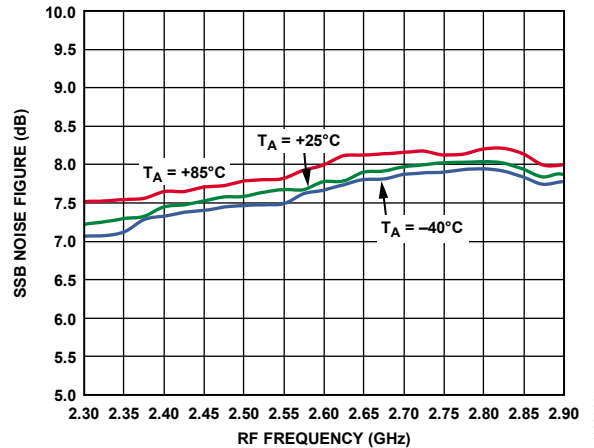


Figure 7. SSB Noise Figure vs. RF Frequency

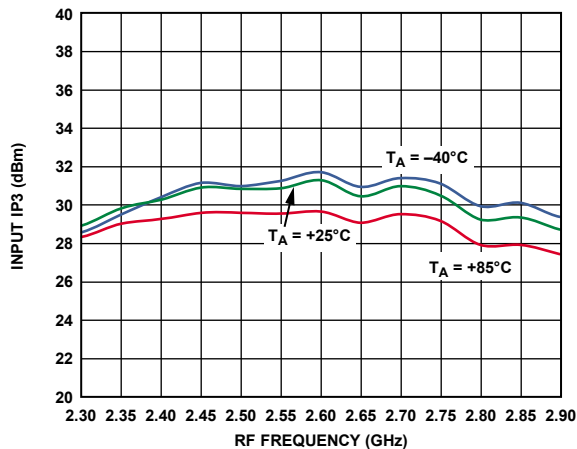


Figure 5. Input IP3 vs. RF Frequency

08914-003

08914-006

08914-004

08914-007

08914-005

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$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, VGS0 = VGS1 = 0 V, and $Z_O = 50\ \Omega$, unless otherwise noted.

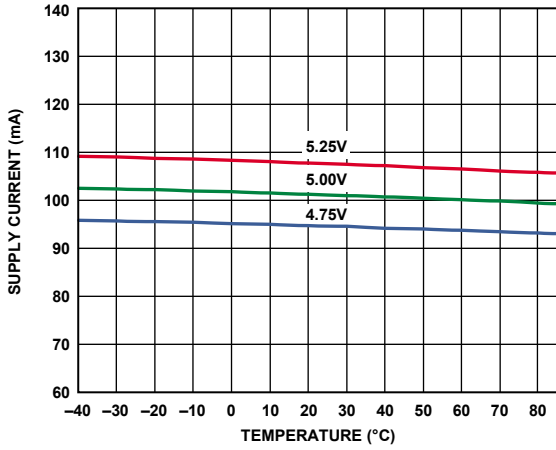


Figure 8. Supply Current vs. Temperature

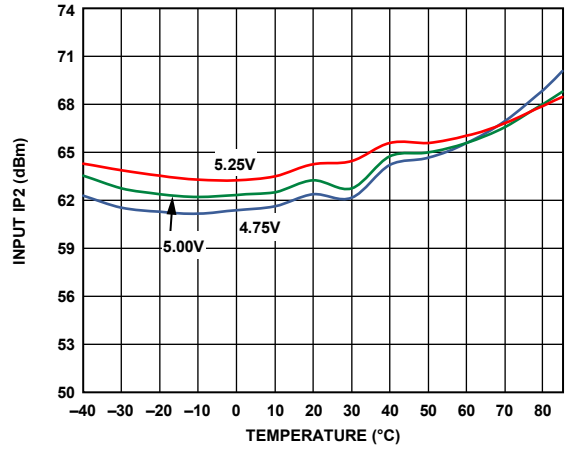


Figure 11. Input IP2 vs. Temperature

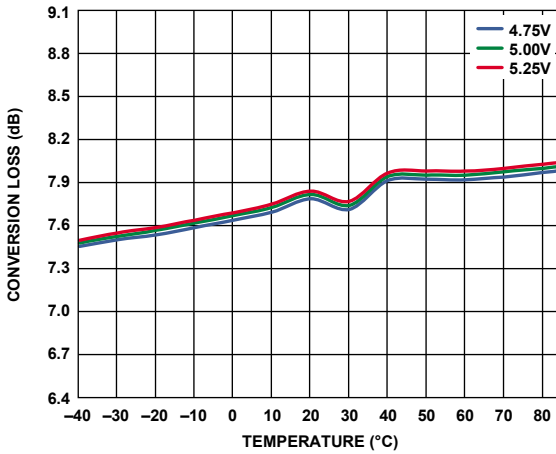


Figure 9. Power Conversion Loss vs. Temperature

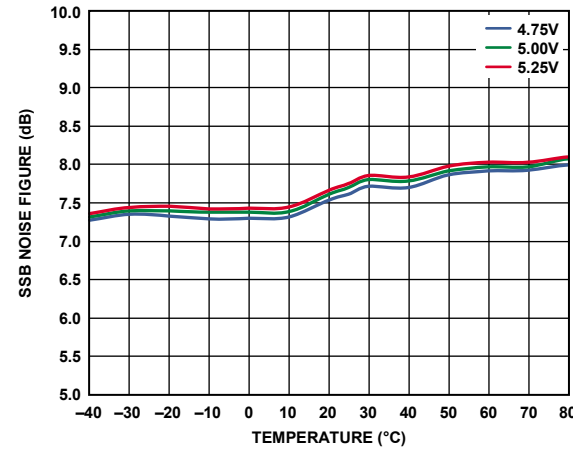


Figure 12. SSB Noise Figure vs. Temperature

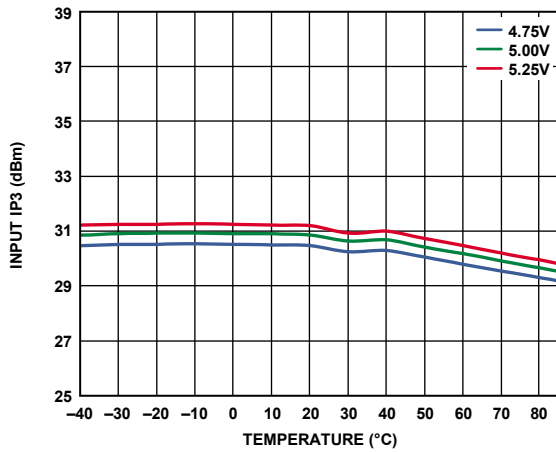


Figure 10. Input IP3 vs. Temperature

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $V_{GS0} = V_{GS1} = 0\text{ V}$, and $Z_O = 50\ \Omega$, unless otherwise noted.

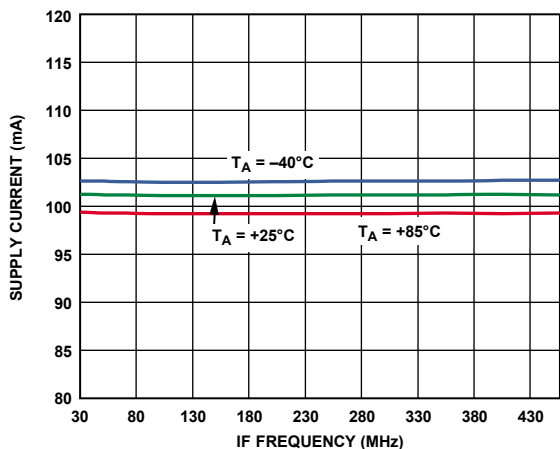


Figure 13. Supply Current vs. IF Frequency

09914-013

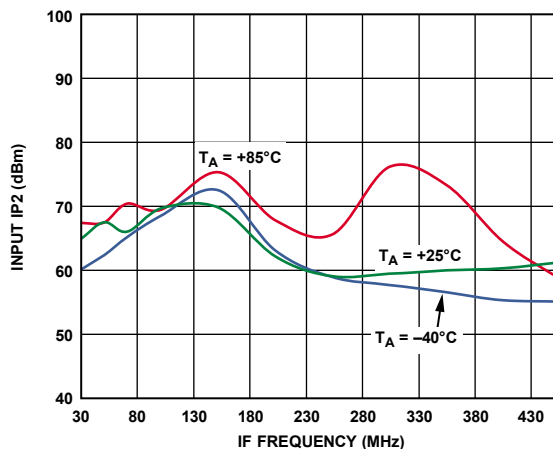


Figure 16. Input IP2 vs. IF Frequency

09914-016

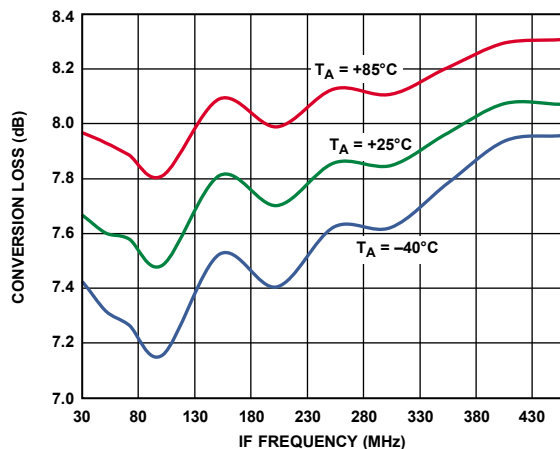


Figure 14. Power Conversion Loss vs. IF Frequency

09914-014

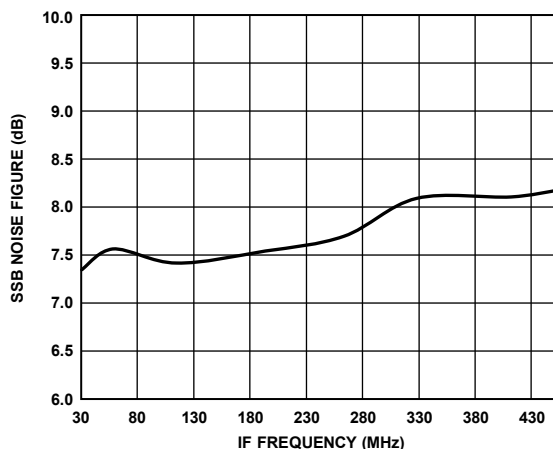


Figure 17. SSB Noise Figure vs. IF Frequency

09914-017

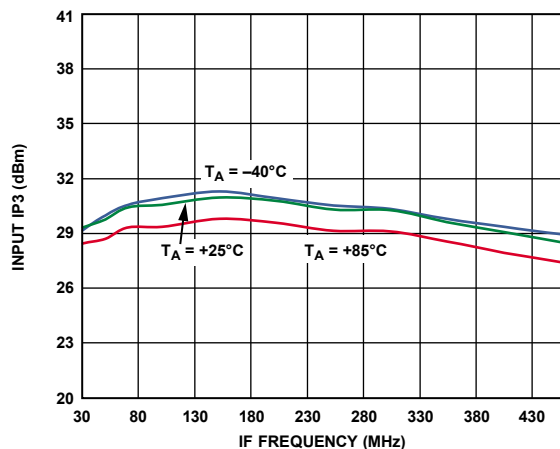


Figure 15. Input IP3 vs. IF Frequency

09914-015

ADL5363

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $V_{GS0} = V_{GS1} = 0\text{ V}$, and $Z_O = 50\ \Omega$, unless otherwise noted.

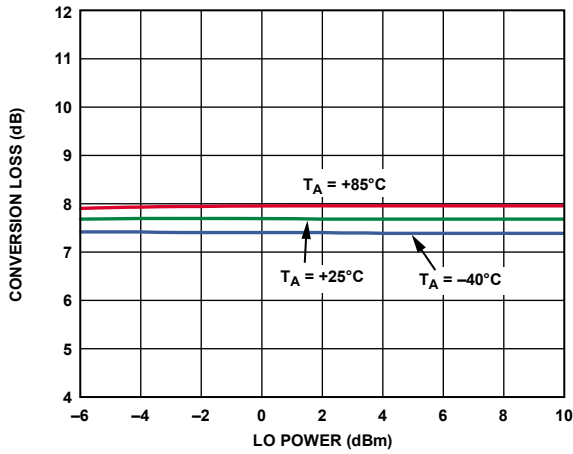


Figure 18. Power Conversion Loss vs. LO Power

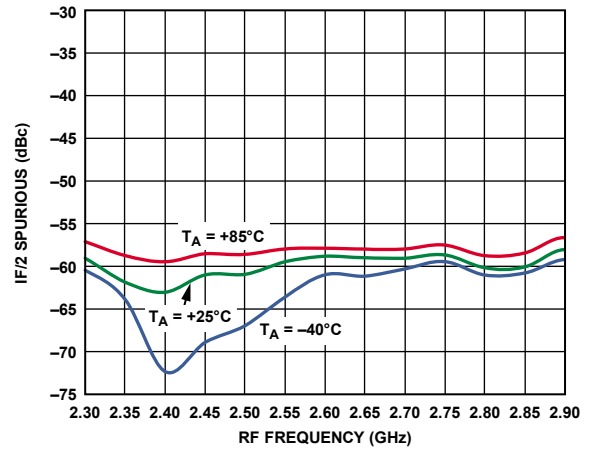


Figure 21. IF/2 Spurious vs. RF Frequency

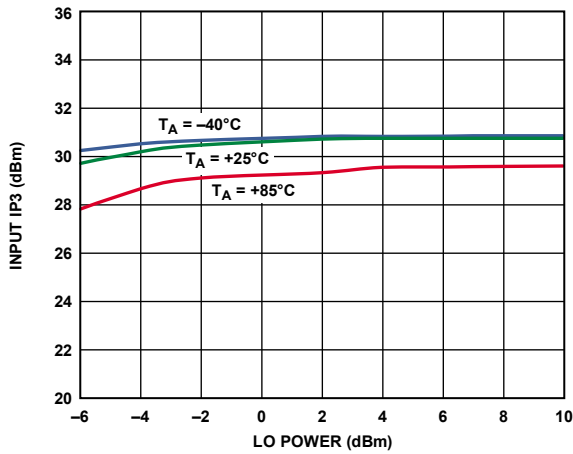


Figure 19. Input IP3 vs. LO Power

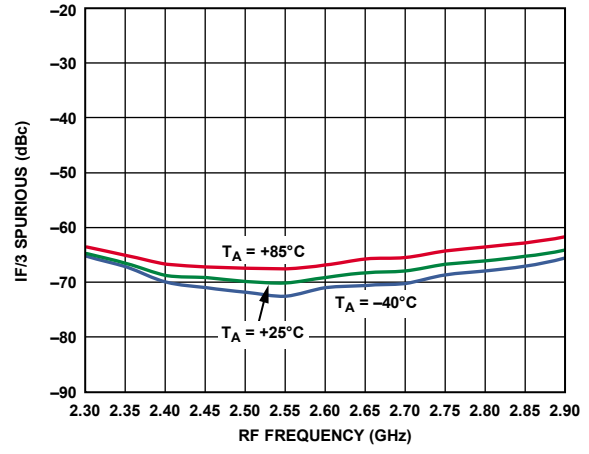


Figure 22. IF/3 Spurious vs. RF Frequency

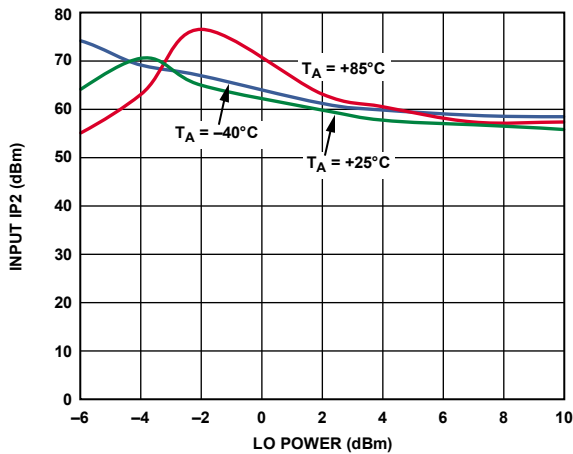


Figure 20. Input IP2 vs. LO Power

08914-018

08914-021

08914-019

08914-022

08914-020

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $V_{GS0} = V_{GS1} = 0\text{ V}$, and $Z_O = 50\ \Omega$, unless otherwise noted.

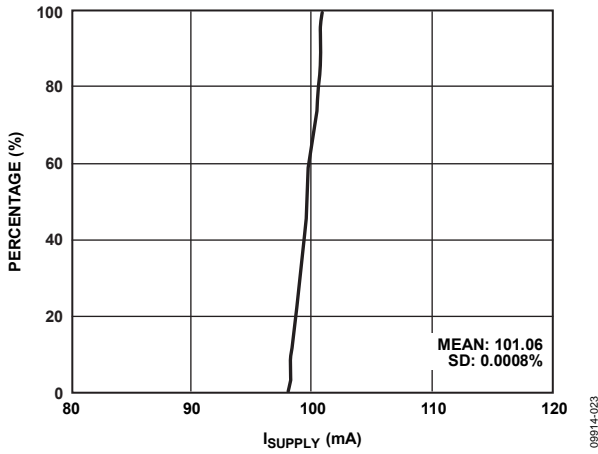


Figure 23. Supply Current Distribution

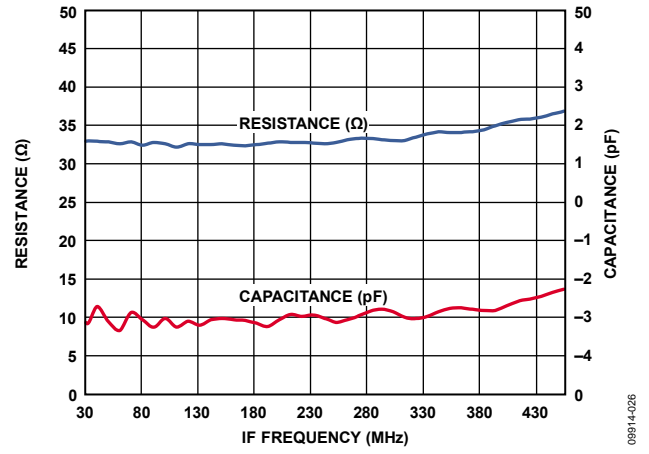


Figure 26. IF Output Impedance (R Parallel, C Equivalent)

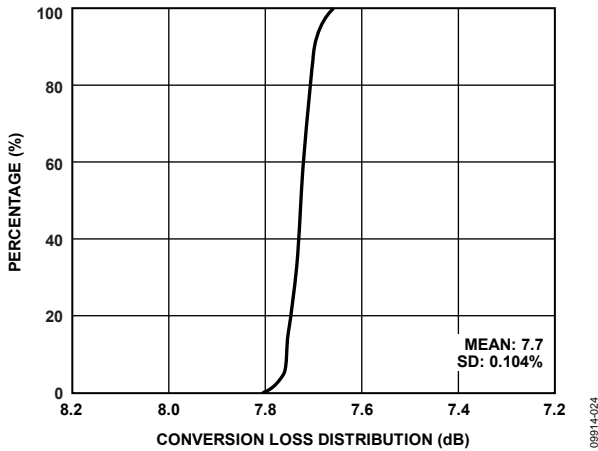


Figure 24. Conversion Loss Distribution

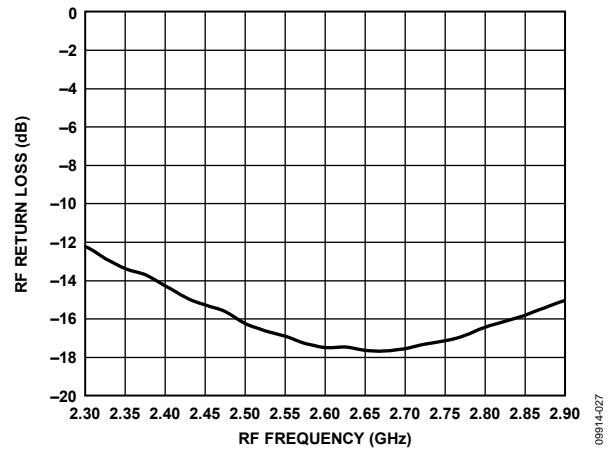


Figure 27. RF Port Return Loss, Fixed IF

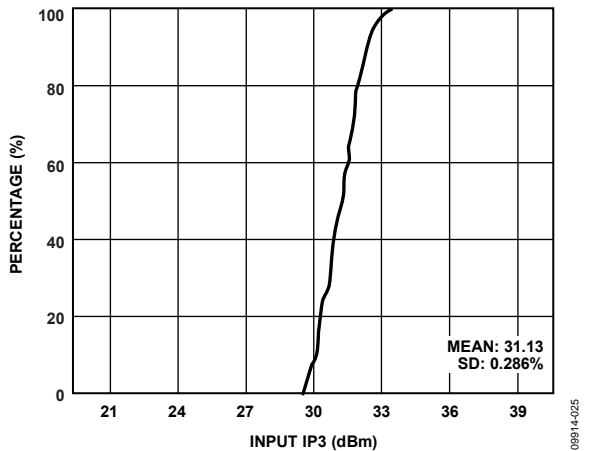


Figure 25. Input IP3 Distribution

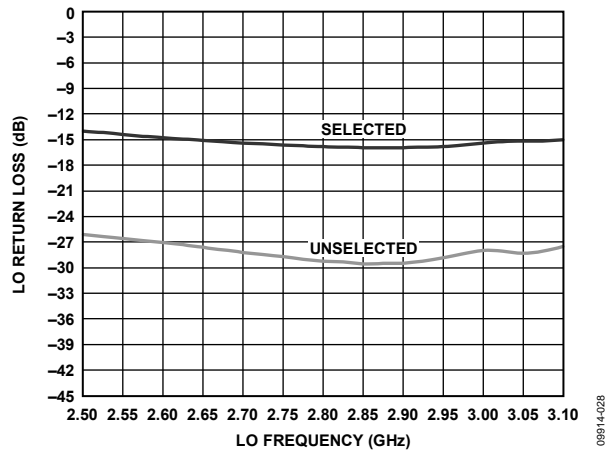


Figure 28. LO Return Loss, Selected and Unselected

ADL5363

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $V_{GS0} = V_{GS1} = 0\text{ V}$, and $Z_O = 50\ \Omega$, unless otherwise noted.

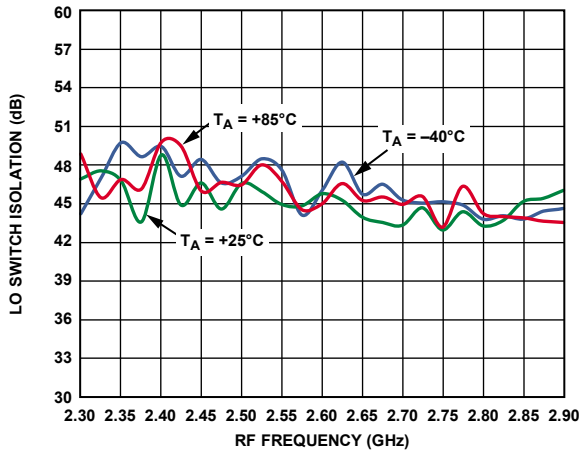


Figure 29. LO Switch Isolation vs. RF Frequency

09914-029

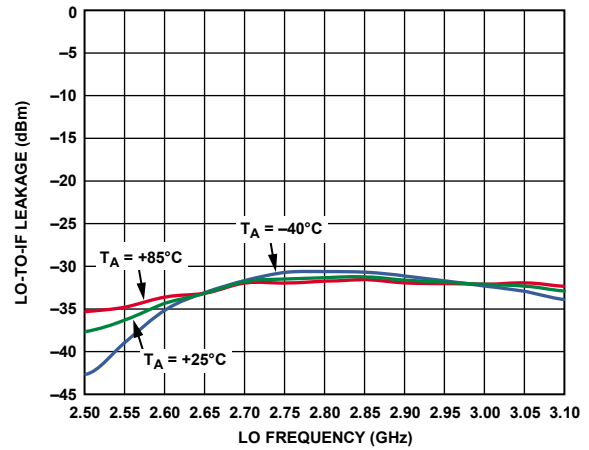


Figure 32. LO-to-RF Leakage vs. LO Frequency

09914-032

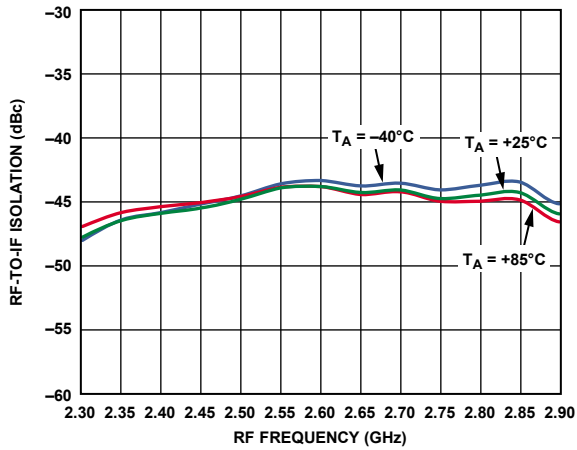


Figure 30. RF-to-IF Isolation vs. RF Frequency

09914-030

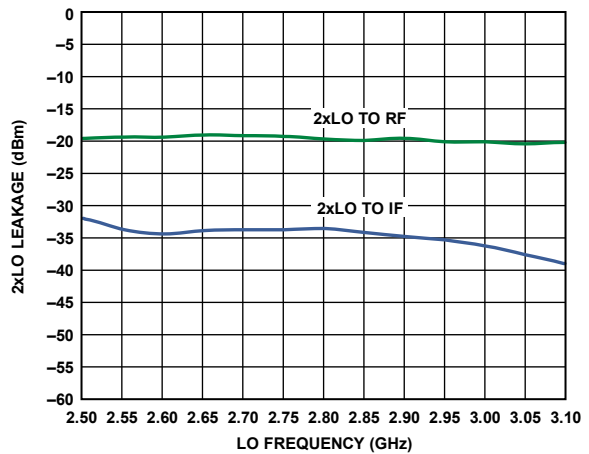


Figure 33. 2xLO Leakage vs. LO Frequency

09914-033

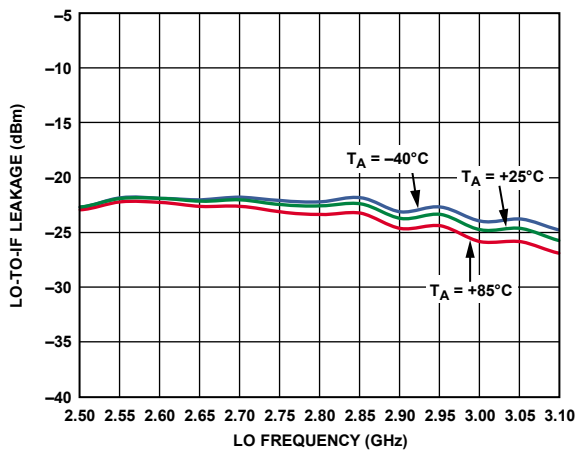


Figure 31. LO-to-IF Leakage vs. LO Frequency

09914-031

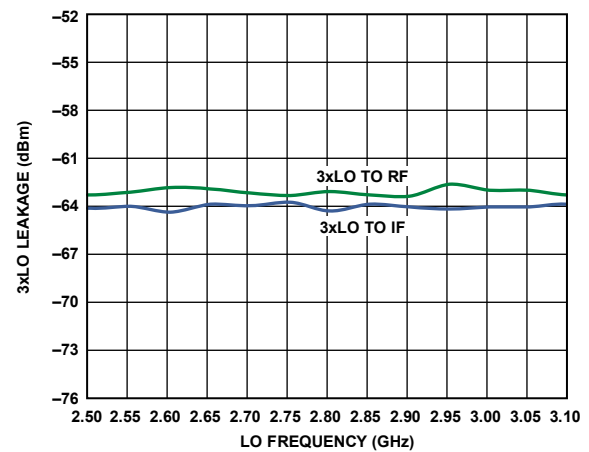


Figure 34. 3xLO Leakage vs. LO Frequency

09914-034

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $V_{GS0} = V_{GS1} = 0\text{ V}$, and $Z_O = 50\ \Omega$, unless otherwise noted.

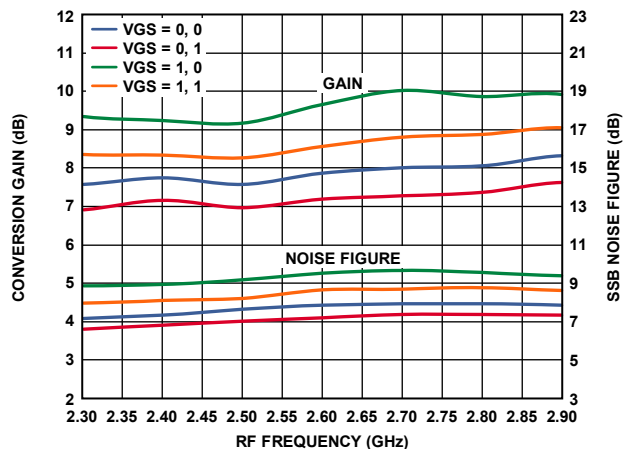


Figure 35. Power Conversion Loss and SSB Noise Figure vs. RF Frequency

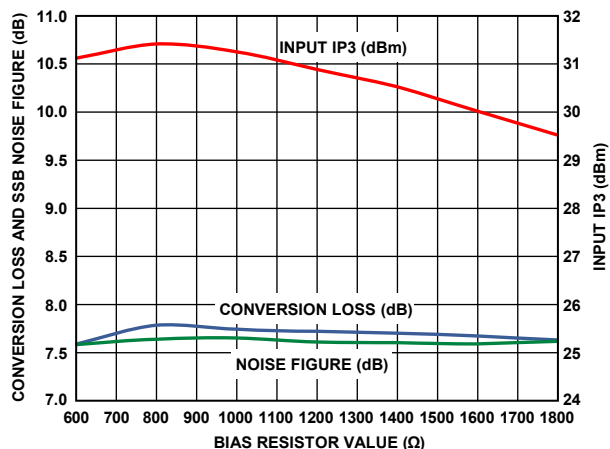


Figure 37. Power Conversion Loss, SSB Noise Figure, and Input IP3 vs. IF Bias Resistor Value

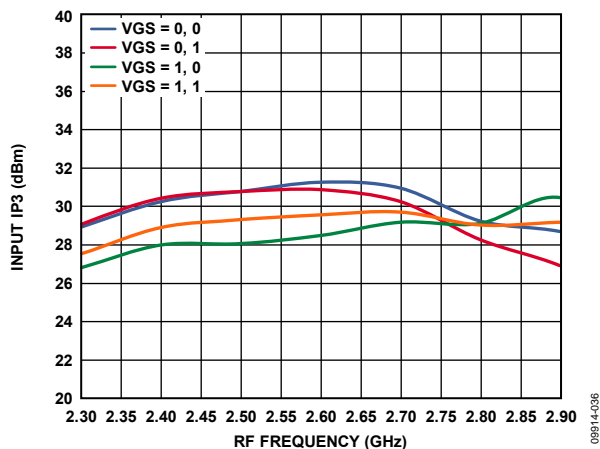


Figure 36. Input IP3 vs. RF Frequency

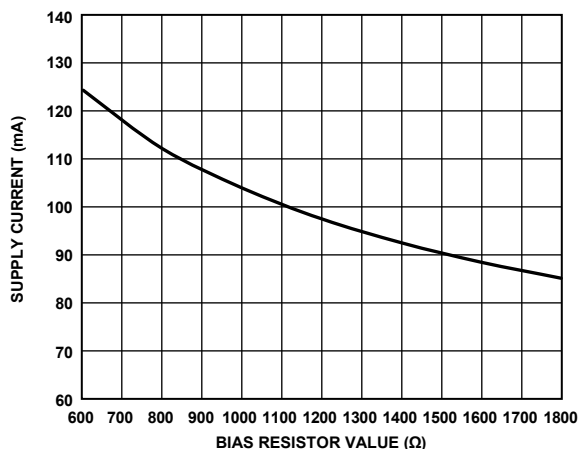


Figure 38. Supply Current vs. Bias Resistor Value

3.3 V PERFORMANCE

$V_S = 3.3\text{ V}$, $I_S = 60\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, $V_{GS0} = V_{GS1} = 0\text{ V}$, and $Z_O = 50\ \Omega$, unless otherwise noted.

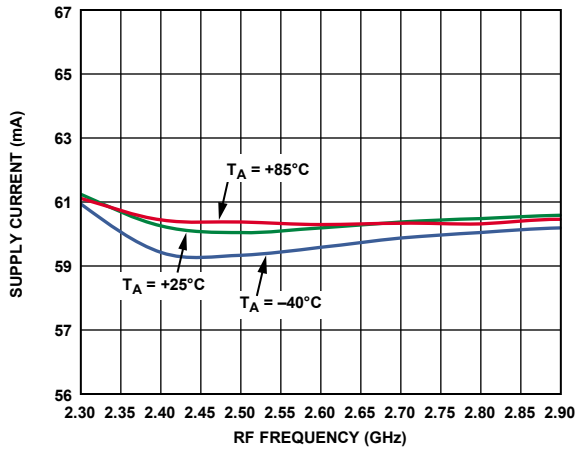


Figure 39. Supply Current vs. RF Frequency at 3.3 V

09914-039

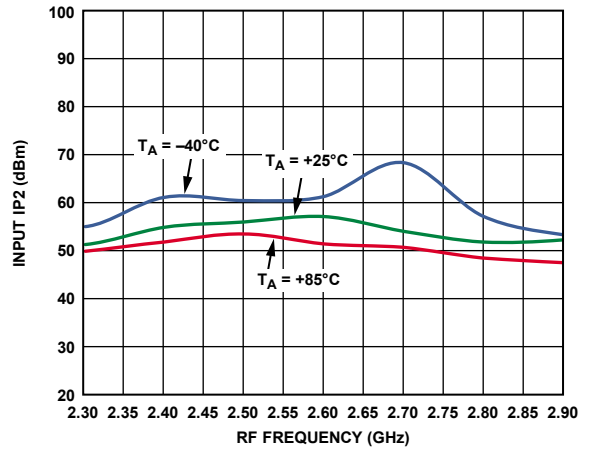


Figure 42. Input IP2 vs. RF Frequency at 3.3 V

09914-042

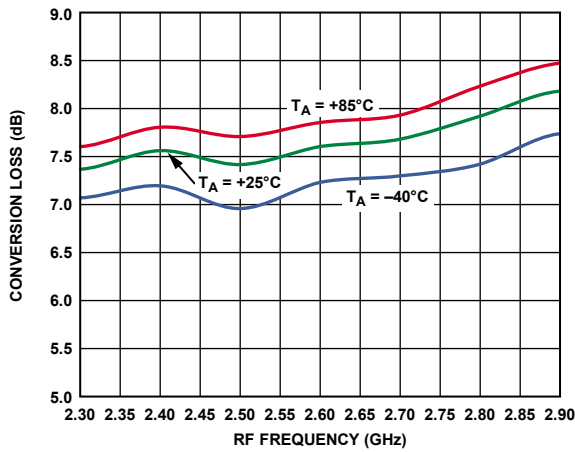


Figure 40. Power Conversion Loss vs. RF Frequency at 3.3 V

09914-040

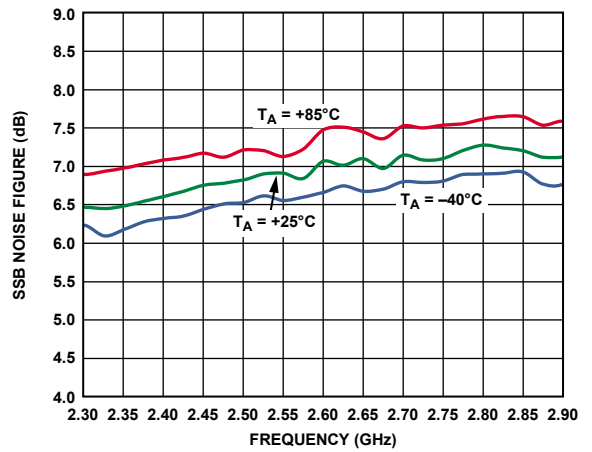


Figure 43. SSB Noise Figure vs. RF Frequency at 3.3 V

09914-043

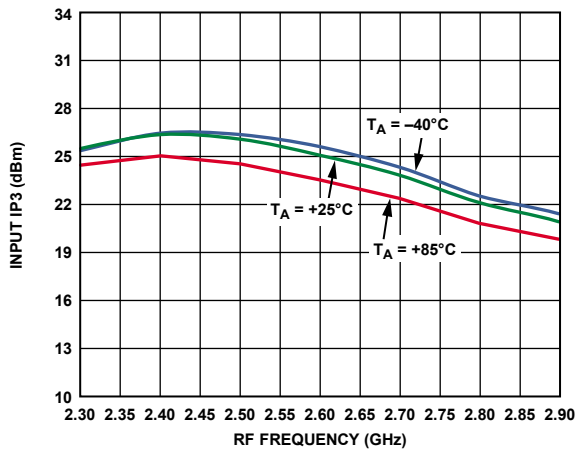


Figure 41. Input IP3 vs. RF Frequency at 3.3 V

09914-041

UPCONVERSION

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, VGS0 = VGS1 = 0 V, and $Z_O = 50\ \Omega$, unless otherwise noted.

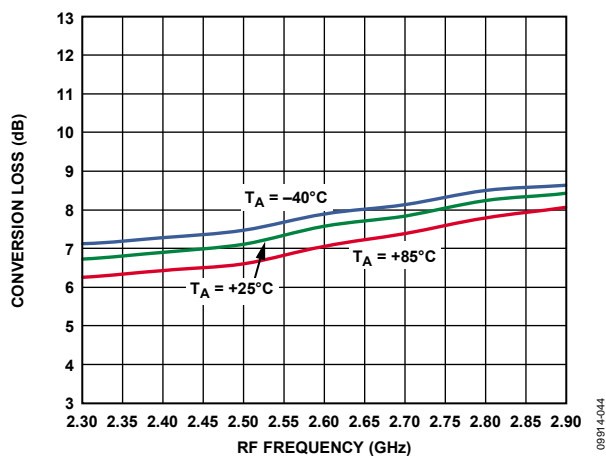


Figure 44. Power Conversion Loss vs. RF Frequency, $V_S = 5\text{ V}$, Upconversion

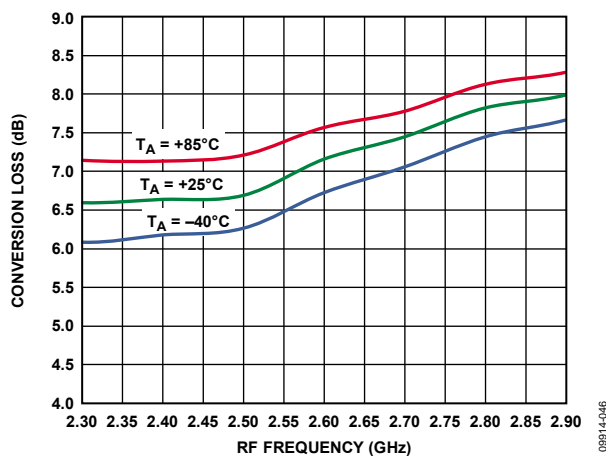


Figure 46. Power Conversion Loss vs. RF Frequency at 3.3 V, Upconversion

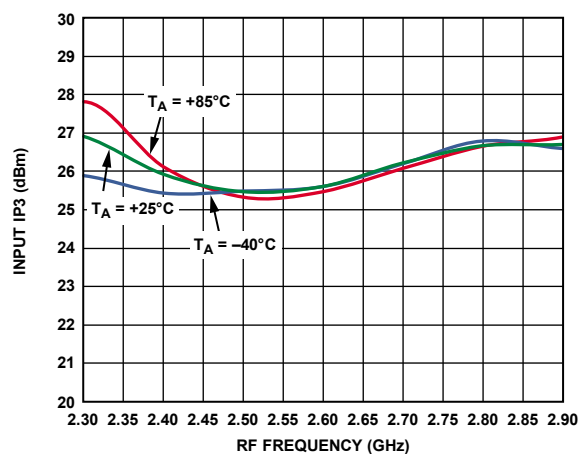


Figure 45. Input IP3 vs. RF Frequency, $V_S = 5\text{ V}$, Upconversion

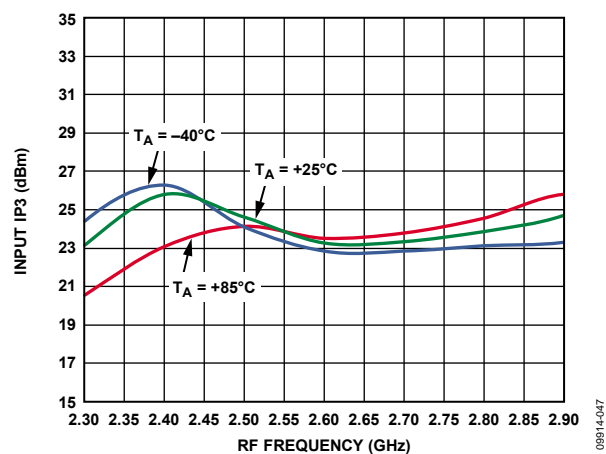


Figure 47. Input IP3 vs. RF Frequency at 3.3 V, Upconversion

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SPURIOUS PERFORMANCE

$(N \times f_{RF}) - (M \times f_{LO})$ spur measurements were made using the standard evaluation board. Mixer spurious products are measured in dBc from the IF output power level. Data was measured only for frequencies less than 6 GHz. Typical noise floor of the measurement system = -100 dBm.

5 V Performance

$V_S = 5\text{ V}$, $I_S = 100\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, RF power = 0 dBm, VGS0 = VGS1 = 0 V, and $Z_O = 50\ \Omega$, unless otherwise noted.

		M															
		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
N	0		-10.9	-28.3	-44.5												
	1	-42.2	0.0	-49.3	-31.2	-49.8											
	2	-75.8	-76.5	-64.6	-78.4	-78.5	-94.7										
	3	<-100	-83.0	<-100	-73.5	-90.9	-89.8	<-100									
	4		<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100							
	5				<-100	<-100	<-100	<-100	<-100	<-100	<-100						
	6					<-100	<-100	<-100	<-100	<-100	<-100	<-100					
	7						<-100	<-100	<-100	<-100	<-100	<-100	<-100				
	8							<-100	<-100	<-100	<-100	<-100	<-100	<-100			
	9								<-100	<-100	<-100	<-100	<-100	<-100	<-100		
	10									<-100	<-100	<-100	<-100	<-100	<-100	<-100	
	11										<-100	<-100	<-100	<-100	<-100	<-100	<-100
	12											<-100	<-100	<-100	<-100	<-100	<-100
	13													<-100	<-100	<-100	<-100
	14														<-100	<-100	<-100
	15															<-100	<-100

3.3 V Performance

$V_S = 3.3\text{ V}$, $I_S = 56\text{ mA}$, $T_A = 25^\circ\text{C}$, $f_{RF} = 2535\text{ MHz}$, $f_{LO} = 2738\text{ MHz}$, LO power = 0 dBm, RF power = 0 dBm, R9 = 226 Ω , VGS0 = VGS1 = 0 V, and $Z_O = 50\ \Omega$, unless otherwise noted.

		M															
		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
N	0		-16.9	-35.1	-61.4												
	1	-41.9	0.0	-49.1	-30.4	-52.6											
	2	-72.3	-80.3	-62.7	-68.5	-71.9	<-100										
	3	-94.6	-71.6	<-100	-61.2	-92.7	-75.1	<-100									
	4		<-100	<-100	<-100	<-100	<-100	<-100	<-100	<-100							
	5				<-100	<-100	<-100	<-100	<-100	<-100	<-100						
	6					<-100	<-100	<-100	<-100	<-100	<-100	<-100					
	7						<-100	<-100	<-100	<-100	<-100	<-100	<-100				
	8							<-100	<-100	<-100	<-100	<-100	<-100	<-100			
	9								<-100	<-100	<-100	<-100	<-100	<-100	<-100		
	10									<-100	<-100	<-100	<-100	<-100	<-100	<-100	
	11										<-100	<-100	<-100	<-100	<-100	<-100	<-100
	12											<-100	<-100	<-100	<-100	<-100	<-100
	13													<-100	<-100	<-100	<-100
	14														<-100	<-100	<-100
	15																<-100

CIRCUIT DESCRIPTION

The ADL5363 consists of two primary components: the radio frequency (RF) subsystem and the local oscillator (LO) subsystem. The combination of design, process, and packaging technology allows the functions of these subsystems to be integrated into a single die, using mature packaging and interconnection technologies to provide a high performance, low cost design with excellent electrical, mechanical, and thermal properties. In addition, the need for external components is minimized, optimizing cost and size.

The RF subsystem consists of an integrated, low loss RF balun, passive MOSFET mixer, sum termination network.

The LO subsystem consists of an SPDT-terminated FET switch and a three-stage limiting LO amplifier. The purpose of the LO subsystem is to provide a large, fixed amplitude, balanced signal to drive the mixer independent of the level of the LO input.

A block diagram of the device is shown in Figure 48.

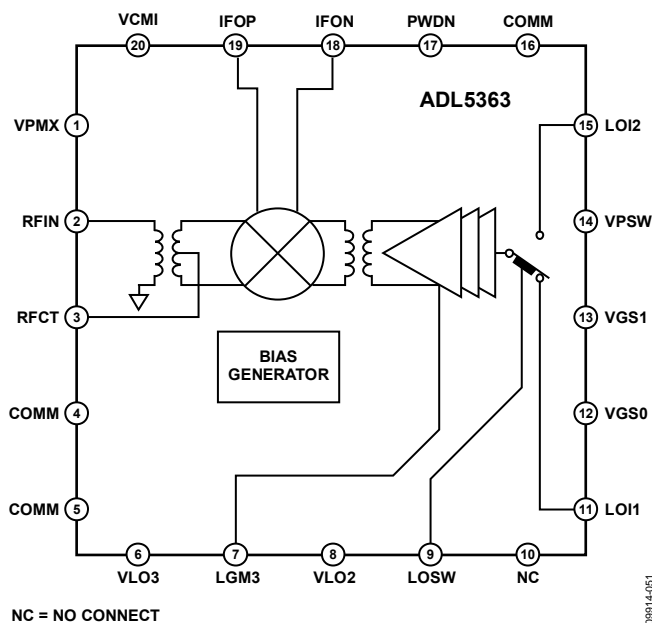


Figure 48. Simplified Schematic

RF SUBSYSTEM

The single-ended, 50 Ω RF input is internally transformed to a balanced signal using a low loss (<1 dB) unbalanced-to-balanced (balun) transformer. This transformer is made possible by an extremely low loss metal stack, which provides both excellent balance and dc isolation for the RF port. Although the port can be dc connected, it is recommended that a blocking capacitor be used to avoid running excessive dc current through the part. The RF balun can easily support an RF input frequency range of 2300 MHz to 2900 MHz.

The resulting balanced RF signal is applied to a passive mixer that commutates the RF input with the output of the LO subsystem. The passive mixer is essentially a balanced, low loss switch that adds minimum noise to the frequency translation. The only noise contribution from the mixer is due to the resistive loss of the switches, which is in the order of a few ohms.

As the mixer is inherently broadband and bidirectional, it is necessary to properly terminate all the idler ($M \times N$ product) frequencies generated by the mixing process. Terminating the mixer avoids the generation of unwanted intermodulation products and reduces the level of unwanted signals at the IF output. This termination is accomplished by the addition of a sum network between the IF output and the mixer.

The IP3 performance can be optimized by adjusting the supply current with an external resistor. Figure 37 and 38 illustrate how the bias resistor affects the performance with a 5 V supply. Additionally, dc current can be saved by increasing either or both resistors. It is permissible to reduce the dc supply voltage to as low as 3.3 V, further reducing the dissipated power of the part. (Note that no performance enhancement is obtained by reducing the value of these resistors and excessive dc power dissipation may result.)

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LO SUBSYSTEM

The ADL5363 has two LO inputs permitting multiple synthesizers to be rapidly switched with extremely short switching times (<40 ns) for frequency agile applications. The two inputs are applied to a high isolation SPDT switch that provides a constant input impedance, regardless of whether the port is selected, to avoid pulling the LO sources. This multiple section switch also ensures high isolation to the off input, minimizing any leakage from the unwanted LO input that may result in undesired IF responses.

The single-ended LO input is converted to a fixed amplitude differential signal using a multistage, limiting LO amplifier. This results in consistent performance over a range of LO input power. Optimum performance is achieved from -6 dBm to +10 dBm, but the circuit continues to function at considerably lower levels of LO input power.

The performance of this amplifier is critical in achieving a high intercept passive mixer without degrading the noise floor of the system. This is a critical requirement in an interferer rich environment, such as cellular infrastructure, where blocking

interferers can limit mixer performance. The bandwidth of the intermodulation performance is somewhat influenced by the current in the LO amplifier chain. For dc current sensitive applications, it is permissible to reduce the current in the LO amplifier by raising the value of the external bias control resistor. For dc current critical applications, the LO chain can operate with a supply voltage as low as 3.3 V, resulting in substantial dc power savings.

In addition, when operating with supply voltages below 3.6 V, the ADL5363 has a power-down mode that permits the dc current to drop to <200 μ A.

All of the logic inputs are designed to work with any logic family that provides a Logic 0 input level of less than 0.4 V and a Logic 1 input level that exceeds 1.4 V. All logic inputs are high impedance up to Logic 1 levels of 3.3 V. At levels exceeding 3.3 V, protection circuitry permits operation up to 5.5 V, although a small bias current is drawn.

All pins, including the RF pins, are ESD protected and have been tested up to a level of 1500 V HBM and 1250 V CDM.

APPLICATIONS INFORMATION

BASIC CONNECTIONS

The ADL5363 mixer is designed to downconvert radio frequencies (RF) primarily between 2300 MHz and 2900 MHz to lower intermediate frequencies (IF) between 30 MHz and 450 MHz. Figure 49 depicts the basic connections of the mixer. To prevent nonzero dc voltages from damaging the RF balun or LO input circuit, ac-couple the RF and LO input ports. The RFIN matching network consists of a series 1.5 pF capacitor and a shunt 12 nH inductor to provide the optimized RF input return loss for the desired frequency band.

IF PORT

The real part of the output impedance is approximately 50 Ω , as seen in Figure 26, which matches many commonly used SAW filters without the need for a transformer. This results in a voltage conversion loss that is approximately the same as the power conversion loss, as shown in Table 3.

BIAS RESISTOR SELECTION

An external resistor, $R_{BIAS\ LO}$, is used to adjust the bias current of the integrated amplifiers at the LO terminals. It is necessary to have a sufficient amount of current to bias the internal LO amplifier to optimize dc current vs. optimum IIP3 performance. Figure 37 and Figure 38 provide the reference for the bias resistor selection when lower power consumption is considered at the expense of conversion gain and IP3 performance.

MIXER VGS CONTROL DAC

The ADL5363 features two logic control pins, VGS0 (Pin 12) and VGS1 (Pin 13), that allow programmability for internal gate-to-source voltages for optimizing mixer performance over desired frequency bands. The evaluation board defaults both VGS0 and VGS1 to ground.

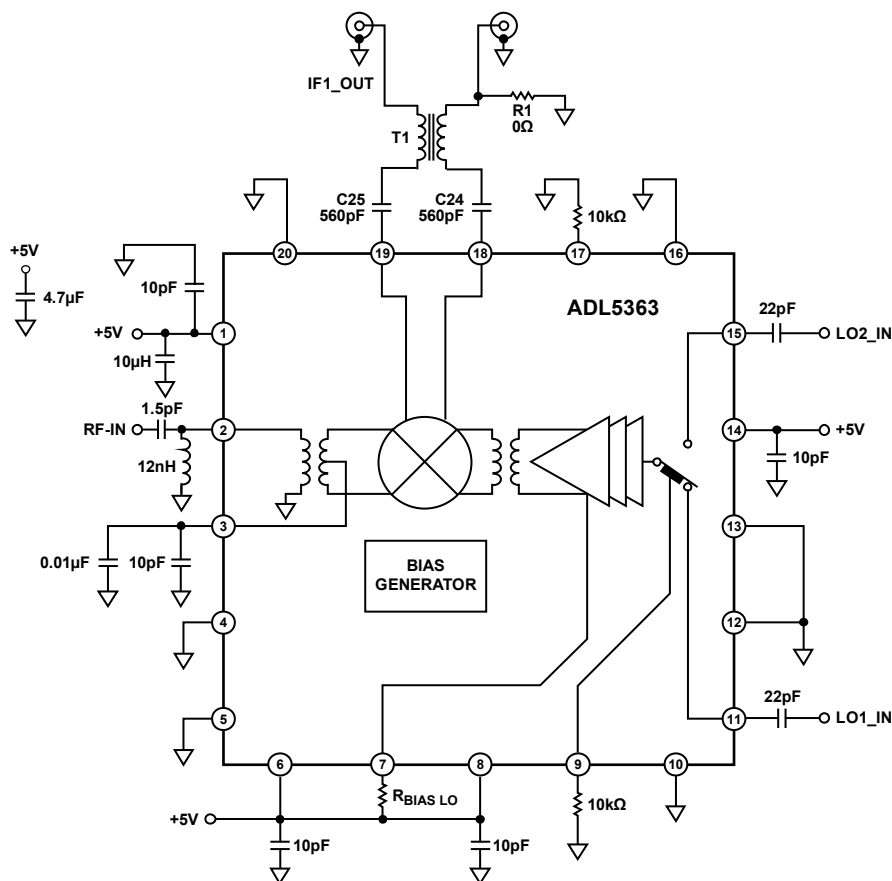


Figure 49. Typical Application Circuit

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EVALUATION BOARD

An evaluation board is available for the family of double balanced mixers. The standard evaluation board schematic is shown in Figure 50. The evaluation board is fabricated using Rogers® RO3003 material. Table 7 describes the various configuration options of the evaluation board. Evaluation board layout is shown in Figure 51 to Figure 54.

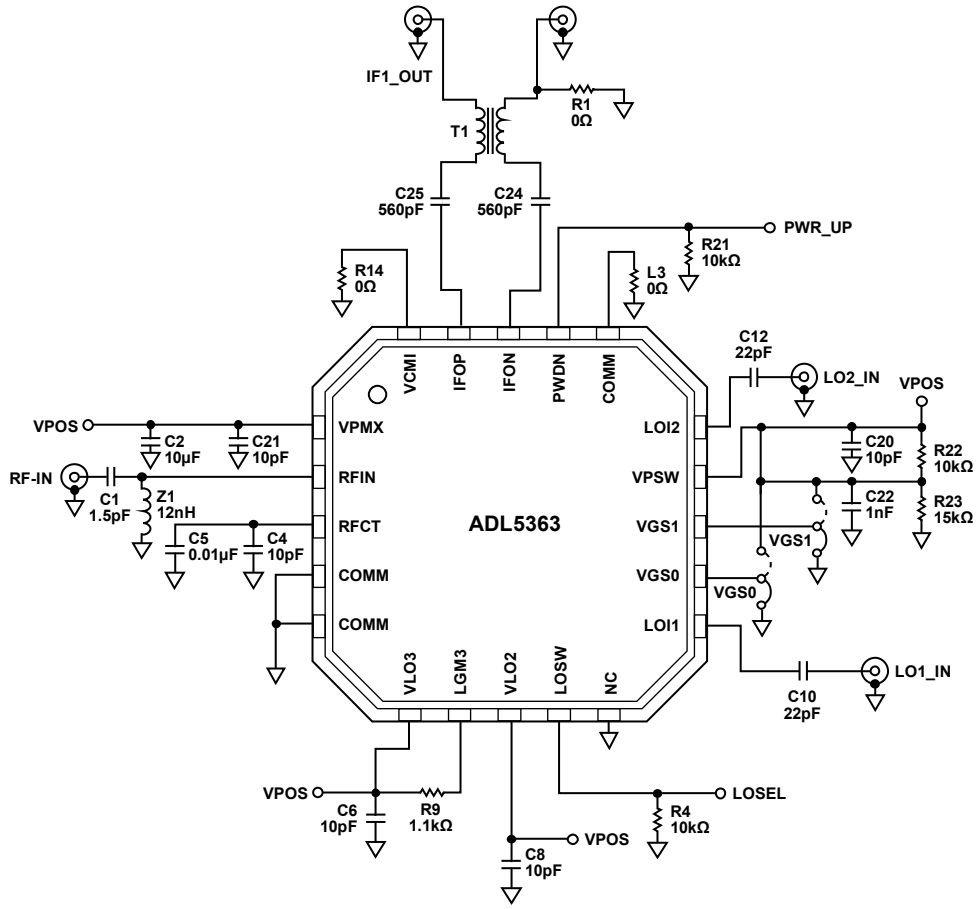


Figure 50. Evaluation Board Schematic

06914-053

Table 7. Evaluation Board Configuration

Components	Function	Description	Default Conditions
C2, C6, C8, C20, C21	Power supply decoupling	Power Supply Decoupling. Nominal supply decoupling consists of a 10 μ F capacitor to ground in parallel with a 10 pF capacitor to ground positioned as close to the device as possible.	C2 = 10 μ F (size 0603), C6, C8, C20, C21 = 10 pF (size 0402)
C1, C4, C5, Z1	RF input interface	RF Input Interface. The input channels are ac-coupled through C1. C4 and C5 provide bypassing for the center taps of the RF input baluns.	C1 = 1.5 pF (size 0402), C4 = 10 pF (size 0402), C5 = 0.01 μ F (size 0402) Z1 = 12 nH (size 0402)
T1, R1, C24, C25	IF output interface	IF Output Interface. T1 is a 1:1 impedance transformer used to provide a single-ended IF output interface. Remove R1 for balanced output operation. C24 and C25 are used to block the dc bias at the IF ports.	T1 = TC1-1-13M+ (Mini-Circuits), R1 = 0 Ω (size 0402), C24, C25 = 560 pF (size 0402)
C10, C12, R4	LO interface	LO Interface. C10 and C12 provide ac coupling for the LO1_IN and LO2_IN local oscillator inputs. LOSEL selects the appropriate LO input for both mixer cores. R4 provides a pull-down to ensure that LO1_IN is enabled when the LOSEL test point is logic low. LO2_IN is enabled when LOSEL is pulled to logic high.	C10, C12 = 22 pF (size 0402), R4 = 10 k Ω (size 0402)
R21	PWDN interface	PWDN Interface. R21 pulls the PWDN logic low and enables the device. The PWR_UP test point allows the PWDN interface to be exercised using the an external logic generator. Grounding the PWDN pin for nominal operation is allowed. Using the PWDN pin when supply voltages exceed 3.3 V is not allowed.	R21 = 10 k Ω (size 0402)
C22, L3, R9, R14, R22, R23, VGS0, VGS1	Bias control	Bias Control. R22 and R23 form a voltage divider to provide 3 V for logic control, bypassed to ground through C22. VGS0 and VGS1 jumpers provide programmability at the VGS0 and VGS1 pins. It is recommended to pull these two pins to ground for nominal operation. R9 sets the bias point for the internal LO buffers.	C22 = 1 nF (size 0402), L3 = 0 Ω (size 0603), R9 = 1.1 k Ω (size 0402), R14 = 0 Ω (size 0402), R22 = 10 k Ω (size 0402), R23 = 15 k Ω (size 0402), VGS0 = VGS1 = 3-pin shunt

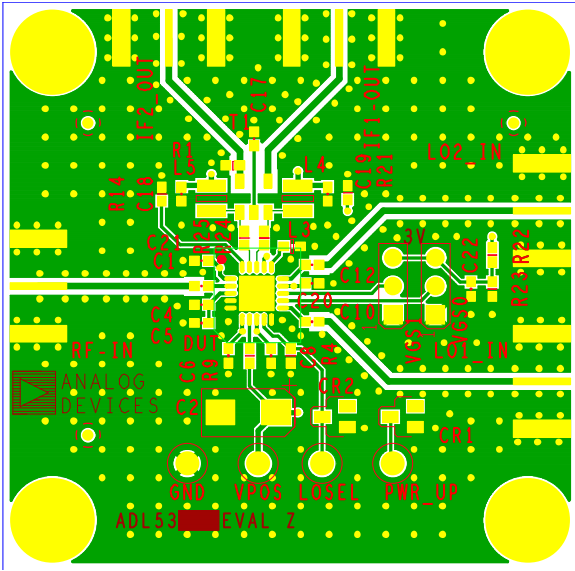


Figure 51. Evaluation Board Top Layer

09914-152

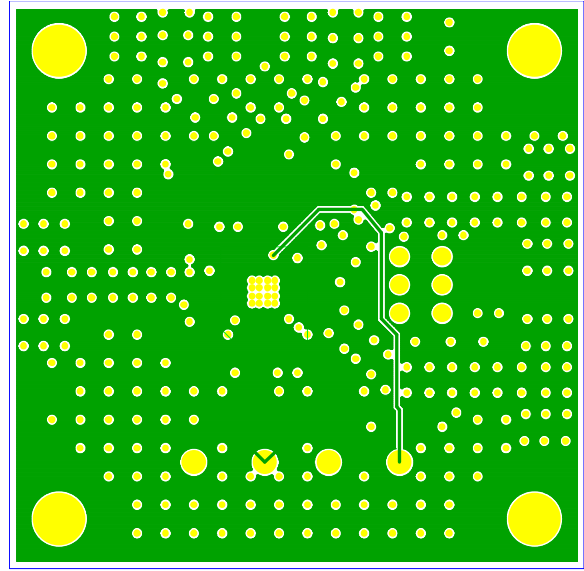


Figure 53. Evaluation Board Power Plane, Internal Layer 2

09914-154

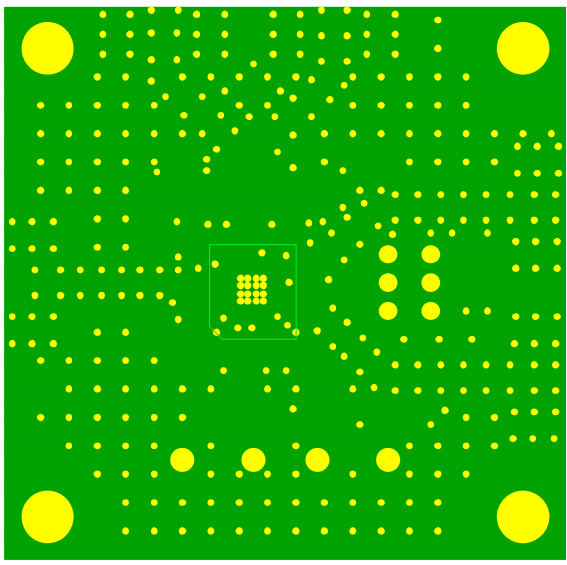


Figure 52. Evaluation Board Ground Plane, Internal Layer 1

09914-153

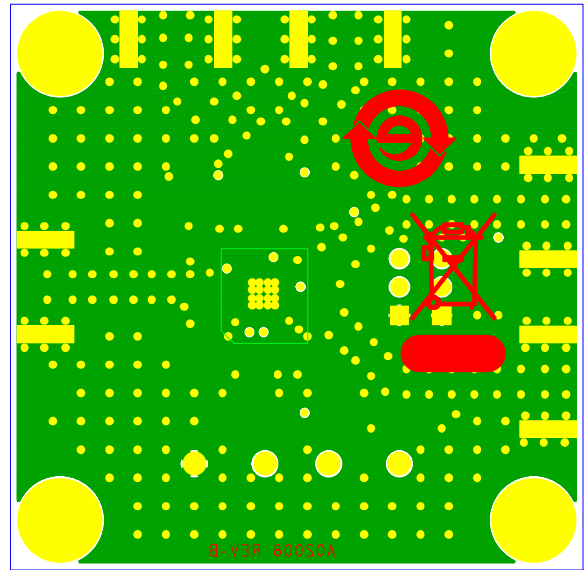
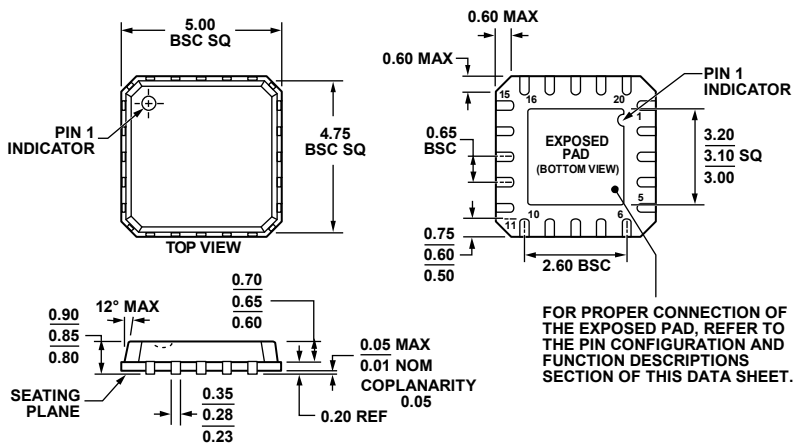


Figure 54. Evaluation Board Bottom Layer

09914-155

OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MO-220-VHHC

Figure 55. 20-Lead Lead Frame Chip Scale Package [LFCSP_VQ]
 5 mm × 5 mm Body, Very Thin Quad
 (CP-20-5)
 Dimensions shown in millimeters

044209-B

ORDERING GUIDE

Model ¹	Temperature Range	Package Description	Package Option	Ordering Quantity
ADL5363ACPZ-R7	-40°C to +85°C	20-Lead Lead Frame Chip Scale Package [LFCSP_VQ] 7" Tape and Reel	CP-20-5	1,500
ADL5363-EVALZ		Evaluation Board		1

¹ Z = RoHS Compliant Part.

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NOTES