MCP6V27

620 µA, 2 MHz Auto-Zeroed Op Amps

Features

- High DC Precision:
  - V_{OS} Drift: ±50 nV/°C (maximum)
  - V_{OS}: ±2 µV (maximum)
  - A_{OL}: 125 dB (minimum)
  - PSRR: 125 dB (minimum)
  - CMRR: 120 dB (minimum)
  - E_{ni}: 1.0 μV_{P-P} (typical), f = 0.1 Hz to 10 Hz
  - E_{ni}: 0.32 μV_{P-P} (typical), f = 0.01 Hz to 1 Hz
- Low Power and Supply Voltages:
  - I_Q: 620 µA/amplifier (typical)
  - Wide Supply Voltage Range: 2.3V to 5.5V
- Easy to Use:
  - Rail-to-Rail Input/Output
  - Gain Bandwidth Product: 2 MHz (typical)
  - Unity Gain Stable
  - Available in Dual
- Extended Temperature Range: -40°C to +125°C

Typical Applications

- Portable Instrumentation
- Sensor Conditioning
- Temperature Measurement
- DC Offset Correction
- Medical Instrumentation

Design Aids

- SPICE Macro Models
- FilterLab® Software
- Microchip Advanced Part Selector (MAPS)
- Analog Demonstration and Evaluation Boards
- Application Notes

Related Parts

Parts with lower power, lower bandwidth and higher noise:

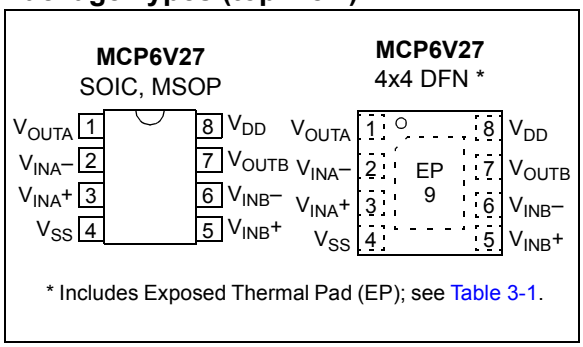
- MCP6V01/2/3: Spread clock
- MCP6V06/7/8: Non-spread clock

Description

The Microchip Technology Inc. MCP6V27 dual operational amplifier has input offset voltage correction for very low offset and offset drift. This device has a wide gain bandwidth product (2 MHz, typical) and strongly rejects switching noise. It is unity gain stable, has no 1/f noise, and has good PSRR and CMRR. This product operates with a single supply voltage as low as 2.3V, while drawing 620 µA/amplifier (typical) of quiescent current.

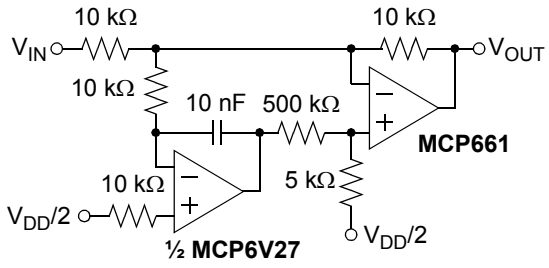
The Microchip Technology Inc. MCP6V27 op amp is offered as a dual. It is designed in an advanced CMOS process.

Package Types (top view)



* Includes Exposed Thermal Pad (EP); see Table 3-1.

Typical Application Circuit



Offset Voltage Correction for Power Driver

NOTES:

1.0 ELECTRICAL CHARACTERISTICS

1.1 Absolute Maximum Ratings †

$V_{DD} - V_{SS}$ 6.5V
Current at Input Pins †† .....±2 mA
Analog Inputs (V_{IN}+ and V_{IN}–) †† ..... V_{SS} – 1.0V to V_{DD}+1.0V
All other Inputs and Outputs ..... V_{SS} – 0.3V to V_{DD}+0.3V
Difference Input voltage ..... $|V_{DD} - V_{SS}|$
Output Short Circuit Current .....Continuous
Current at Output and Supply Pins .....±30 mA
Storage Temperature .....-65°C to +150°C
Max. Junction Temperature .....+150°C
ESD protection on all pins (HBM, CDM, MM) ≥ 4 kV,1.5 kV, 300V

† Notice: Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only and functional operation of the device at those or any other conditions above those indicated in the operational listings of this specification is not implied. Exposure to maximum rating conditions for extended periods may affect device reliability.

†† See **Section 4.2.1, Rail-to-Rail Inputs**.

1.2 Specifications

TABLE 1-1: DC ELECTRICAL SPECIFICATIONS

Electrical Characteristics: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to +5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2 and R_L = 10 kΩ to V_L (refer to Figure 1-4 and Figure 1-5).						
Parameters	**Sym**	**Min**	**Typ**	**Max**	**Units**	**Conditions**
Input Offset						
Input Offset Voltage	V_{OS}	-2	—	+2	µV	T_A = +25°C **(Note 1)**
Input Offset Voltage Drift with Temperature (linear Temp. Co.)	TC_1	-50	—	+50	nV/°C	T_A = -40 to +125°C **(Note 1)**
Input Offset Voltage Quadratic Temperature Coefficient	TC_2	—	±0.2	—	nV/°C^2	T_A = -40 to +125°C
Power Supply Rejection	PSRR	125	142	—	dB	**(Note 1)**
Input Bias Current and Impedance						
Input Bias Current	I_B	—	+7	—	pA	
Input Bias Current across Temperature	I_B	—	+110	—	pA	T_A = +85°C
	I_B	—	+1.2	+5	nA	T_A = +125°C
Input Offset Current	I_{OS}	—	±70	—	pA	
Input Offset Current across Temperature	I_{OS}	—	±50	—	pA	T_A = +85°C
	I_{OS}	—	±60	—	pA	T_A = +125°C
Common Mode Input Impedance	Z_{CM}	—	10^{13}||12	—	Ω||pF	
Differential Input Impedance	Z_{DIFF}	—	10^{13}||12	—	Ω||pF	

Note 1: Set by design and characterization. Due to thermal junction and other effects in the production environment, these parts can only be screened in production (except TC_1; see **Appendix B: "Offset Related Test Screens"**).

2: Figure 2-18 shows how V_{CML} and V_{CMH} changed across temperature for the first production lot.

TABLE 1-1: DC ELECTRICAL SPECIFICATIONS (CONTINUED)

Electrical Characteristics: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to +5.5V, V_{SS} = GND, $V_{CM} = V_{DD}/3$, $V_{OUT} = V_{DD}/2$, $V_L = V_{DD}/2$ and R_L = 10 kΩ to V_L (refer to Figure 1-4 and Figure 1-5).

Parameters	Sym	Min	Typ	Max	Units	Conditions
Common Mode						
Common-Mode Input Voltage Range Low	V_{CML}	—	—	$V_{SS} - 0.15$	V	**(Note 2)**
Common-Mode Input Voltage Range High	V_{CMH}	$V_{DD} + 0.2$	—	—	V	**(Note 2)**
Common-Mode Rejection	CMRR	120	136	—	dB	V_{DD} = 2.3V, V_{CM} = -0.15V to 2.5V **(Note 1, Note 2)**
	CMRR	125	142	—	dB	V_{DD} = 5.5V, V_{CM} = -0.15V to 5.7V **(Note 1, Note 2)**
Open-Loop Gain						
DC Open-Loop Gain (large signal)	A_{OL}	125	147	—	dB	V_{DD} = 2.3V, V_{OUT} = 0.2V to 2.1V **(Note 1)**
	A_{OL}	133	155	—	dB	V_{DD} = 5.5V, V_{OUT} = 0.2V to 5.3V **(Note 1)**
Output						
Minimum Output Voltage Swing	V_{OL}	—	V_{SS} + 5	$V_{SS} + 15$	mV	G = +2, 0.5V input overdrive
Maximum Output Voltage Swing	V_{OH}	$V_{DD} - 15$	$V_{DD} - 5$	—	mV	G = +2, 0.5V input overdrive
Output Short Circuit Current	I_{SC}	—	±12	—	mA	V_{DD} = 2.3V
	I_{SC}	—	±22	—	mA	V_{DD} = 5.5V
Power Supply						
Supply Voltage	V_{DD}	2.3	—	5.5	V	
Quiescent Current per amplifier	I_Q	450	620	800	µA	I_O = 0
POR Trip Voltage	V_{POR}	1.15	—	1.65	V	

Note 1: Set by design and characterization. Due to thermal junction and other effects in the production environment, these parts can only be screened in production (except TC_1; see **Appendix B: "Offset Related Test Screens"**).

2: Figure 2-18 shows how V_{CML} and V_{CMH} changed across temperature for the first production lot.

TABLE 1-2: AC ELECTRICAL SPECIFICATIONS

Electrical Characteristics: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to +5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF (refer to Figure 1-4 and Figure 1-5).						
Parameters	**Sym**	**Min**	**Typ**	**Max**	**Units**	**Conditions**
Amplifier AC Response						
Gain Bandwidth Product	GBWP	—	2.0	—	MHz	
Slew Rate	SR	—	1.0	—	V/µs	
Phase Margin	PM	—	65	—	°	G = +1
Amplifier Noise Response						
Input Noise Voltage	E_{ni}	—	0.32	—	μV_{P-P}	f = 0.01 Hz to 1 Hz
	E_{ni}	—	1.0	—	μV_{P-P}	f = 0.1 Hz to 10 Hz
Input Noise Voltage Density	e_{ni}	—	50	—	nV/√Hz	f < 5 kHz
	e_{ni}	—	29	—	nV/√Hz	f = 100 kHz
Input Noise Current Density	i_{ni}	—	0.6	—	fA/√Hz	
Amplifier Distortion (Note 1)						
Intermodulation Distortion (AC)	IMD	—	40	—	μV_{PK}	V_{CM} tone = 50 mV_{PK} at 1 kHz, G_N = 1
Amplifier Step Response						
Start Up Time	t_{STR}	—	75	—	µs	G = +1, V_{OS} within 50 µV of its final value **(Note 2)**
Offset Correction Settling Time	t_{STL}	—	150	—	µs	G = +1, V_{IN} step of 2V, V_{OS} within 50 µV of its final value
Output Overdrive Recovery Time	t_{ODR}	—	45	—	µs	G = -100, ±0.5V input overdrive to V_{DD}/2, V_{IN} 50% point to V_{OUT} 90% point **(Note 3)**

Note 1: These parameters were characterized using the circuit in Figure 1-6. In Figure 2-37 and Figure 2-38, there is an IMD tone at DC, a residual tone at 1 kHz, other IMD tones and clock tones.

2: High gains behave differently; see **Section 4.3.3, Offset at Power Up**.

3: t_{ODR} includes some uncertainty due to clock edge timing.

TABLE 1-3: TEMPERATURE SPECIFICATIONS

Electrical Characteristics: Unless otherwise indicated, all limits are specified for: V_{DD} = +2.3V to +5.5V, V_{SS} = GND.						
Parameters	**Sym**	**Min**	**Typ**	**Max**	**Units**	**Conditions**
Temperature Ranges						
Specified Temperature Range	T_A	-40	—	+125	°C	
Operating Temperature Range	T_A	-40	—	+125	°C	**(Note 1)**
Storage Temperature Range	T_A	-65	—	+150	°C	
Thermal Package Resistances						
Thermal Resistance, 8L-4x4 DFN	θ_{JA}	—	48	—	°C/W	**(Note 2)**
Thermal Resistance, 8L-MSOP	θ_{JA}	—	211	—	°C/W	
Thermal Resistance, 8L-SOIC	θ_{JA}	—	150	—	°C/W	

Note 1: Operation must not cause T_J to exceed Maximum Junction Temperature specification (+150°C).

2: Measured on a standard JC51-7, four layer printed circuit board with ground plane and vias.

1.3 Timing Diagrams

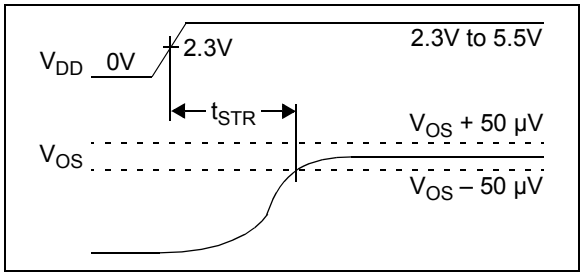


FIGURE 1-1: *Amplifier Start Up.*

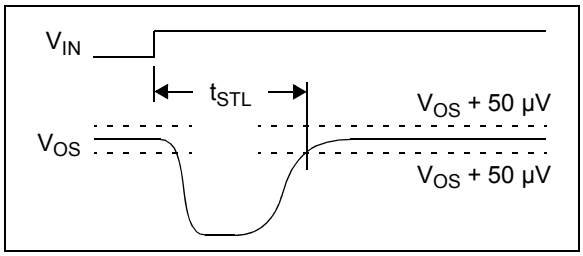


FIGURE 1-2: *Offset Correction Settling Time.*

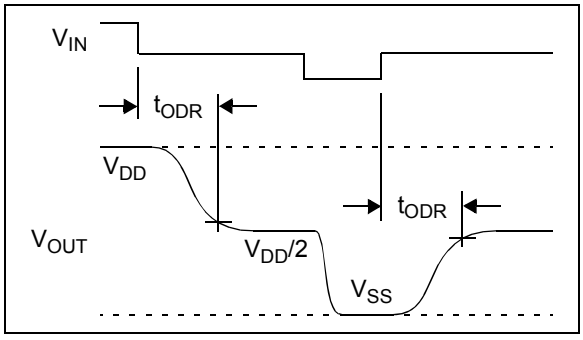


FIGURE 1-3: *Output Overdrive Recovery.*

1.4 Test Circuits

The circuits used for the DC and AC tests are shown in Figure 1-4 and Figure 1-5. Lay the bypass capacitors out as discussed in **Section 4.3.10, Supply Bypassing and Filtering**. R_N is equal to the parallel combination of R_F and R_G to minimize bias current effects.

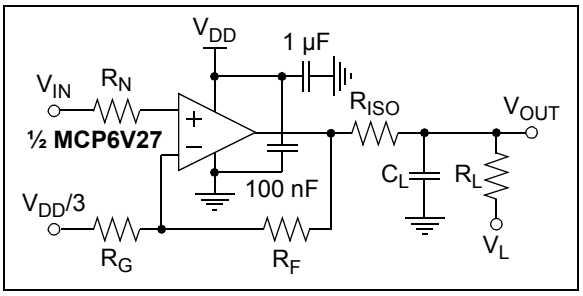


FIGURE 1-4: *AC and DC Test Circuit for Most Non-Inverting Gain Conditions.*

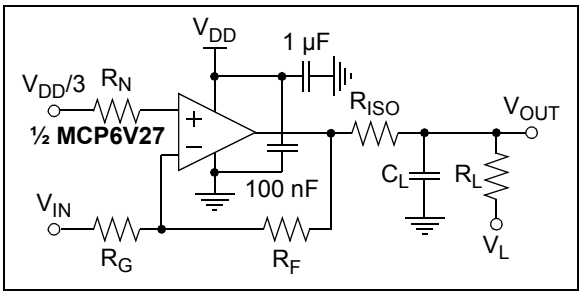


FIGURE 1-5: *AC and DC Test Circuit for Most Inverting Gain Conditions.*

The circuit in Figure 1-6 tests the op amp input's dynamic behavior (i.e., IMD, t_{STR}, t_{STL} and t_{ODR}). The potentiometer balances the resistor network (V_{OUT} should equal V_{REF} at DC). The op amp's common mode input voltage is $V_{CM} = V_{IN}/2$. The error at the input (V_{ERR}) appears at V_{OUT} with a noise gain of 10 V/V.

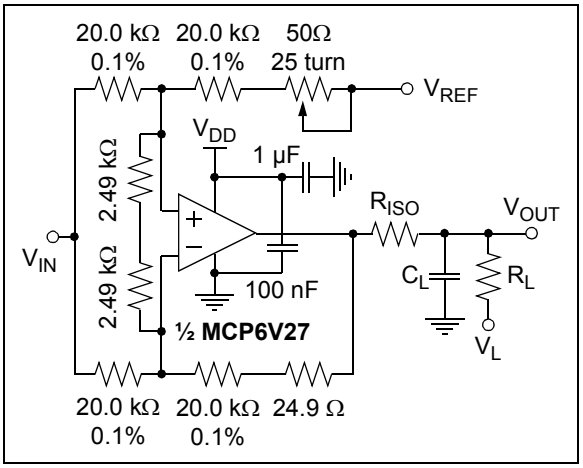


FIGURE 1-6: *Test Circuit for Dynamic Input Behavior.*

2.0 TYPICAL PERFORMANCE CURVES

Note: The graphs and tables provided following this note are a statistical summary based on a limited number of samples and are provided for informational purposes only. The performance characteristics listed herein are not tested or guaranteed. In some graphs or tables, the data presented may be outside the specified operating range (e.g., outside specified power supply range) and therefore outside the warranted range.

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

2.1 DC Input Precision

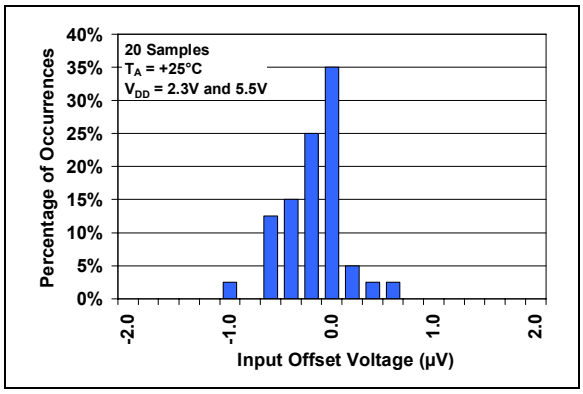


FIGURE 2-1: *Input Offset Voltage.*

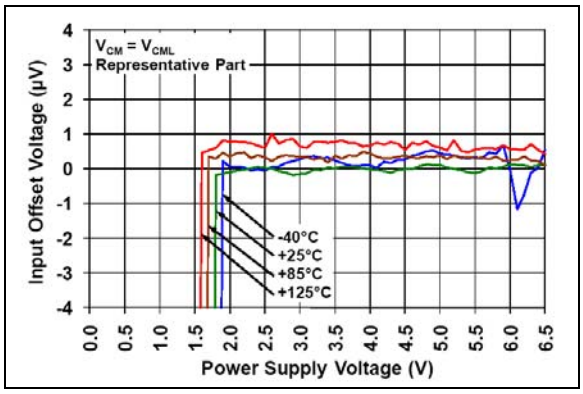


FIGURE 2-4: *Input Offset Voltage vs. Power Supply Voltage with V_{CM} = V_{CML}.*

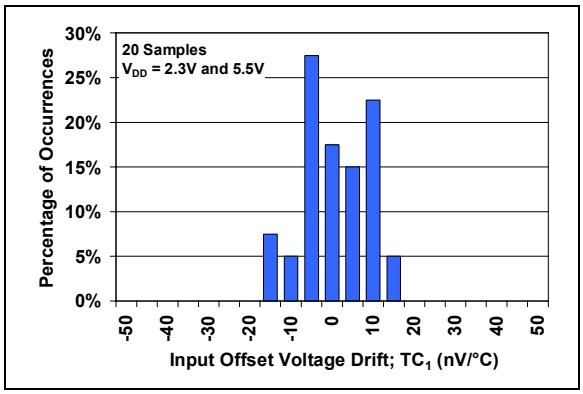


FIGURE 2-2: *Input Offset Voltage Drift.*

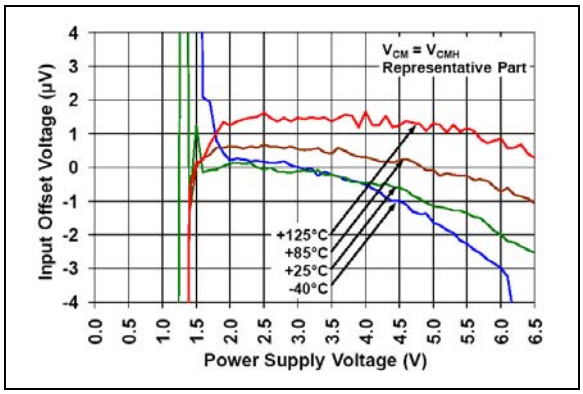


FIGURE 2-5: *Input Offset Voltage vs. Power Supply Voltage with V_{CM} = V_{CMH}.*

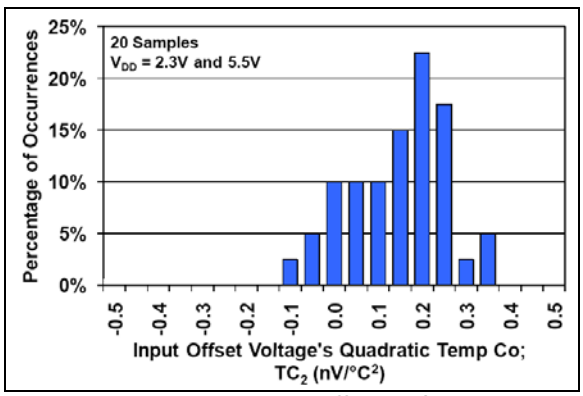


FIGURE 2-3: *Input Offset Voltage Quadratic Temperature Coefficient.*

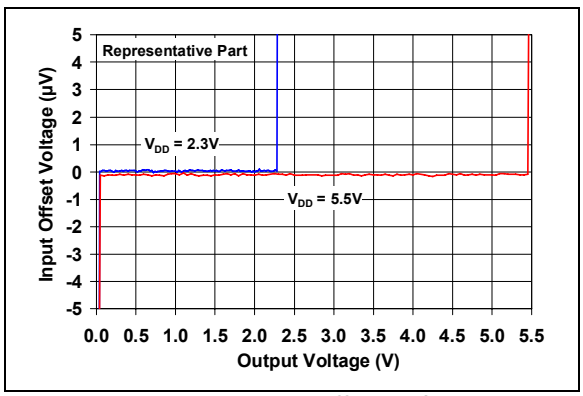


FIGURE 2-6: *Input Offset Voltage vs. Output Voltage.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

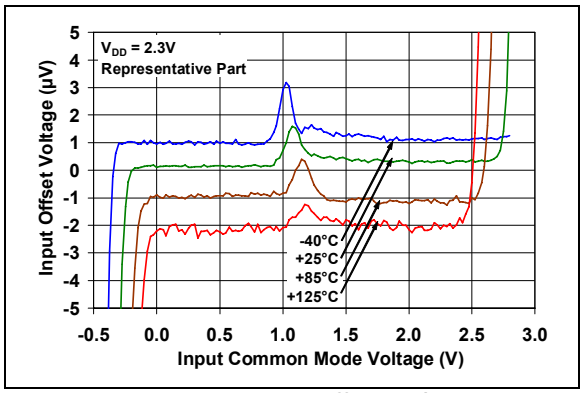


FIGURE 2-7: *Input Offset Voltage vs. Common Mode Voltage with V_{DD} = 2.3V.*

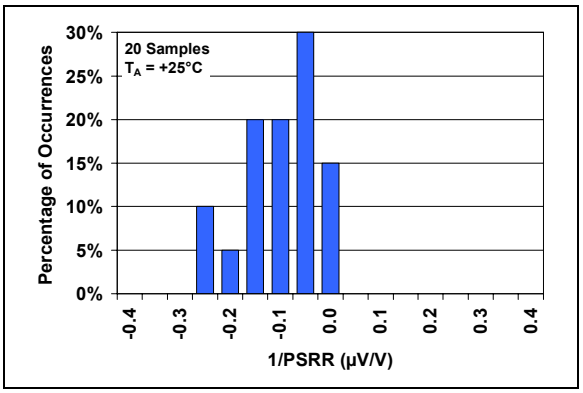


FIGURE 2-10: *PSRR.*

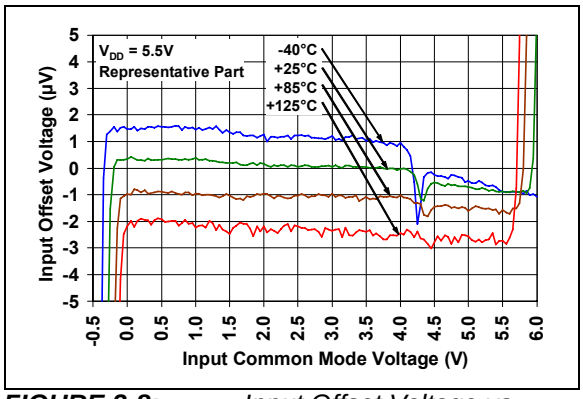


FIGURE 2-8: *Input Offset Voltage vs. Common Mode Voltage with V_{DD} = 5.5V.*

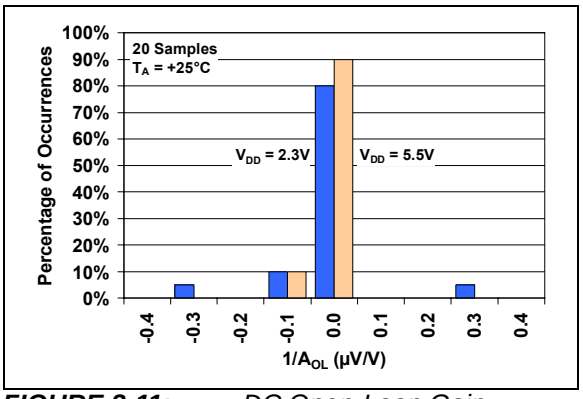


FIGURE 2-11: *DC Open-Loop Gain.*

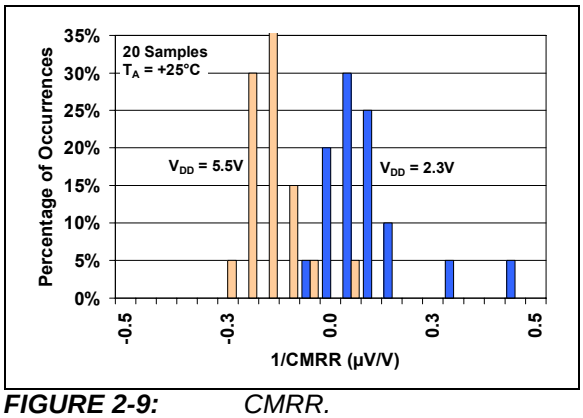


FIGURE 2-9: *CMRR.*

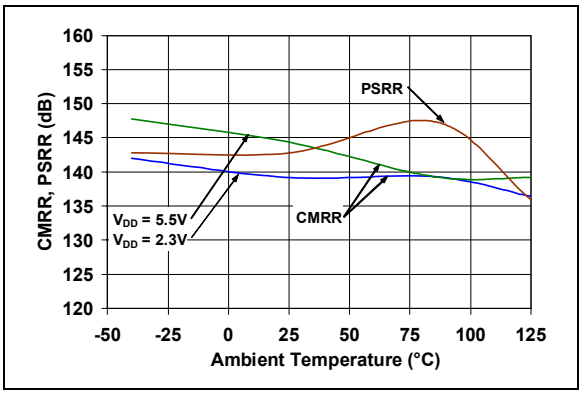


FIGURE 2-12: *CMRR and PSRR vs. Ambient Temperature.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

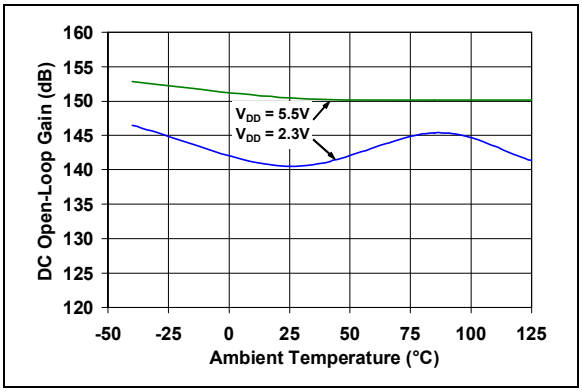


FIGURE 2-13: *DC Open-Loop Gain vs. Ambient Temperature.*

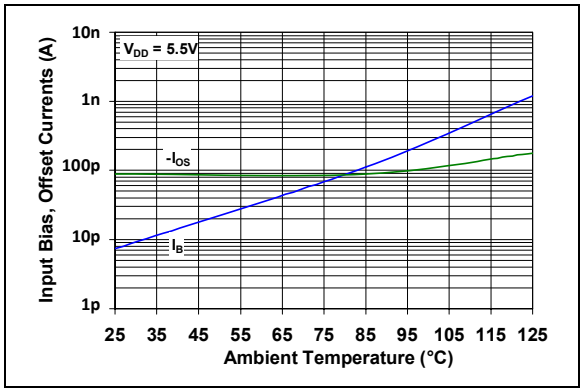


FIGURE 2-16: *Input Bias and Offset Currents vs. Ambient Temperature with V_{DD} = +5.5V.*

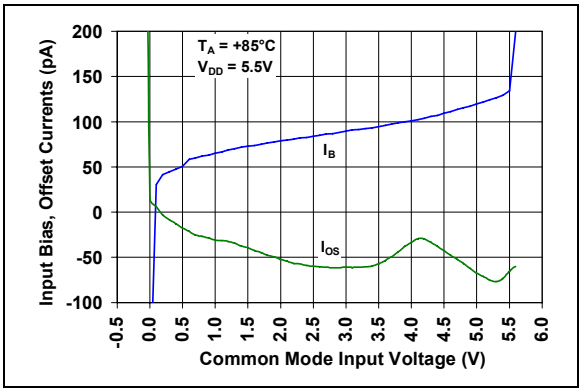


FIGURE 2-14: *Input Bias and Offset Currents vs. Common Mode Input Voltage with T_A = +85°C.*

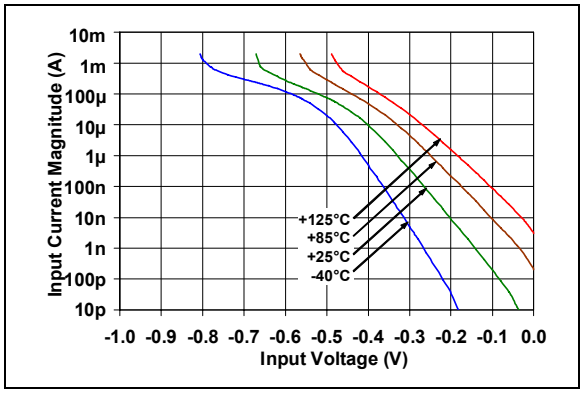


FIGURE 2-17: *Input Bias Current vs. Input Voltage (below V_{SS}).*

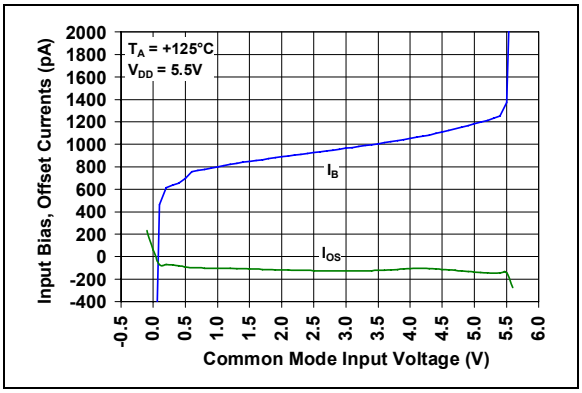


FIGURE 2-15: *Input Bias and Offset Currents vs. Common Mode Input Voltage with T_A = +125°C.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

2.2 Other DC Voltages and Currents

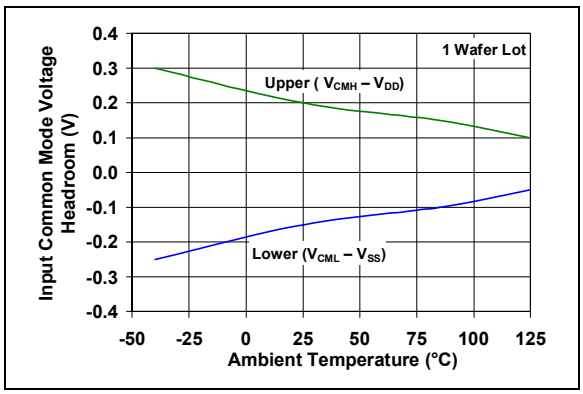


FIGURE 2-18: *Input Common Mode Voltage Headroom (Range) vs. Ambient Temperature.*

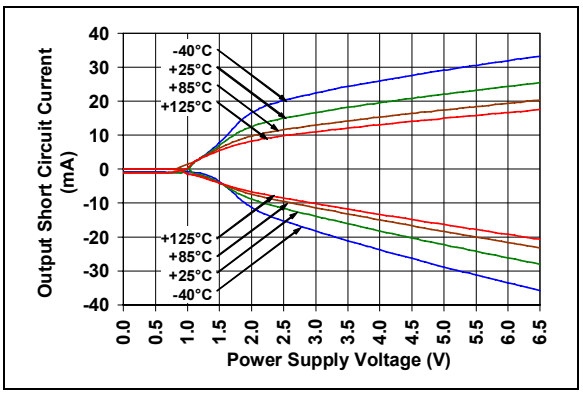


FIGURE 2-21: *Output Short Circuit Current vs. Power Supply Voltage.*

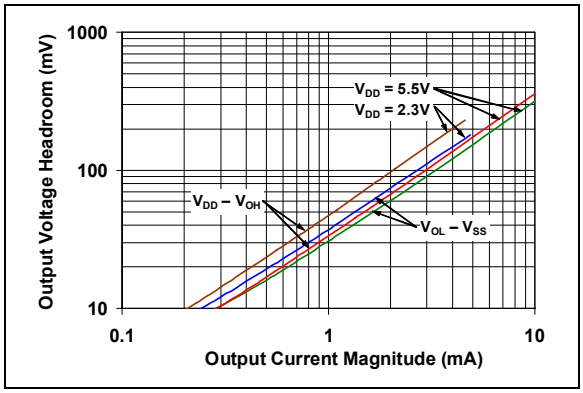


FIGURE 2-19: *Output Voltage Headroom vs. Output Current.*

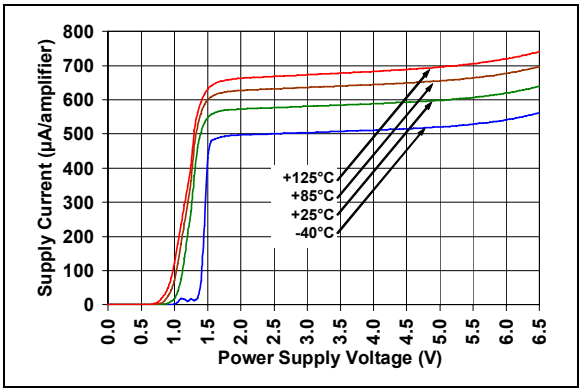


FIGURE 2-22: *Supply Current vs. Power Supply Voltage.*

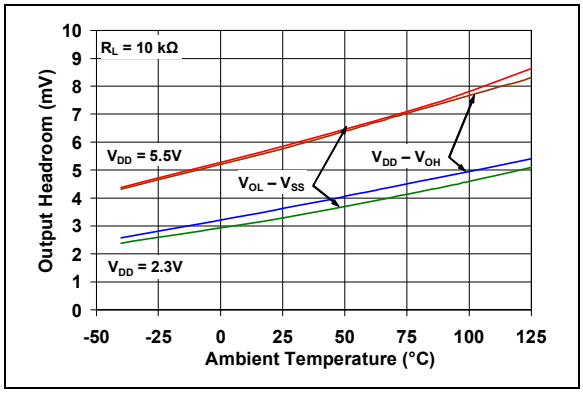


FIGURE 2-20: *Output Voltage Headroom vs. Ambient Temperature.*

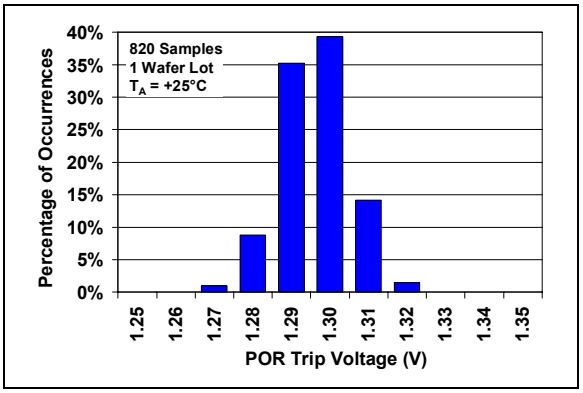


FIGURE 2-23: *Power On Reset Trip Voltage.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

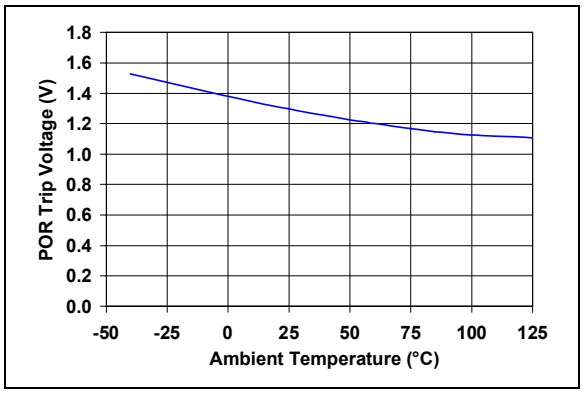


FIGURE 2-24: *Power On Reset Voltage vs. Ambient Temperature.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

2.3 Frequency Response

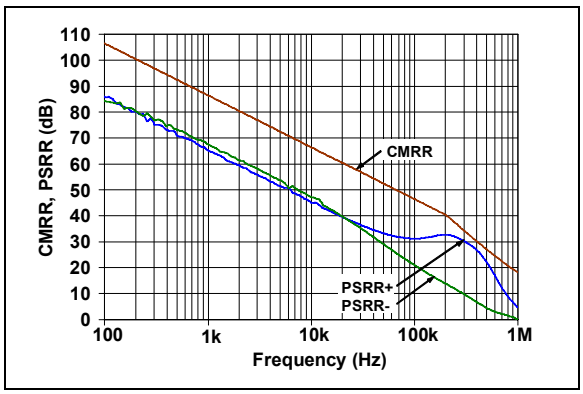


FIGURE 2-25: *CMRR and PSRR vs. Frequency.*

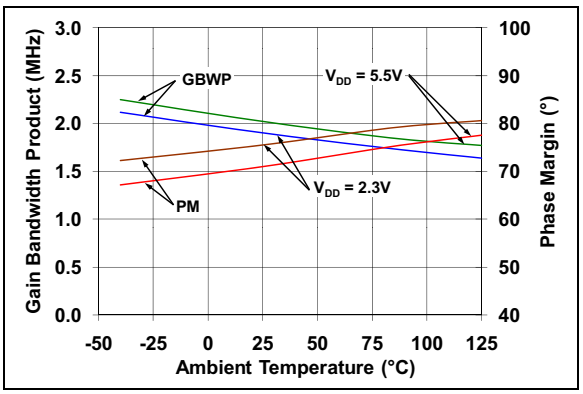


FIGURE 2-28: *Gain Bandwidth Product and Phase Margin vs. Ambient Temperature.*

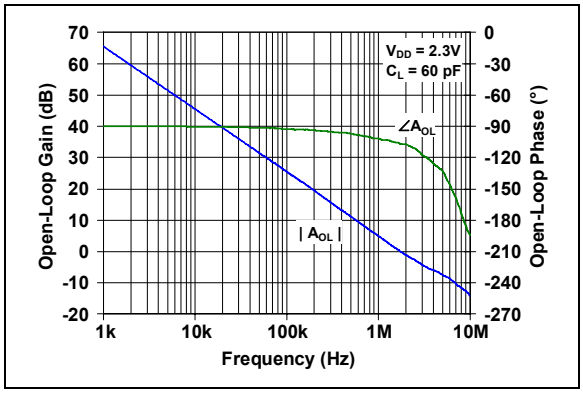


FIGURE 2-26: *Open-Loop Gain vs. Frequency with V_{DD} = 2.3V.*

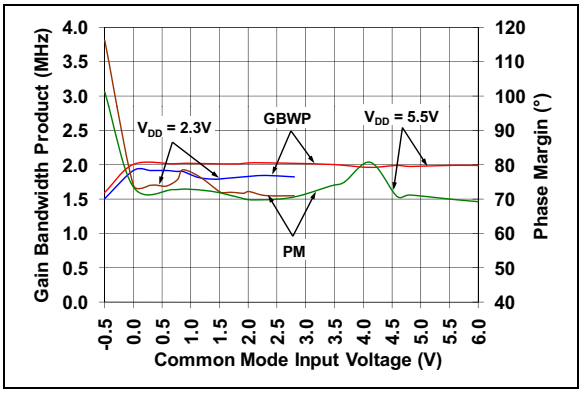


FIGURE 2-29: *Gain Bandwidth Product and Phase Margin vs. Common Mode Input Voltage.*

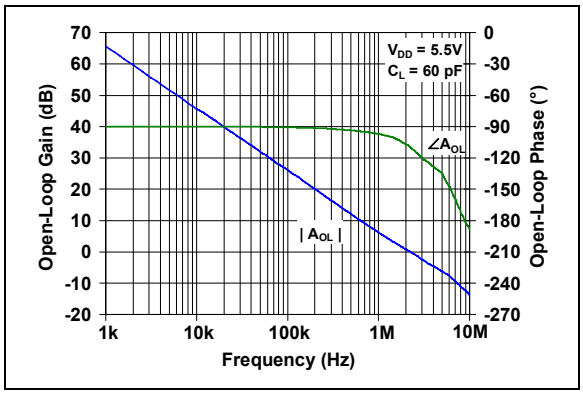


FIGURE 2-27: *Open-Loop Gain vs. Frequency with V_{DD} = 5.5V.*

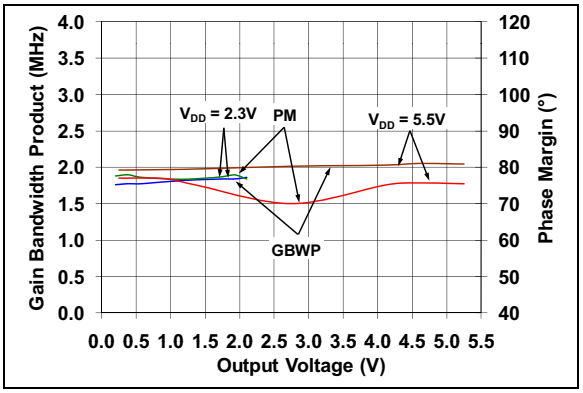


FIGURE 2-30: *Gain Bandwidth Product and Phase Margin vs. Output Voltage.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

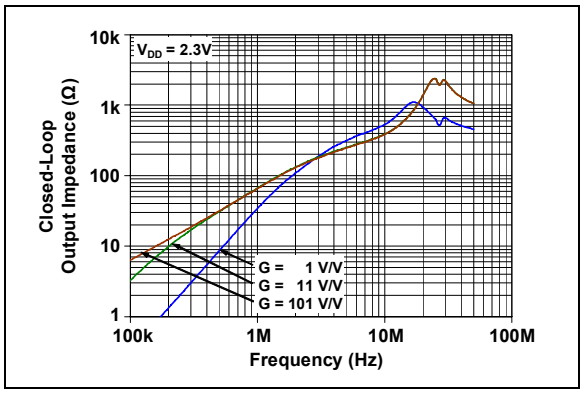


FIGURE 2-31: *Closed-Loop Output Impedance vs. Frequency with V_{DD} = 2.3V.*

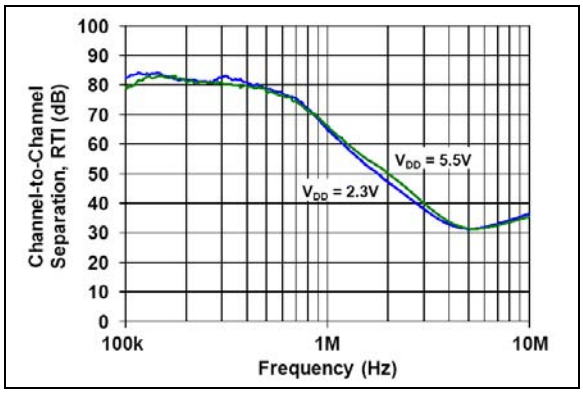


FIGURE 2-33: *Channel-to-Channel Separation vs. Frequency.*

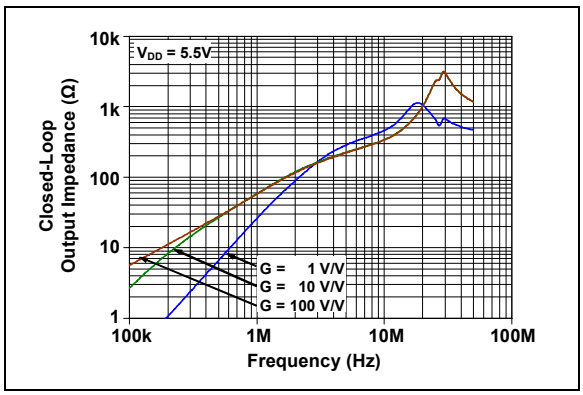


FIGURE 2-32: *Closed-Loop Output Impedance vs. Frequency with V_{DD} = 5.5V.*

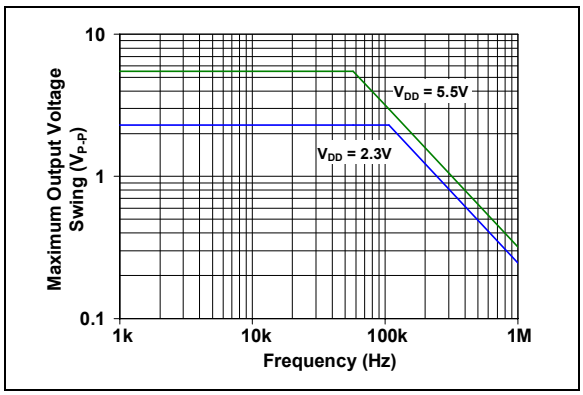


FIGURE 2-34: *Maximum Output Voltage Swing vs. Frequency.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

2.4 Input Noise and Distortion

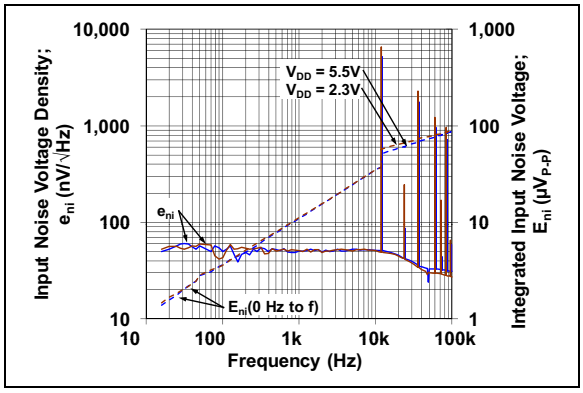


FIGURE 2-35: *Input Noise Voltage Density and Integrated Input Noise Voltage vs. Frequency.*

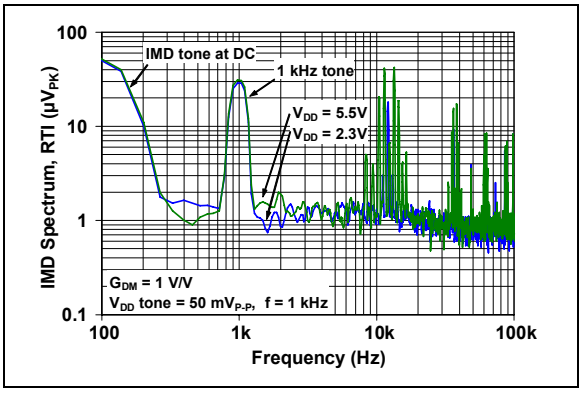


FIGURE 2-38: *Inter-Modulation Distortion vs. Frequency with V_{DD} Disturbance (see Figure 1-6).*

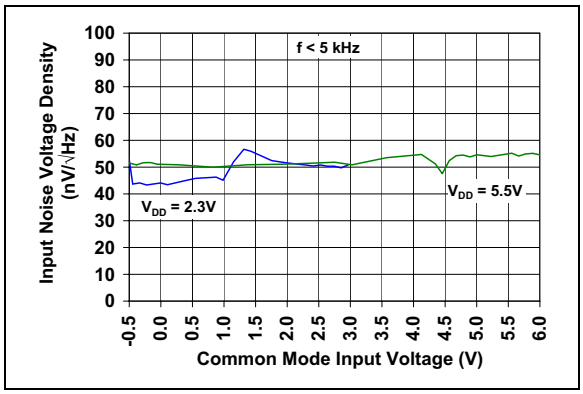


FIGURE 2-36: *Input Noise Voltage Density vs. Input Common Mode Voltage.*

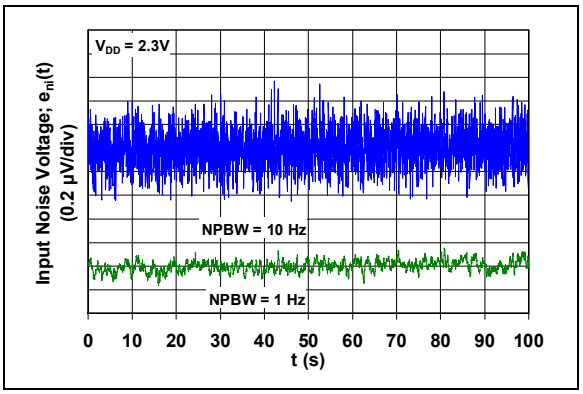


FIGURE 2-39: *Input Noise vs. Time with 1 Hz and 10 Hz Filters and V_{DD} =2.3V.*

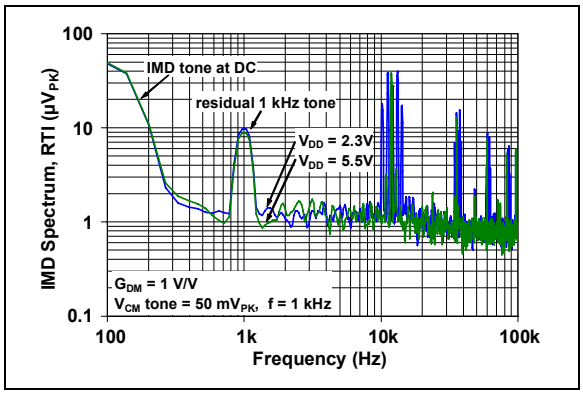


FIGURE 2-37: *Inter-Modulation Distortion vs. Frequency with V_{CM} Disturbance (see Figure 1-6).*

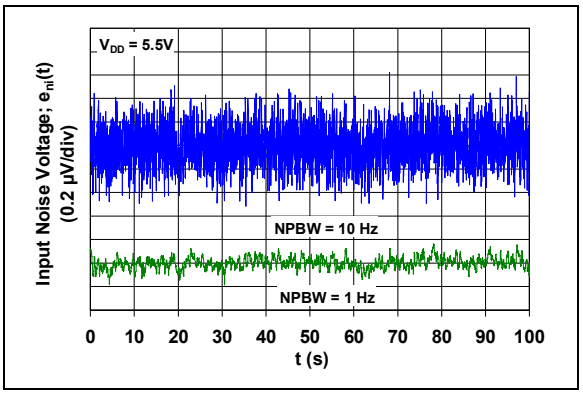


FIGURE 2-40: *Input Noise vs. Time with 1 Hz and 10 Hz Filters and V_{DD} =5.5V.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

2.5 Time Response

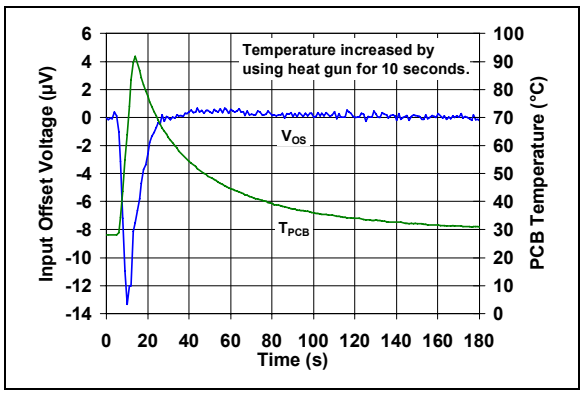


FIGURE 2-41: *Input Offset Voltage vs. Time with Temperature Change.*

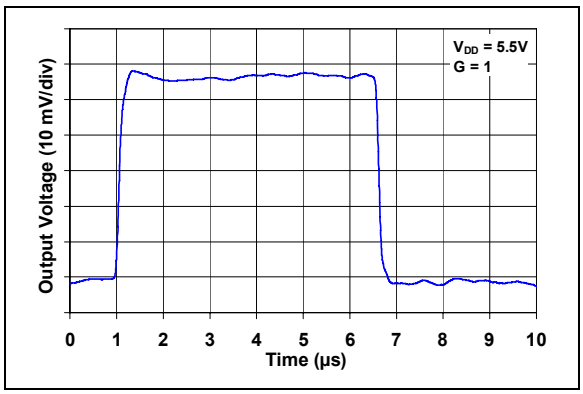


FIGURE 2-44: *Non-inverting Small Signal Step Response.*

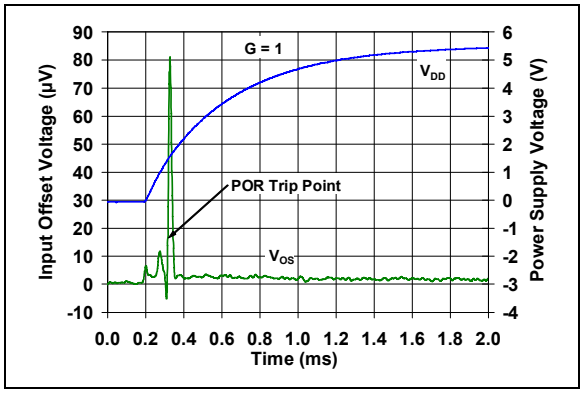


FIGURE 2-42: *Input Offset Voltage vs. Time at Power Up.*

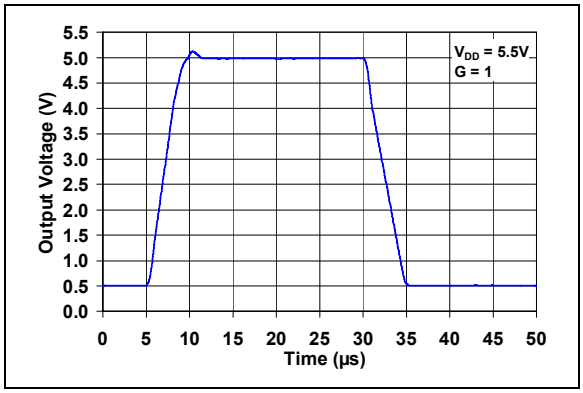


FIGURE 2-45: *Non-inverting Large Signal Step Response.*

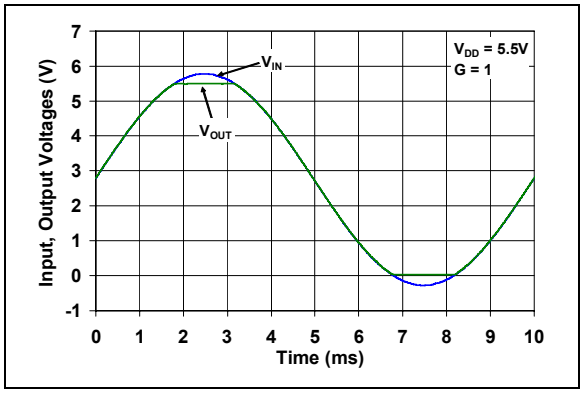


FIGURE 2-43: *The MCP6V27 Device Shows No Input Phase Reversal with Overdrive.*

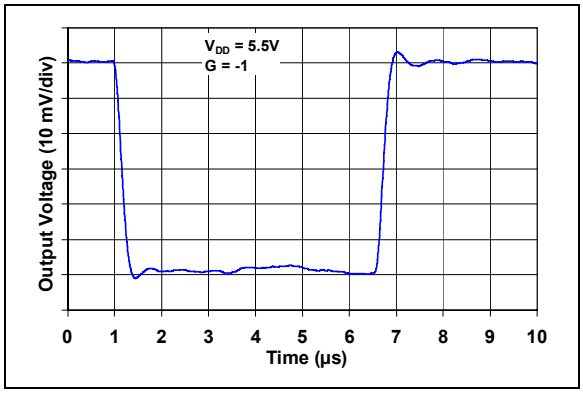


FIGURE 2-46: *Inverting Small Signal Step Response.*

Note: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to 5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2, R_L = 10 kΩ to V_L and C_L = 60 pF.

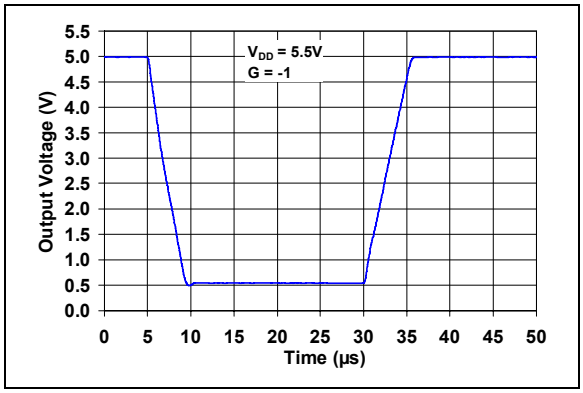


FIGURE 2-47: *Inverting Large Signal Step Response.*

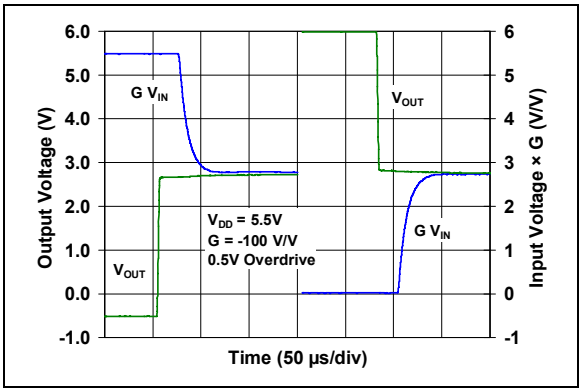


FIGURE 2-49: *Output Overdrive Recovery vs. Time with G = -100 V/V.*

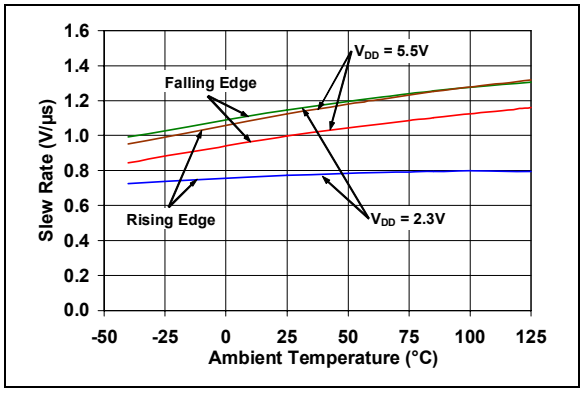


FIGURE 2-48: *Slew Rate vs. Ambient Temperature.*

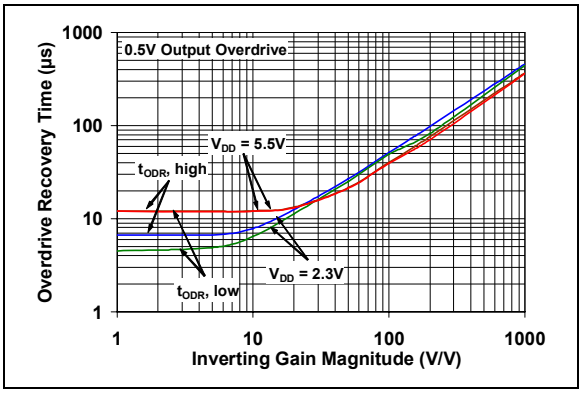


FIGURE 2-50: *Output Overdrive Recovery Time vs. Inverting Gain.*

3.0 PIN DESCRIPTIONS

Descriptions of the pins are listed in Table 3-1.

TABLE 3-1: PIN FUNCTION TABLE

MCP6V27		Symbol	Description
DFN	MSOP, SOIC		
1	1	V_{OUT}, V_{OUTA}	Output (op amp A)
2	2	$V_{IN}–$, $V_{INA}–$	Inverting Input (op amp A)
3	3	$V_{IN}+$, $V_{INA}+$	Non-inverting Input (op amp A)
4	4	V_{SS}	Negative Power Supply
5	5	$V_{INB}+$	Non-inverting Input (op amp B)
6	6	$V_{INB}–$	Inverting Input (op amp B)
7	7	V_{OUTB}	Output (op amp B)
8	8	V_{DD}	Positive Power Supply
9	—	EP	Exposed Thermal Pad (EP); must be connected to V_{SS}

3.1 Analog Outputs

The analog output pins (V_{OUT}) are low-impedance voltage sources.

3.2 Analog Inputs

The non-inverting and inverting inputs ($V_{IN}+$, $V_{IN}–$, …) are high-impedance CMOS inputs with low bias currents.

3.3 Power Supply Pins

The positive power supply (V_{DD}) is 2.3V to 5.5V higher than the negative power supply (V_{SS}). For normal operation, the other pins are between V_{SS} and V_{DD}.

Typically, these parts are used in a single (positive) supply configuration. In this case, V_{SS} is connected to ground and V_{DD} is connected to the supply. V_{DD} will need bypass capacitors.

3.4 Exposed Thermal Pad (EP)

There is an internal connection between the Exposed Thermal Pad (EP) and the V_{SS} pin; they must be connected to the same potential on the Printed Circuit Board (PCB).

This pad can be connected to a PCB ground plane to provide a larger heat sink. This improves the package thermal resistance (θ_{JA}).

NOTES:

4.0 APPLICATIONS

The MCP6V27 auto-zeroed op amp is manufactured using Microchip's state of the art CMOS process. It is designed for low cost, low power and high precision applications. Its low supply voltage, low quiescent current and wide bandwidth makes the MCP6V27 device ideal for battery-powered applications.

4.1 Overview of Auto-Zeroing Operation

Figure 4-1 shows a simplified diagram of the MCP6V27 auto-zeroed op amp. This will be used to explain how the DC voltage errors are reduced in this architecture.

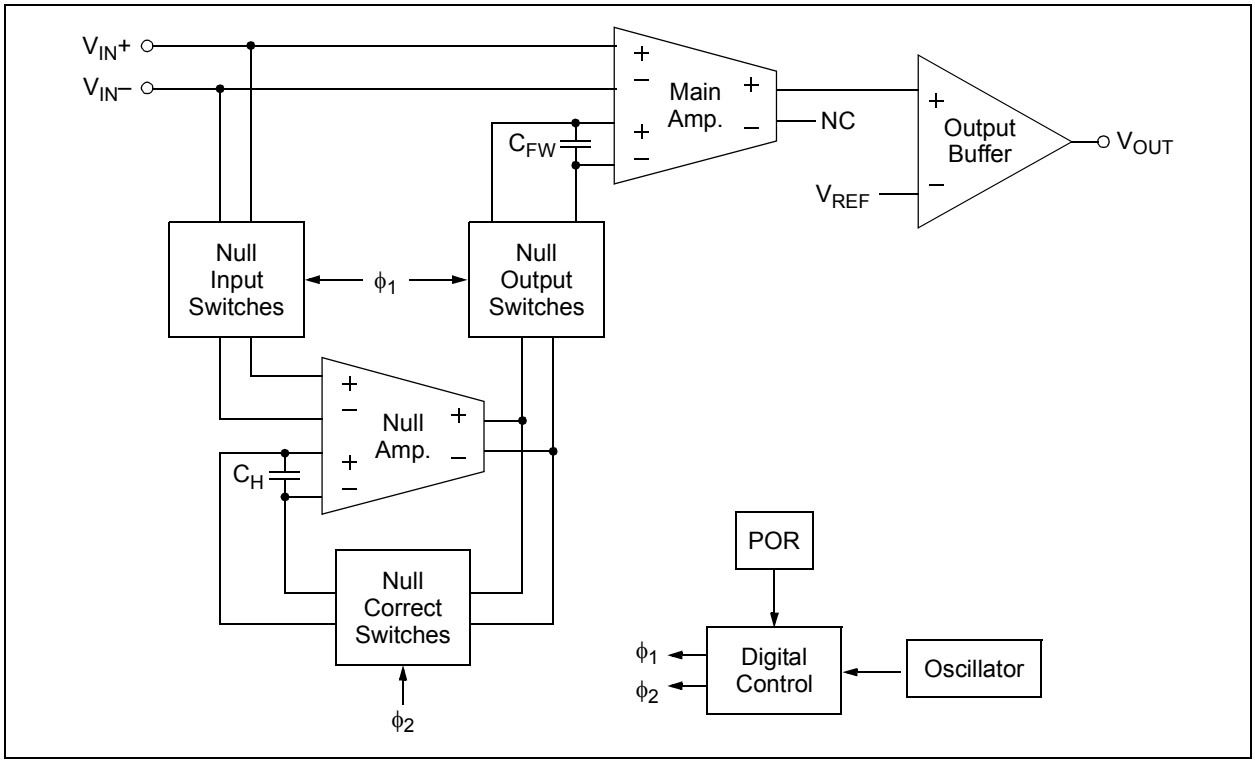


FIGURE 4-1: *Simplified Auto-Zeroed Op Amp Functional Diagram.*

4.1.1 BUILDING BLOCKS

The Null Amplifier and Main Amplifier are designed for high gain and accuracy using a differential topology. They have a main input pair (+ and - pins at their top left) used for the signal. They have an auxiliary input pair (+ and - pins at their bottom left) used for correcting the offset voltages. Both input pairs are added together internally. The capacitors at the auxiliary inputs (C_{FW} and C_H) hold the corrected values during normal operation.

The Output Buffer is designed to drive external loads at the V_{OUT} pin. It also produces a single ended output voltage (V_{REF} is an internal reference voltage).

All of these switches are make-before-break in order to minimize glitch-induced errors. They are driven by two clock phases (ϕ_1 and ϕ_2) that select between normal mode and auto-zeroing mode.

The clock is derived from an internal R-C oscillator running at a rate of f_{OSC1} = 850 kHz. The oscillator's output is divided down to the desired rate.

The internal POR ensures the part starts up in a known good state. It also provides protection against power supply brown-out events.

The Digital Control circuitry takes care of all of the housekeeping details of the switching operation. It also takes care of POR events.

4.1.2 AUTO-ZEROING ACTION

Figure 4-2 shows the connections between amplifiers during the Normal Mode of operation (ϕ_1). The hold capacitor (C_H) corrects the Null Amplifier's input offset. Since the Null Amplifier has very high gain, it dominates the signal seen by the Main Amplifier. This greatly reduces the impact of the Main Amplifier's input offset voltage on overall performance. Essentially, the Null Amplifier and Main Amplifier behave as a regular op amp with very high gain (A_{OL}) and very low offset voltage (V_{OS}).

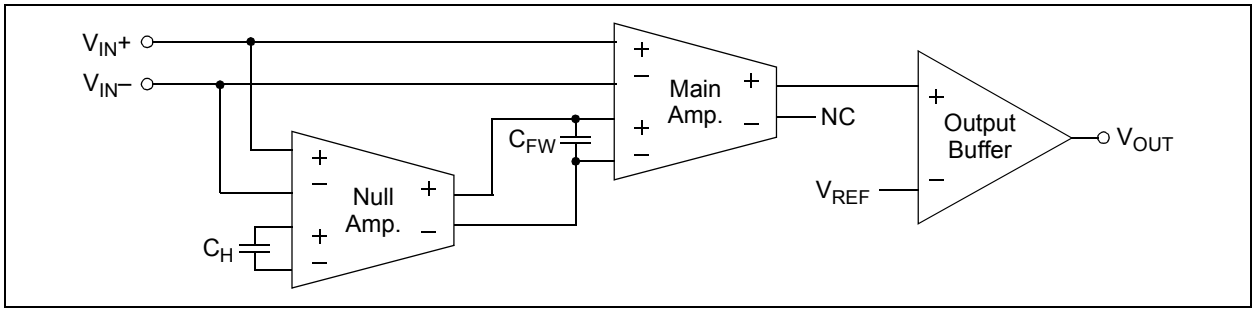


FIGURE 4-2: *Normal Mode of Operation (ϕ_1); Equivalent Amplifier Diagram.*

Figure 4-3 shows the connections between amplifiers during the Auto-zeroing Mode of operation (ϕ_2). The signal goes directly through the Main Amplifier, and the flywheel capacitor (C_{FW}) maintains a constant correction on the Main Amplifier's offset.

The Null Amplifier uses its own high open loop gain to drive the voltage across C_H to the point where its input offset voltage is almost zero. Because the signal input pair is connected to V_{IN}+, the auto-zeroing action corrects the offset at the current common mode input voltage (V_{CM}) and supply voltage (V_{DD}). This makes the DC CMRR and PSRR very high also.

Since these corrections happen every 40 µs, or so, we also minimize slow errors, including offset drift with temperature ($\Delta V_{OS}/\Delta T_A$), 1/f noise, and input offset aging.

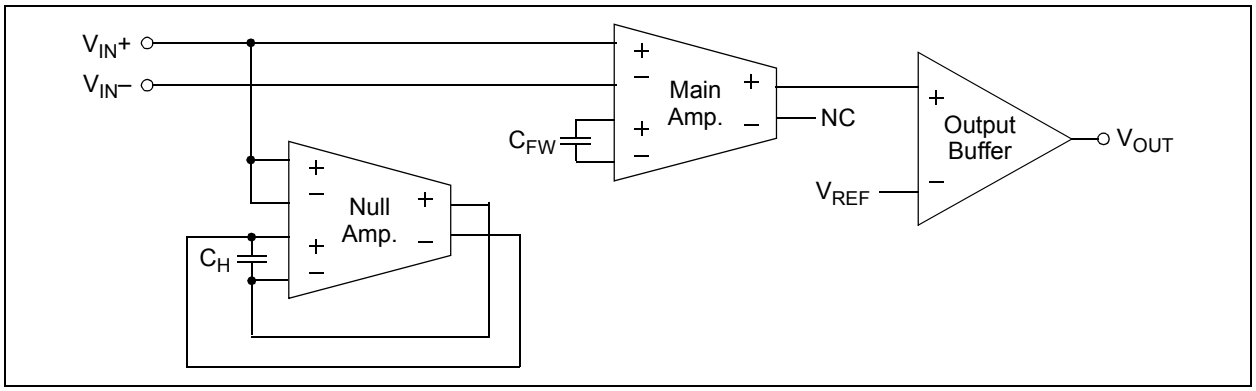


FIGURE 4-3: *Auto-zeroing Mode of Operation (ϕ_2); Equivalent Diagram.*

4.1.3 INTERMODULATION DISTORTION (IMD)

The MCP6V27 op amp will show intermodulation distortion (IMD), products when an AC signal is present.

The signal and clock can be decomposed into sine wave tones (Fourier series components). These tones interact with the auto-zeroing circuitry's non-linear response to produce IMD tones at sum and difference frequencies. IMD distortion tones are generated about all of the square wave clock's harmonics. See Figure 2-37 and Figure 2-38.

4.2 Other Functional Blocks

4.2.1 RAIL-TO-RAIL INPUTS

The input stage of the MCP6V27 op amp uses two differential CMOS input stages in parallel. One operates at low common mode input voltage (V_{CM}, which is approximately equal to $V_{IN}+$ and $V_{IN}–$ in normal operation) and the other at high V_{CM}. With this topology, the input operates with V_{CM} up to V_{DD} + 0.2V, and down to V_{SS} – 0.15V, at +25°C (see Figure 2-18). The input offset voltage (V_{OS}) is measured at $V_{CM} = V_{SS} – 0.15V$ and V_{DD} + 0.2V to ensure proper operation.

The transition between the input stages occurs when $V_{CM} \approx V_{DD} – 1.2V$ (see Figure 2-7 and Figure 2-8). For the best distortion and gain linearity, with non-inverting gains, avoid this region of operation.

4.2.1.1 Phase Reversal

The input devices are designed to not exhibit phase inversion when the input pins exceed the supply voltages. Figure 2-43 shows an input voltage exceeding both supplies with no phase inversion.

4.2.1.2 Input Voltage Limits

In order to prevent damage and/or improper operation of these amplifiers, the circuit must limit the voltages at the input pins (see **Section 1.1, Absolute Maximum Ratings †**). This requirement is independent of the current limits discussed later on.

The ESD protection on the inputs can be depicted as shown in Figure 4-4. This structure was chosen to protect the input transistors against many (but not all) over-voltage conditions, and to minimize input bias current (I_B).

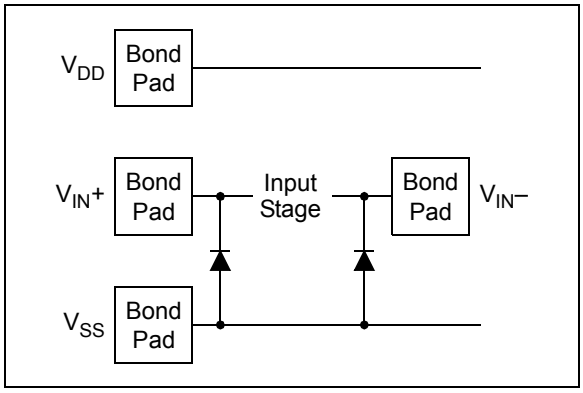


FIGURE 4-4: *Simplified Analog Input ESD Structures.*

The input ESD diodes clamp the inputs when they try to go more than one diode drop below V_{SS}. They also clamp any voltages that are well above V_{DD}; their breakdown voltage is high enough to allow normal operation, but not low enough to protect against slow over-voltage (beyond V_{DD}) events. Very fast ESD events (that meet the spec) are limited so that damage does not occur.

In some applications, it may be necessary to prevent excessive voltages from reaching the op amp inputs; Figure 4-5 shows one approach to protecting these inputs. D_1 and D_2 may be small signal silicon diodes, Schottky diodes for lower clamping voltages or diode-connected FETs for low leakage.

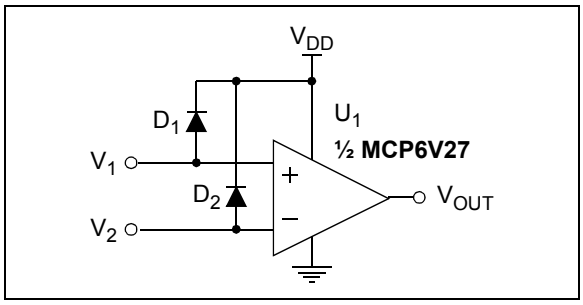


FIGURE 4-5: *Protecting the Analog Inputs Against High Voltages.*

4.2.1.3 Input Current Limits

In order to prevent damage and/or improper operation of these amplifiers, the circuit must limit the currents into the input pins (see **Section 1.1, Absolute Maximum Ratings †**). This requirement is independent of the voltage limits previously discussed.

Figure 4-6 shows one approach to protecting these inputs. The resistors R_1 and R_2 limit the possible current in or out of the input pins (and into D_1 and D_2). The diode currents will dump onto V_{DD}.

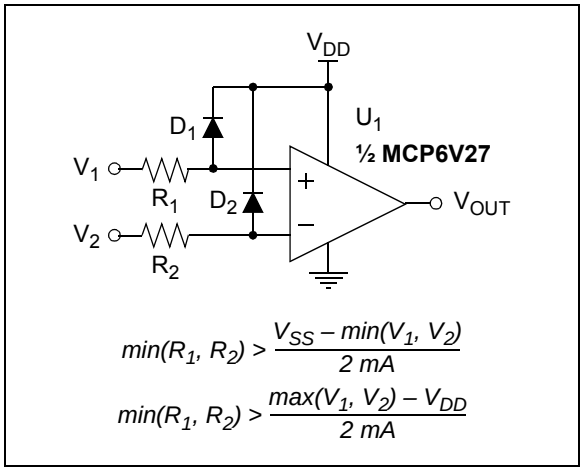


FIGURE 4-6: *Protecting the Analog Inputs Against High Currents.*

It is also possible to connect the diodes to the left of resistors R_1 and R_2. In this case, the currents through the diodes D_1 and D_2 need to be limited by some other mechanism. The resistors then serve as in-rush current limiters; the DC current into the input pins (V_{IN}+ and V_{IN}–) should be very small.

A significant amount of current can flow out of the inputs (through the ESD diodes) when the common mode voltage (V_{CM}) is below ground (V_{SS}); see Figure 2-17.

4.2.2 RAIL-TO-RAIL OUTPUT

The output voltage range of the MCP6V27 zero-drift op amp is V_{DD} – 15 mV (minimum) and V_{SS} + 15 mV (maximum) when R_L = 10 kΩ is connected to $V_{DD}/2$ and V_{DD} = 5.5V. Refer to Figure 2-19 and Figure 2-20.

This op amp is designed to drive light loads; use another amplifier to buffer the output from heavy loads.

4.3 Application Tips

4.3.1 INPUT OFFSET VOLTAGE OVER TEMPERATURE

Table 1-1 gives both the linear and quadratic temperature coefficients (TC_1 and TC_2) of input offset voltage. The input offset voltage, at any temperature in the specified range, can be calculated as follows:

EQUATION 4-1:

$$V_{OS}(T_A) = V_{OS} + TC_1\Delta T + TC_2\Delta T^2$$

Where:

ΔT	=	T_A – 25°C
$V_{OS}(T_A)$	=	input offset voltage at T_A
V_{OS}	=	input offset voltage at +25°C
TC_1	=	linear temperature coefficient
TC_2	=	quadratic temperature coefficient

4.3.2 DC GAIN PLOTS

Figure 2-9, Figure 2-10 and Figure 2-11 are histograms of the reciprocals (in units of µV/V) of CMRR, PSRR and A_{OL}, respectively. They represent the change in input offset voltage (V_{OS}) with a change in common mode input voltage (V_{CM}), power supply voltage (V_{DD}) and output voltage (V_{OUT}).

The $1/A_{OL}$ histogram is centered near 0 µV/V because the measurements are dominated by the op amp's input noise. The negative values shown represent noise, *not* unstable behavior. We validate the op amps' stability by making multiple measurements of V_{OS}; an unstable part would show either greater variability in V_{OS}, or the output is stuck at one of the rails.

4.3.3 OFFSET AT POWER UP

When this part powers up, the input offset (V_{OS}) starts at its uncorrected value (usually less than ±5 mV). Circuits with high DC gain can cause the output to reach one of the two rails. In this case, the time to a valid output is delayed by an output overdrive time (like t_{ODR}), in addition to the startup time (like t_{STR}).

It can be simple to avoid this extra startup time. Reducing the gain is one method. Adding a capacitor across the feedback resistor (R_F) is another method.

4.3.4 SOURCE RESISTANCES

The input bias currents have two significant components; switching glitches that dominate at room temperature and below, and input ESD diode leakage currents that dominate at +85°C and above.

Make the resistances seen by the inputs small and equal. This minimizes the output offset caused by the input bias currents.

The inputs should see a resistance on the order of 10Ω to 1 kΩ at high frequencies (i.e., above 1 MHz). This helps minimize the impact of switching glitches, which are very fast, on overall performance. In some cases, it may be necessary to add resistors in series with the inputs to achieve this improvement in performance.

4.3.5 SOURCE CAPACITANCE

The capacitances seen by the two inputs should be small and matched. The internal switches connected to the inputs dump charges on these capacitors; an offset can be created if the capacitances do not match.

4.3.6 CAPACITIVE LOADS

Driving large capacitive loads can cause stability problems for voltage feedback op amps. As the load capacitance increases, the feedback loop's phase margin decreases and the closed-loop bandwidth is reduced. This produces gain peaking in the frequency response, with overshoot and ringing in the step response. These auto-zeroed op amps have a different output impedance than most op amps, due to their unique topology.

When driving a capacitive load with these op amps, a series resistor at the output (R_{ISO} in Figure 4-7) improves the feedback loop's phase margin (stability) by making the output load resistive at higher frequencies. The bandwidth will be generally lower than the bandwidth with no capacitive load.

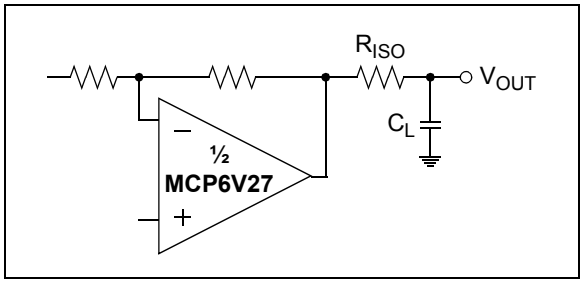


FIGURE 4-7: *Output Resistor, R_{ISO}, Stabilizes Capacitive Loads.*

Figure 4-8 gives recommended R_{ISO} values for different capacitive loads and gains. The x-axis is the normalized load capacitance (C_L/G_N^2). The y-axis is the normalized resistance ($G_N R_{ISO}$).

G_N is the circuit's noise gain. For non-inverting gains, G_N and the Signal Gain are equal. For inverting gains, G_N is 1+|Signal Gain| (e.g., -1 V/V gives G_N = +2 V/V).

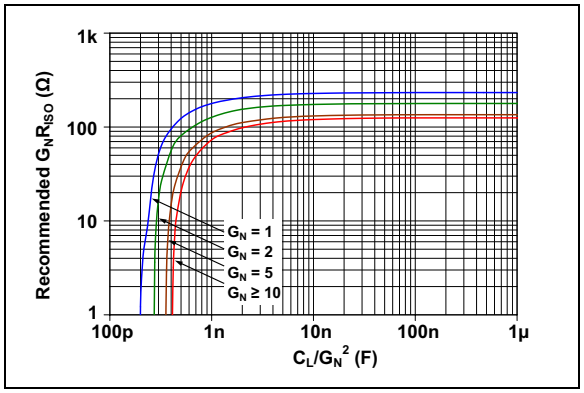


FIGURE 4-8: *Recommended R_{ISO} values for Capacitive Loads.*

After selecting R_{ISO} for your circuit, double check the resulting frequency response peaking and step response overshoot. Modify R_{ISO}'s value until the response is reasonable. Bench evaluation and simulations with the MCP6V27 SPICE macro model are helpful.

4.3.7 STABILIZING OUTPUT LOADS

This auto-zeroed op amp has an output impedance (Figure 2-31 and Figure 2-32) that has a double zero when the gain is low. This can cause a large phase shift in feedback networks that have low resistance near the part's bandwidth. This large phase shift can cause stability problems.

Figure 4-9 shows that the load on the output is (R_L + R_{ISO})||(R_F + R_G), where R_{ISO} is before the load (like Figures 4-7). This load needs to be large enough to maintain stability; it should be at least (2 kΩ)/G_N.

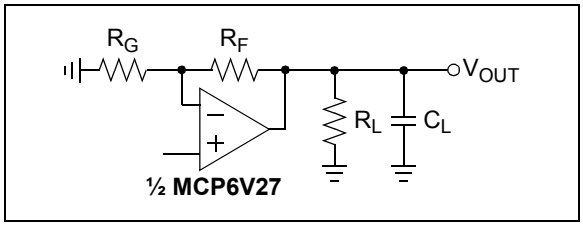


FIGURE 4-9: *Output Load.*

4.3.8 GAIN PEAKING

Figure 4-10 shows an op amp circuit that represents non-inverting amplifiers (V_M is a DC voltage and V_P is the input) or inverting amplifiers (V_P is a DC voltage and V_M is the input). The capacitances C_N and C_G represent the total capacitance at the input pins; they include the op amp's common mode input capacitance (C_{CM}), board parasitic capacitance and any capacitor placed in parallel.

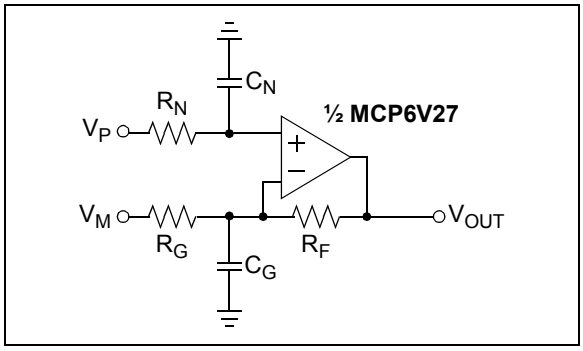


FIGURE 4-10: *Amplifier with Parasitic Capacitance.*

C_G acts in parallel with R_G (except for a gain of +1 V/V), which causes an increase in gain at high frequencies. C_G also reduces the phase margin of the feedback loop, which becomes less stable. This effect can be reduced by either reducing C_G or $R_F||R_G$.

C_N and R_N form a low-pass filter that affects the signal at V_P. This filter has a single real pole at $1/(2\pi R_N C_N)$.

The largest value of R_F that should be used depends on noise gain (see G_N in **Section 4.3.6, Capacitive Loads**), C_G and the open-loop gain's phase shift. An approximate limit for R_F is:

EQUATION 4-2:

$$R_F \leq 2\ k\Omega \times \frac{12\ pF}{C_G} \times G_N^{\ 2}$$

Some applications may modify these values to reduce either output loading or gain peaking (step response overshoot).

4.3.9 REDUCING UNDESIRED NOISE AND SIGNALS

Reduce undesired noise and signals with:

- Low bandwidth signal filters:
  - Minimizes random analog noise
  - Reduces interfering signals
- Good PCB layout techniques:
  - Minimizes crosstalk
  - Minimizes parasitic capacitances and inductances that interact with fast switching edges
- Good power supply design:
  - Provides isolation from other parts
  - Filters interference on supply line(s)

4.3.10 SUPPLY BYPASSING AND FILTERING

With this operational amplifier, the power supply pin (V_{DD} for single supply) should have a local bypass capacitor (i.e., 0.01 µF to 0.1 µF) within 2 mm of the pin for good high-frequency performance.

This part also needs a bulk capacitor (i.e., 1 µF or larger) within 100 mm to provide large, slow currents. This bulk capacitor can be shared with other low noise, analog parts.

In some cases, high-frequency power supply noise (e.g., switched mode power supplies) may cause undue intermodulation distortion, with a DC offset shift; this noise needs to be filtered. Adding a resistor into the supply connection can be helpful. This resistors needs to be small enough to prevent a large drop in V_{DD} for the op amp, which would cause a reduced output range and possible load-induced power supply noise. It also needs to be large enough to dissipate little power when V_{DD} is turned on and off quickly. Figure 4-11 shows a circuit with resistors in the supply connections. It gives good rejection out to 1 MHz for switched mode power supplies. Smaller resistors and capacitors are a better choice for designs where the power supply is not as noisy.

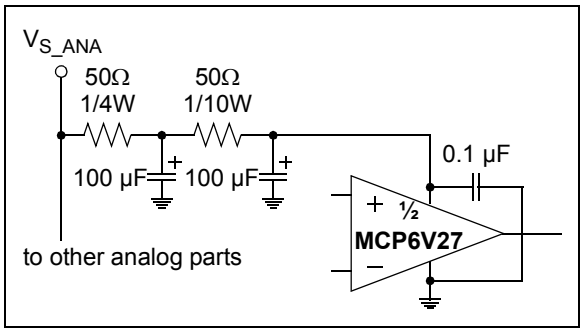


FIGURE 4-11: *Additional Supply Filtering.*

4.3.11 PCB DESIGN FOR DC PRECISION

In order to achieve DC precision on the order of ±1 µV, many physical errors need to be minimized. The design of the Printed Circuit Board (PCB), the wiring and the thermal environment has a strong impact on the precision achieved. A poor PCB design can easily be more than 100 times worse than the MCP6V27 op amp minimum and maximum specifications.

4.3.11.1 PCB Layout

Any time two dissimilar metals are joined together, a temperature dependent voltage appears across the junction (the Seebeck or thermo-junction effect). This effect is used in thermocouples to measure temperature. The following are examples of thermo-junctions on a PCB:

- Components (resistors, op amps, …) soldered to a copper pad
- Wires mechanically attached to the PCB
- Jumpers
- Solder joints
- PCB vias

Typical thermo-junctions have temperature to voltage conversion coefficients of 10 to 100 µV/°C (sometimes higher).

Microchip's AN1258 (*"Op Amp Precision Design: PCB Layout Techniques"*) contains in depth information on PCB layout techniques that minimize thermo-junction effects. It also discusses other effects, such as crosstalk, impedances, mechanical stresses and humidity.

4.3.11.2 Crosstalk

DC crosstalk causes offsets that appear as a larger input offset voltage. Common causes include:

- Common mode noise (remote sensors)
- Ground loops (current return paths)
- Power supply coupling

Interference from the mains (usually 50 Hz or 60 Hz), and other AC sources, can also affect the DC performance. Non-linear distortion can convert these signals to multiple tones, included a DC shift in voltage. When the signal is sampled by an ADC, these AC signals can also be aliased to DC, causing an apparent shift in offset.

To reduce interference:

- Keep traces and wires as short as possible
- Use shielding (e.g., encapsulant)
- Use ground plane (at least a star ground)
- Place the input signal source near to the DUT
- Use good PCB layout techniques
- Use a separate power supply filter (bypass capacitors) for these auto-zeroed op amps

4.3.11.3 Miscellaneous Effects

Keep the resistances seen by the input pins as small and as near to equal as possible to minimize bias current related offsets.

Make the (trace) capacitances seen by the input pins small and equal. This is helpful in minimizing switching glitch-induced offset voltages.

Bending a coax cable with a radius that is too small causes a small voltage drop to appear on the center conductor (the tribo-electric effect). Make sure the bending radius is large enough to keep the conductors and insulation in full contact.

Mechanical stresses can make some capacitor types (such as ceramic) to output small voltages. Use more appropriate capacitor types in the signal path and minimize mechanical stresses and vibration.

Humidity can cause electro-chemical potential voltages to appear in a circuit. Proper PCB cleaning helps, as does the use of encapsulants.

4.4 Typical Applications

4.4.1 WHEATSTONE BRIDGE

Many sensors are configured as Wheatstone bridges. Strain gauges and pressure sensors are two common examples. These signals can be small and the common mode noise large. Amplifier designs with high differential gain are desirable.

Figure 4-12 shows how to interface to a Wheatstone bridge with a minimum of components. Because the circuit is not symmetric, the ADC input is single ended, and there is a minimum of filtering, the CMRR is good enough for moderate common mode noise.

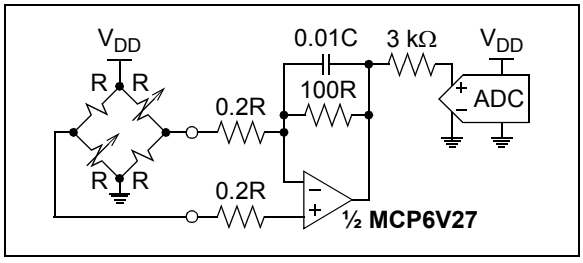


FIGURE 4-12: *Simple Design.*

Figure 4-13 shows a higher performance circuit for Wheatstone bridges. This circuit is symmetric and has high CMRR. Using a differential input to the ADC helps with the CMRR.

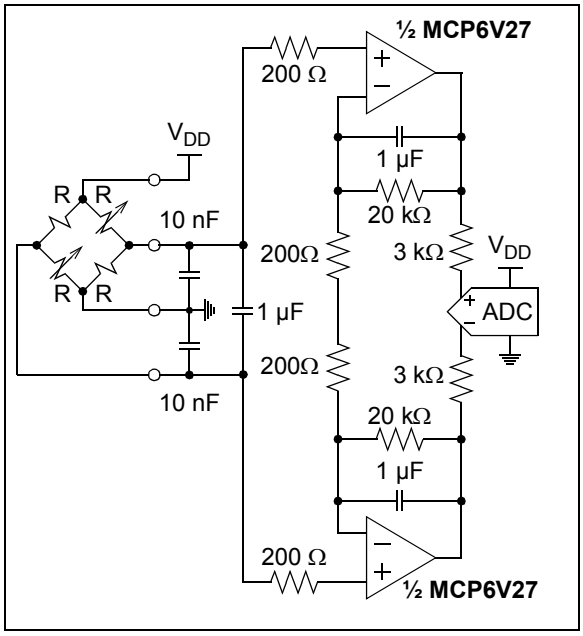


FIGURE 4-13: *High Performance Design.*

4.4.2 RTD SENSOR

The ratiometric circuit in Figure 4-14 conditions a three wire RTD. It corrects for the sensor's wiring resistance by subtracting the voltage across the middle R_W. The top R_1 does not change the output voltage; it balances the op amp inputs. Failure (open) of the RTD is detected by an out-of-range voltage.

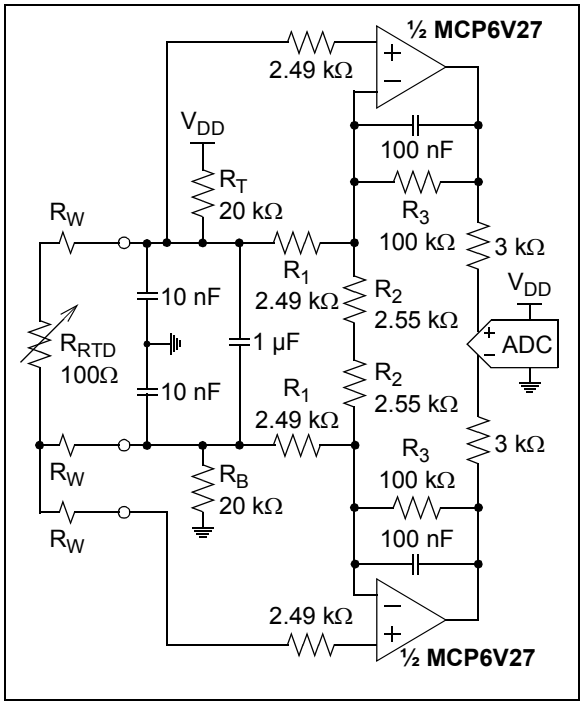


FIGURE 4-14: *RTD Sensor.*

The voltages at the input of the ADC can be calculated with the following:

$$G_{RTD} = 1 + 2 \cdot R_3/R_2$$
$$G_W = G_{RTD} - R_3/R_1$$
$$V_{DM} = G_{RTD}(V_T - V_B) + G_W V_W$$
$$V_{CM} = \frac{V_T + V_B + (G_{RTD} + 1 - G_W)V_W}{2}$$

Where:

V_T	=	Voltage at the top of R_{RTD}
V_B	=	Voltage at the bottom of R_{RTD}
V_W	=	Voltage across top and middle R_W's
V_{CM}	=	ADC's common mode input
V_{DM}	=	ADC's differential mode input

4.4.3 THERMOCOUPLE SENSOR

Figure 4-15 shows a simplified diagram of an amplifier and temperature sensor used in a thermocouple application. The type K thermocouple senses the temperature at the hot junction (T_{HJ}), and produces a voltage at V_1 proportional to T_{HJ} (in °C). The amplifier's gain is set so that V_4/T_{HJ} is 10 mV/°C. V_3 represents the output of a temperature sensor, which produces a voltage proportional to the temperature (in °C) at the cold junction (T_{CJ}), and with a 0.50V offset. V_2 is set so that V_4 is 0.50V when $T_{HJ} - T_{CJ}$ is 0°C.

EQUATION 4-3:

$$V_1 \approx T_{HJ}(40\ \mu V/°C)$$
$$V_2 = (1.00V)$$
$$V_3 = T_{CJ}(10\ mV/°C) + (0.50V)$$
$$V_4 = 250V_1 + (V_2 - V_3)$$
$$\approx (10\ mV/°C)\ (T_{HJ} - T_{CJ}) + (0.50V)$$

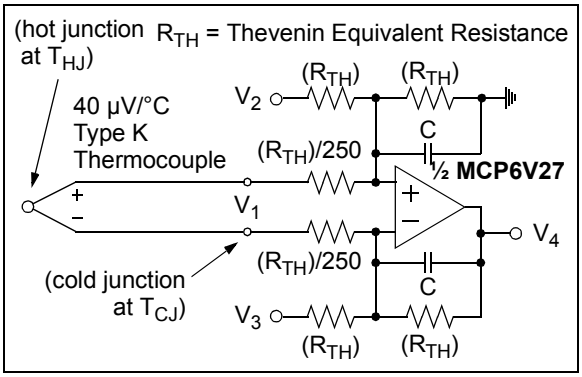


FIGURE 4-15: *Thermocouple Sensor; Simplified Circuit.*

Figure 4-16 shows a more complete implementation of this circuit. The dashed red arrow indicates a thermally conductive connection between the thermocouple and the MCP9700A; it needs to be very short and have low thermal resistance.

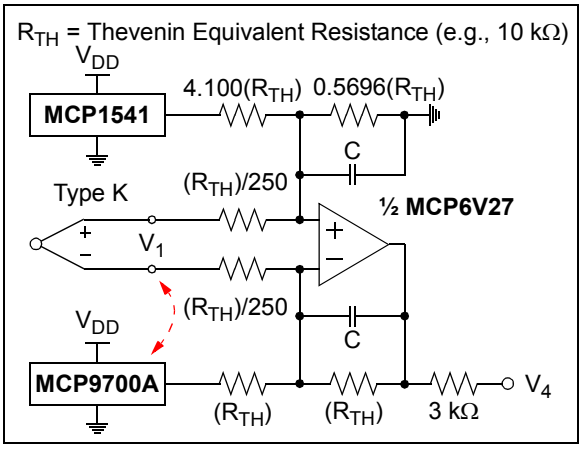


FIGURE 4-16: *Thermocouple Sensor.*

The MCP9700A senses the temperature at its physical location. It needs to be at the same temperature as the cold junction (T_{CJ}), and produces V_3 (Figure 4-15).

The MCP1541 produces a 4.10V output, assuming V_{DD} is at 5.0V. This voltage, tied to a resistor ladder of 4.100(R_{TH}) and 1.3224(R_{TH}), would produce a Thevenin equivalent of 1.00V and 250(R_{TH}). The 1.3224(R_{TH}) resistor is combined in parallel with the top right R_{TH} resistor (in Figure 4-15), producing the 0.5696(R_{TH}) resistor.

V_4 should be converted to digital, then corrected for the thermocouple's non-linearity. The ADC can use the MCP1541 as its voltage reference. Alternately, an absolute reference inside a PICmicro® device can be used instead of the MCP1541.

4.4.4 OFFSET VOLTAGE CORRECTION

Figure 4-17 shows an MCP6V27 correcting the input offset voltage of another op amp. R_2 and C_2 integrate the offset error seen at the other op amp's input; the integration needs to be slow enough to be stable (with the feedback provided by R_1 and R_3).

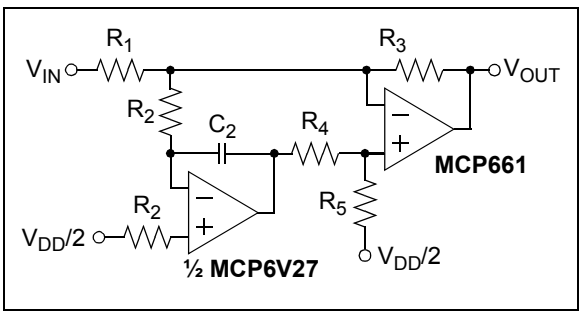


FIGURE 4-17: *Offset Correction.*

4.4.5 PRECISION COMPARATOR

Use high gain before a comparator to improve the latter's performance. Do not use MCP6V27 as a comparator by itself; the V_{OS} correction circuitry does not operate properly without a feedback loop.

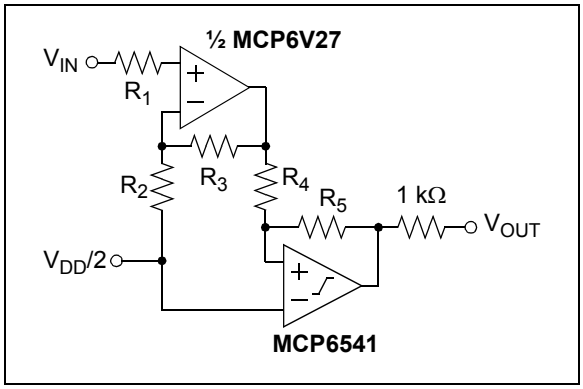


FIGURE 4-18: *Precision Comparator.*

NOTES:

5.0 DESIGN AIDS

Microchip provides the basic design aids needed for the MCP6V27 op amp.

5.1 SPICE Macro Model

The latest SPICE macro model for the MCP6V27 op amp is available on the Microchip web site at www.microchip.com. This model is intended to be an initial design tool that works well in the op amp's linear region of operation over the temperature range. See the model file for information on its capabilities.

Bench testing is a very important part of any design and cannot be replaced with simulations. Also, simulation results using this macro model need to be validated by comparing them to the data sheet specifications and characteristic curves.

5.2 FilterLab® Software

Microchip's FilterLab® software is an innovative software tool that simplifies analog active filter (using op amps) design. Available at no cost from the Microchip web site at www.microchip.com/filterlab, the Filter-Lab design tool provides full schematic diagrams of the filter circuit with component values. It also outputs the filter circuit in SPICE format, which can be used with the macro model to simulate actual filter performance.

5.3 Microchip Advanced Part Selector (MAPS)

MAPS is a software tool that helps efficiently identify Microchip devices that fit a particular design requirement. Available at no cost from the Microchip website at www.microchip.com/maps, the MAPS is an overall selection tool for Microchip's product portfolio that includes Analog, Memory, MCUs and DSCs. Using this tool, a customer can define a filter to sort features for a parametric search of devices and export side-by-side technical comparison reports. Helpful links are also provided for Data sheets, Purchase and Sampling of Microchip parts.

5.4 Analog Demonstration and Evaluation Boards

Microchip offers a broad spectrum of Analog Demonstration and Evaluation Boards that are designed to help customers achieve faster time to market. For a complete listing of these boards and their corresponding user's guides and technical information, visit the Microchip web site at www.microchip.com/analogtools.

Some boards that are especially useful are:

- MCP6V01 Thermocouple Auto-Zeroed Reference Design
- MCP6XXX Amplifier Evaluation Board 1
- MCP6XXX Amplifier Evaluation Board 2
- MCP6XXX Amplifier Evaluation Board 3
- MCP6XXX Amplifier Evaluation Board 4
- Active Filter Demo Board Kit
- P/N SOIC8EV: 8-Pin SOIC/MSOP/TSSOP/DIP Evaluation Board
- P/N SOIC14EV: 14-Pin SOIC/TSSOP/DIP Evaluation Board

5.5 Application Notes

The following Microchip Application Notes are available on the Microchip web site at www.microchip.com/appnotes and are recommended as supplemental reference resources.

ADN003: *"Select the Right Operational Amplifier for your Filtering Circuits"*, DS21821

AN722: *"Operational Amplifier Topologies and DC Specifications"*, DS00722

AN723: *"Operational Amplifier AC Specifications and Applications"*, DS00723

AN884: *"Driving Capacitive Loads With Op Amps"*, DS00884

AN990: *"Analog Sensor Conditioning Circuits – An Overview"*, DS00990

AN1177: *"Op Amp Precision Design: DC Errors"*, DS01177

AN1228: *"Op Amp Precision Design: Random Noise"*, DS01228

AN1258: *"Op Amp Precision Design: PCB Layout Techniques"*, DS01258

These application notes and others are listed in the design guide:

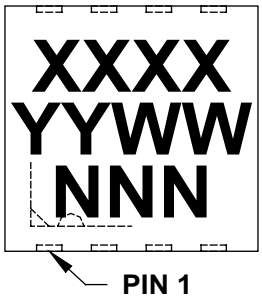
"Signal Chain Design Guide", DS21825

NOTES:

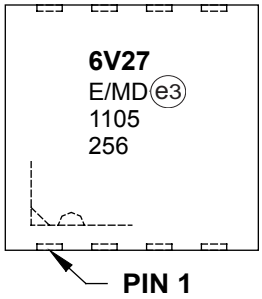
6.0 PACKAGING INFORMATION

6.1 Package Marking Information

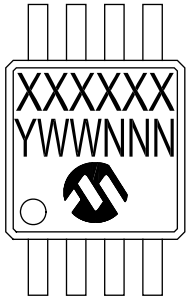
8-Lead DFN (4x4 mm)



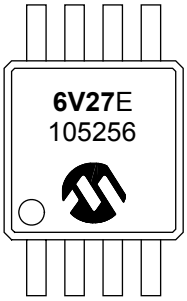
Example



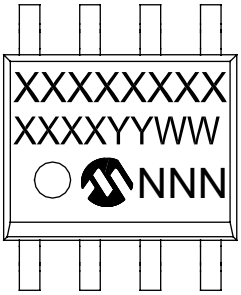
8-Lead MSOP



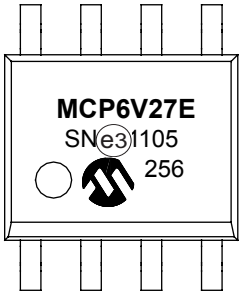
Example



8-Lead SOIC (150 mil)



Example

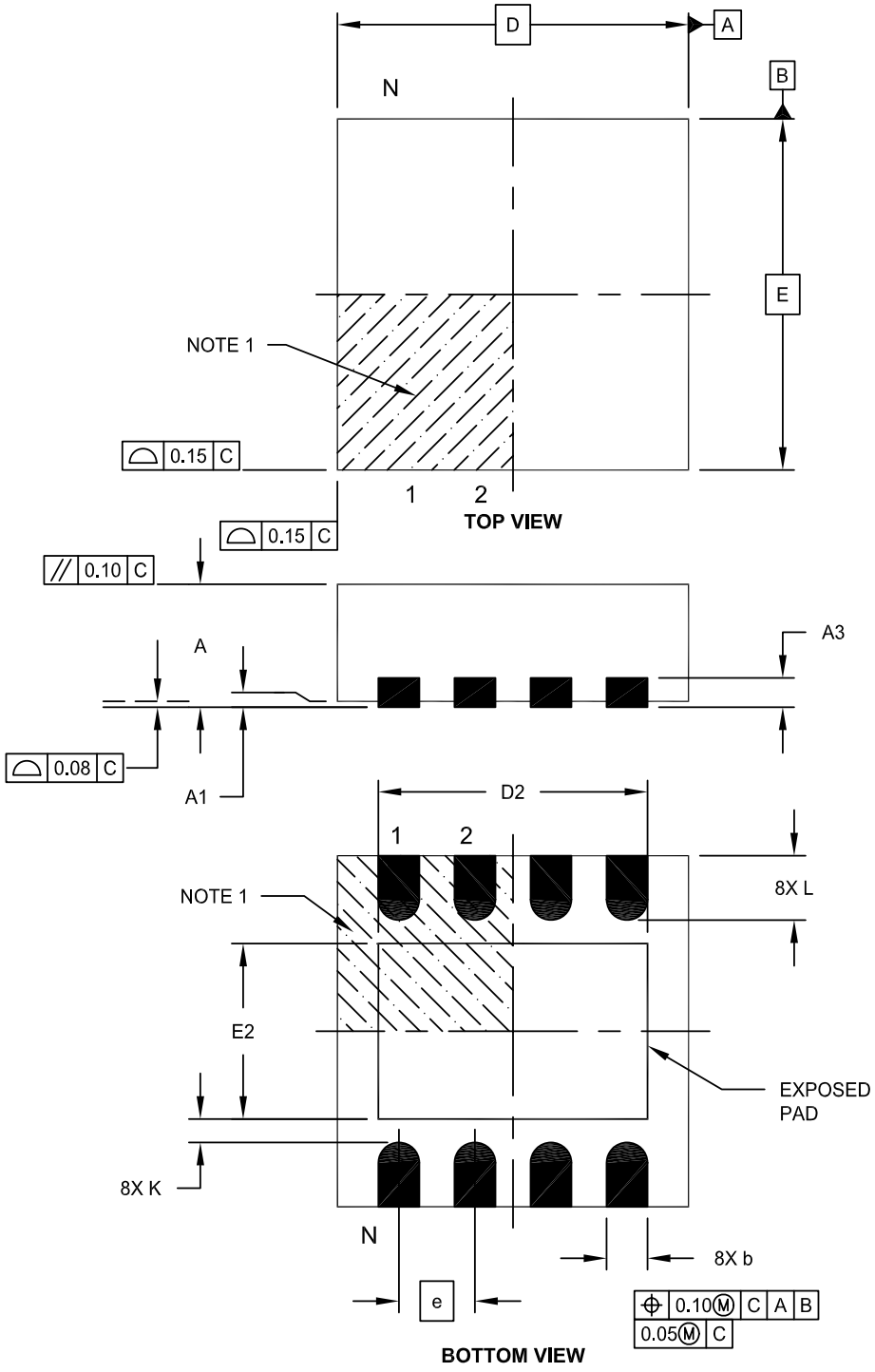


Legend:	XX...X	Customer-specific information
	Y	Year code (last digit of calendar year)
	YY	Year code (last 2 digits of calendar year)
	WW	Week code (week of January 1 is week ‘01’)
	NNN	Alphanumeric traceability code
	(e3)	Pb-free JEDEC designator for Matte Tin (Sn)
	*	This package is Pb-free. The Pb-free JEDEC designator ((e3)) can be found on the outer packaging for this package.

Note: In the event the full Microchip part number cannot be marked on one line, it will be carried over to the next line, thus limiting the number of available characters for customer-specific information.

8-Lead Plastic Dual Flat, No Lead Package (MD) – 4x4x0.9 mm Body [DFN]

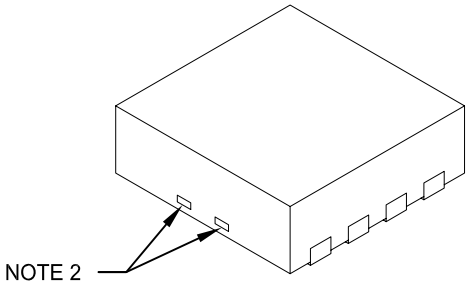
Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



Microchip Technology Drawing C04-131E Sheet 1 of 2

8-Lead Plastic Dual Flat, No Lead Package (MD) – 4x4x0.9 mm Body [DFN]

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



Units		MILLIMETERS		
Dimension Limits		MIN	NOM	MAX
Number of Pins	N		8	
Pitch	e		0.80 BSC	
Overall Height	A	0.80	0.90	1.00
Standoff	A1	0.00	0.02	0.05
Contact Thickness	A3		0.20 REF	
Overall Length	D		4.00 BSC	
Exposed Pad Width	E2	2.60	2.70	2.80
Overall Width	E		4.00 BSC	
Exposed Pad Length	D2	3.40	3.50	3.60
Contact Width	b	0.25	0.30	0.35
Contact Length	L	0.30	0.40	0.50
Contact-to-Exposed Pad	K	0.20	-	-

Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.
2. Package may have one or more exposed tie bars at ends.
3. Package is saw singulated
4. Dimensioning and tolerancing per ASME Y14.5M

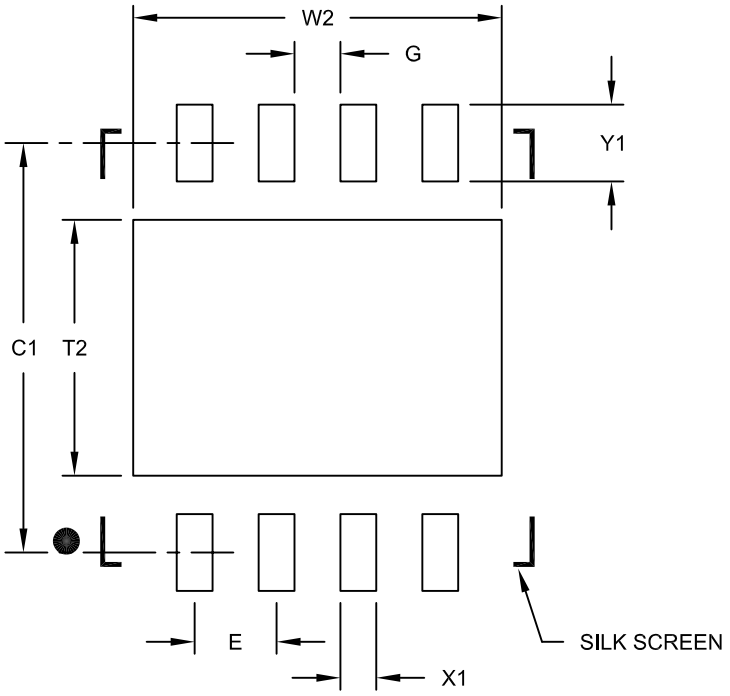
   BSC: Basic Dimension. Theoretically exact value shown without tolerances.

   REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing C04-131E Sheet 2 of 2

8-Lead Plastic Dual Flat, No Lead Package (MD) - 4x4x0.9 mm Body [DFN]

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



RECOMMENDED LAND PATTERN

Units		MILLIMETERS		
Dimension Limits		MIN	NOM	MAX
Contact Pitch	E		0.80 BSC	
Optional Center Pad Width	W2			3.60
Optional Center Pad Length	T2			2.50
Contact Pad Spacing	C1		4.00	
Contact Pad Width (X8)	X1			0.35
Contact Pad Length (X8)	Y1			0.75
Distance Between Pads	G	0.45		

Notes:

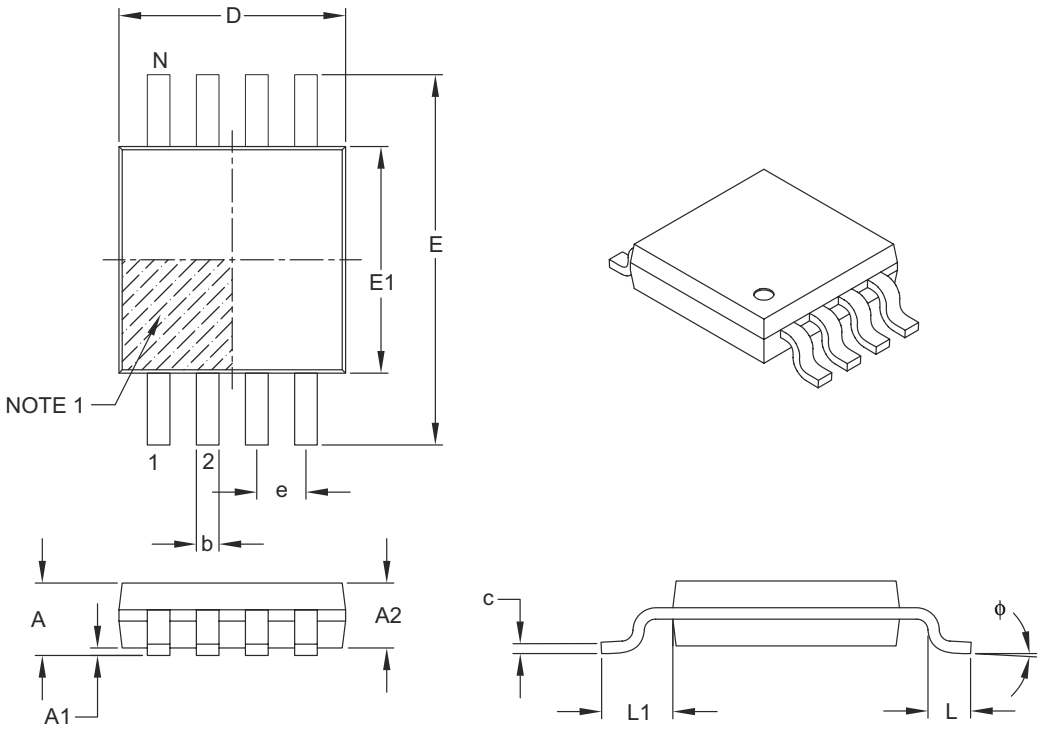
1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2131C

8-Lead Plastic Micro Small Outline Package (MS) [MSOP]

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



Units		MILLIMETERS		
Dimension Limits		MIN	NOM	MAX
Number of Pins	N		8	
Pitch	e		0.65 BSC	
Overall Height	A	–	–	1.10
Molded Package Thickness	A2	0.75	0.85	0.95
Standoff	A1	0.00	–	0.15
Overall Width	E		4.90 BSC	
Molded Package Width	E1		3.00 BSC	
Overall Length	D		3.00 BSC	
Foot Length	L	0.40	0.60	0.80
Footprint	L1		0.95 REF	
Foot Angle	ϕ	0°	–	8°
Lead Thickness	c	0.08	–	0.23
Lead Width	b	0.22	–	0.40

Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.
2. Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.15 mm per side.
3. Dimensioning and tolerancing per ASME Y14.5M.

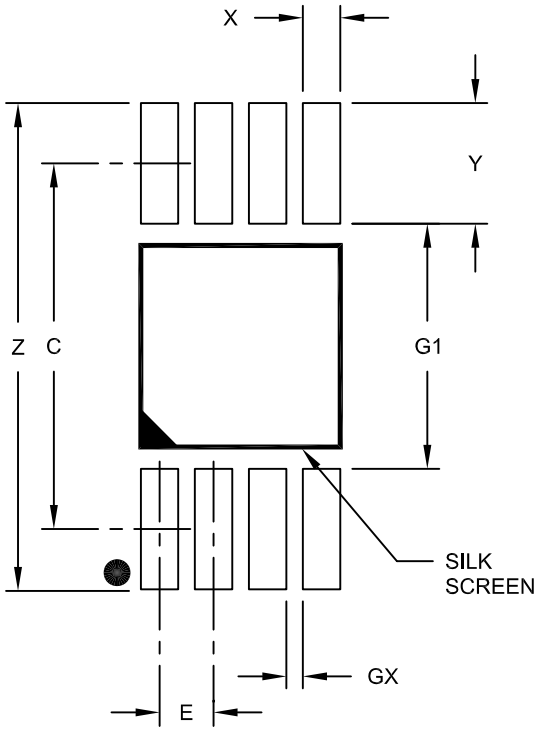
BSC: Basic Dimension. Theoretically exact value shown without tolerances.

REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing C04-111B

8-Lead Plastic Micro Small Outline Package (MS) [MSOP]

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



RECOMMENDED LAND PATTERN

Units		MILLIMETERS		
Dimension Limits		MIN	NOM	MAX
Contact Pitch	E		0.65 BSC	
Contact Pad Spacing	C		4.40	
Overall Width	Z			5.85
Contact Pad Width (X8)	X1			0.45
Contact Pad Length (X8)	Y1			1.45
Distance Between Pads	G1	2.95		
Distance Between Pads	GX	0.20		

Notes:

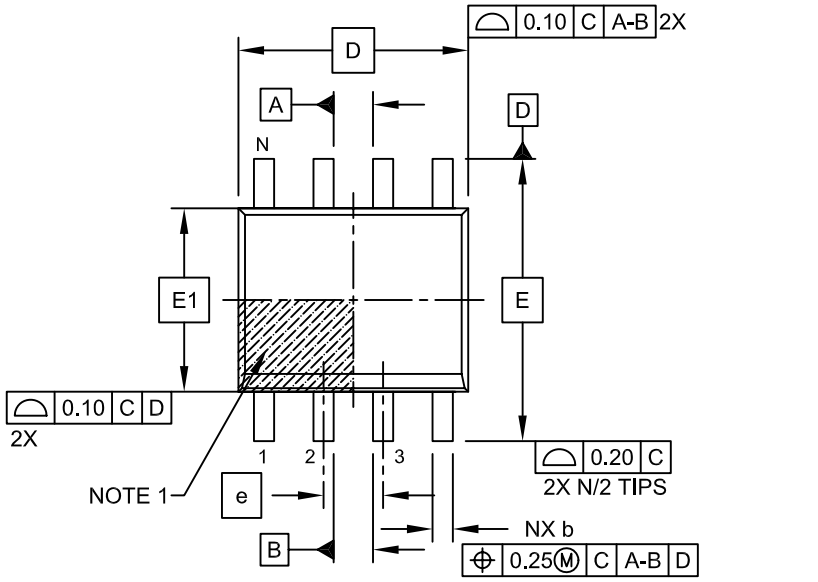
1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

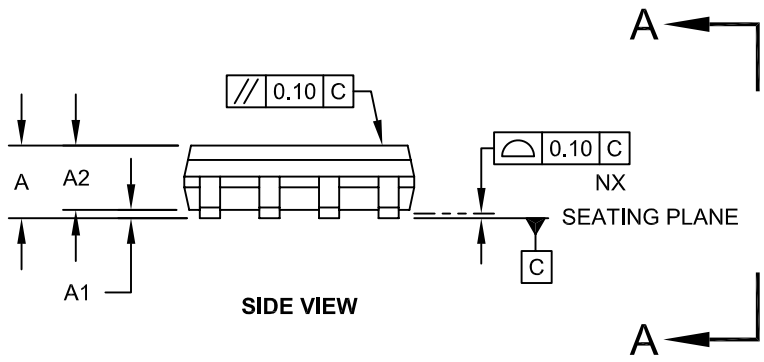
Microchip Technology Drawing No. C04-2111A

8-Lead Plastic Small Outline (SN) - Narrow, 3.90 mm Body [SOIC]

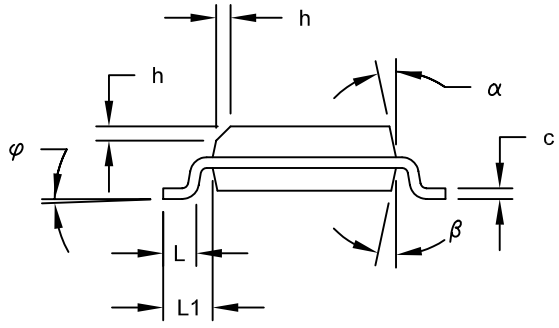
Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



TOP VIEW



SIDE VIEW

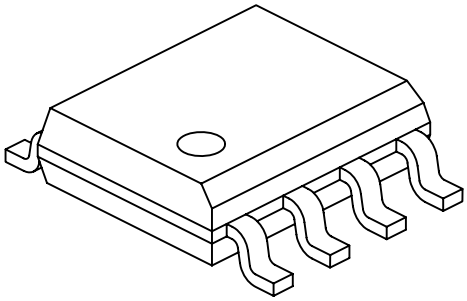


VIEW A-A

Microchip Technology Drawing No. C04-057C Sheet 1 of 2

8-Lead Plastic Small Outline (SN) - Narrow, 3.90 mm Body [SOIC]

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



Units		MILLIMETERS		
Dimension Limits		MIN	NOM	MAX
Number of Pins	N		8	
Pitch	e		1.27 BSC	
Overall Height	A	-	-	1.75
Molded Package Thickness	A2	1.25	-	-
Standoff §	A1	0.10	-	0.25
Overall Width	E		6.00 BSC	
Molded Package Width	E1		3.90 BSC	
Overall Length	D		4.90 BSC	
Chamfer (Optional)	h	0.25	-	0.50
Foot Length	L	0.40	-	1.27
Footprint	L1		1.04 REF	
Foot Angle	φ	0°	-	8°
Lead Thickness	c	0.17	-	0.25
Lead Width	b	0.31	-	0.51
Mold Draft Angle Top	α	5°	-	15°
Mold Draft Angle Bottom	β	5°	-	15°

Notes:

1. Pin 1 visual index feature may vary, but must be located within the hatched area.
2. § Significant Characteristic
3. Dimensions D and E1 do not include mold flash or protrusions. Mold flash or protrusions shall not exceed 0.15mm per side.
4. Dimensioning and tolerancing per ASME Y14.5M

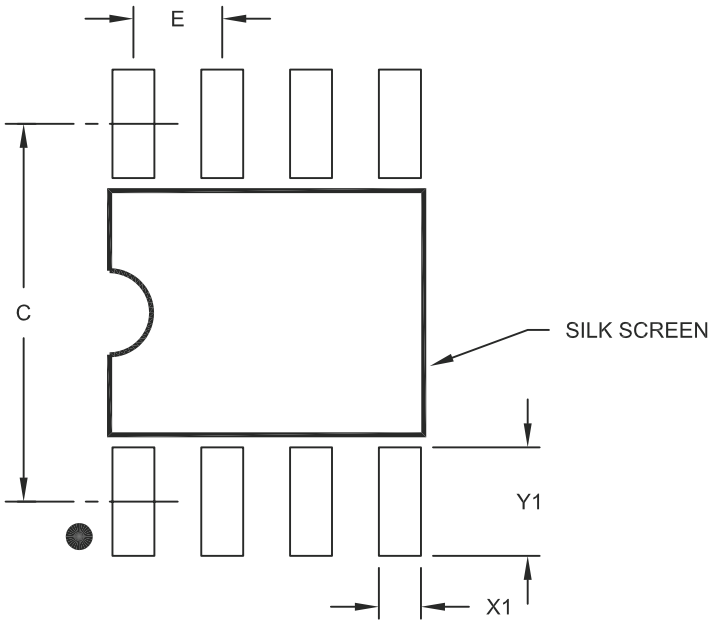
   BSC: Basic Dimension. Theoretically exact value shown without tolerances.

   REF: Reference Dimension, usually without tolerance, for information purposes only.

Microchip Technology Drawing No. C04-057C Sheet 2 of 2

8-Lead Plastic Small Outline (SN) – Narrow, 3.90 mm Body [SOIC]

Note: For the most current package drawings, please see the Microchip Packaging Specification located at http://www.microchip.com/packaging



RECOMMENDED LAND PATTERN

Units		MILLIMETERS		
Dimension Limits		MIN	NOM	MAX
Contact Pitch	E		1.27 BSC	
Contact Pad Spacing	C		5.40	
Contact Pad Width (X8)	X1			0.60
Contact Pad Length (X8)	Y1			1.55

Notes:

1. Dimensioning and tolerancing per ASME Y14.5M

BSC: Basic Dimension. Theoretically exact value shown without tolerances.

Microchip Technology Drawing No. C04-2057A

NOTES:

APPENDIX A: REVISION HISTORY

Revision A (March 2011)

- Original Release of this Document.

APPENDIX B: OFFSET RELATED TEST SCREENS

Input offset voltage related specifications in the DC spec table (Table 1-1) are based on bench measurements (see **Section 2.1 "DC Input Precision"**). These measurements are much more accurate because:

- More compact circuit
- Soldered parts on the PCB (to validate other measurements)
- More time spent averaging (reduces noise)
- Better temperature control
  - Reduced temperature gradients
  - Greater accuracy

We use production screens to ensure the quality of our outgoing products. These screens are set at wider limits to eliminate any fliers; see Table B-1.

TABLE B-1: OFFSET RELATED TEST SCREENS

Electrical Characteristics: Unless otherwise indicated, T_A = +25°C, V_{DD} = +2.3V to +5.5V, V_{SS} = GND, V_{CM} = V_{DD}/3, V_{OUT} = V_{DD}/2, V_L = V_{DD}/2 and R_L = 10 kΩ to V_L (refer to Figure 1-4 and Figure 1-5).					
Parameters	**Sym**	**Min**	**Max**	**Units**	**Conditions**
Input Offset					
Input Offset Voltage	V_{OS}	-10	+10	µV	T_A = +25°C **(Note 1, Note 2)**
Input Offset Voltage Drift with Temperature (linear Temp. Co.)	TC_1	—	—	nV/°C	T_A = -40 to +125°C **(Note 3)**
Power Supply Rejection	PSRR	115	—	dB	**(Note 1)**
Common Mode					
Common Mode Rejection	CMRR	106	—	dB	V_{DD} = 2.3V, V_{CM} = -0.15V to 2.5V **(Note 1)**
	CMRR	116	—	dB	V_{DD} = 5.5V, V_{CM} = -0.15V to 5.7V **(Note 1)**
Open-Loop Gain					
DC Open-Loop Gain (large signal)	A_{OL}	114	—	dB	V_{DD} = 2.3V, V_{OUT} = 0.2V to 2.1V **(Note 1)**
	A_{OL}	122	—	dB	V_{DD} = 5.5V, V_{OUT} = 0.2V to 5.3V **(Note 1)**

Note 1: Due to thermal junctions and other errors in the production environment, these specifications are only screened in production.

2: V_{OS} is also sample screened at +125°C.

3: TC_1 is not measured in production.

PRODUCT IDENTIFICATION SYSTEM

To order or obtain information, e.g., on pricing or delivery, refer to the factory or the listed sales office.

PART NO.	–X	/XX
Device	Temperature Range	Package

Device:	MCP6V27	Dual Op Amp
	MCP6V27T	Dual Op Amp (Tape and Reel)
Temperature Range:	E	= -40°C to +125°C
Package:	MD	= Plastic Dual Flat, No-Lead (4×4x0.9 mm), 8-lead
	MS	= Plastic Micro Small Outline Package, 8-lead
	SN	= Plastic SOIC (150 mil Body), 8-lead

Examples:

a) MCP6V27-E/MD: Extended temperature, 8LD 4x4 DFN package

b) MCP6V27T-E/MD: Tape and Reel Extended temperature, 8LD 4x4 DFN package

c) MCP6V27-E/MS: Extended temperature, 8LD MSOP package

d) MCP6V27T-E/MS: Tape and Reel, Extended temperature, 8LD MSOP package.

e) MCP6V27-E/SN: Extended temperature, 8LD SOIC package.

f) MCP6V27T-E/SN: Tape and Reel, Extended temperature, 8LD SOIC package.

NOTES:

Note the following details of the code protection feature on Microchip devices:

- Microchip products meet the specification contained in their particular Microchip Data Sheet.
- Microchip believes that its family of products is one of the most secure families of its kind on the market today, when used in the intended manner and under normal conditions.
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