



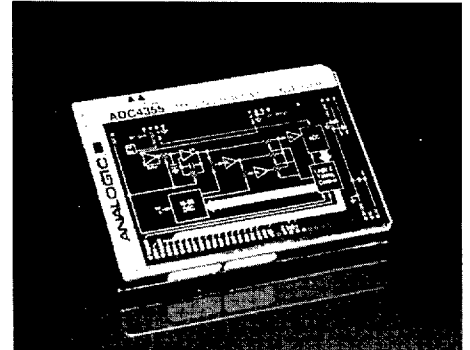
Low Noise, Low distortion High Speed, 16-Bit Sampling A/D Converters

Designed for High Performance Applications

Introduction

The Analogic ADC435X series of products consists of high speed, low noise, low distortion, 16-bit A/D converters. The ADC4355 and ADC4357 are sampling A/D converters that have throughput rates of 100 kHz and 200 kHz respectively; the ADC4356 is a 7 μ s buffered A/D converter. Designed for high performance applications, they are pin-compatible to the industry standard Analogic MP2735A and AM40516 A/D converters. The ADC435X converters are ideally suited for applications where high speed, true 16-bit linearity, and excellent frequency domain features are a must, such as spectroscopy, professional digital audio, telecommunications, ATE, and medical imaging.

The ADC435X series features excellent differential nonlinearity of $\pm 1/2$ LSB, a low 35 μ V RMS noise, and optional bipolar or unipolar 10V input ranges. The ADC435X series utilizes a 3-pass subranging architecture that both minimizes parts count and yields unprecedented stability, linearity, and accuracy. To achieve its superior performance, the ADC435X relies on a proprietary reference D/A converter that has inherent 16-bit accuracy and linearity. Use of a CMOS flash A/D converter eliminates the -5 V requirement, an inconvenience in most high speed 16-bit ADCs. With TTL and CMOS compatibility, tri-state data outputs, self-contained reference and timing circuitry, the ADC435X series offers easy system integration conveniently packaged in a 3" x 4" fully-shielded module.



Features

- ┆ 16-Bit Resolution
- ┆ No Missing Codes
- ┆ Wide Dynamic Range: 96 dB
- ┆ Signal to Noise Ratio: 95 dB
- ┆ Peak Distortion: -110 dB (1 kHz)
- ┆ Total Harmonic Distortion: -103 dB (1 kHz)
- ┆ ± 0.5 LSB Differential Non-Linearity
- ┆ 200 kHz Throughput Rate (ADC4357)
- ┆ 100 kHz Throughput Rate (ADC4355)
- ┆ Ease of Use
- ┆ Built-In S/H Amplifier (ADC4355/57)
- ┆ TTL Compatibility
- ┆ No -5 V Requirement
- ┆ High Input Impedance
- ┆ Electromagnetic/Electrostatic Shielding

Applications

- ┆ Professional Audio Encoding
- ┆ Digital Telecommunications
- ┆ Automatic Test Equipment
- ┆ High-Resolution Imaging
- ┆ Spectroscopy
- ┆ Medical Data Acquisition
- ┆ Satellite Communications
- ┆ Multiplexed Data Acquisition

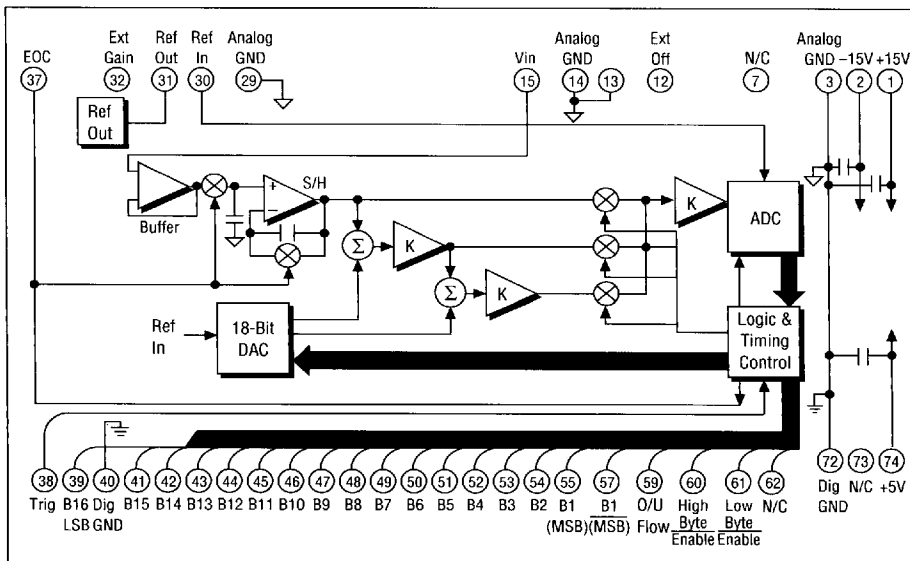


Figure 1. ADC4355/ADC4356/ADC4357 Functional Block Diagram and Pin-Out.

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ADC4355/ADC4356/ ADC4357

Specifications ⁽¹⁾

| | ADC4355/ADC4356 | | | ADC4357 | | | |
|---------------------------------------|---|----------------|-----------|--|----------------|-------|------------|
| | Min. | Typ. | Max. | Min. | Typ. | Max. | Units |
| ANALOG INPUT | | | | | | | |
| Input Range ⁽²⁾ | | | | | | | |
| Unipolar | 0 | | +10 | 0 | | +10 | V |
| Bipolar | -5 | | +5 | -5 | | +5 | V |
| Input Bias Current | | 0.5 μ A | 2 μ A | | 1 nA | 50 nA | |
| Input Capacitance | | 10 | | | 10 | | pF |
| Input Resistance | 100 | | | 100 | | | M Ω |
| Max. Input without Damage | | \pm Supplies | | | \pm Supplies | | |
| DIGITAL INPUTS | | | | | | | |
| Logic Levels | LSTTL/CMOS-Compatible | | | LSTTL/CMOS-Compatible | | | |
| Logic "0" | | | 0.8 | | | 0.8 | V |
| Logic "1" | 2.0 | | | 2.0 | | | V |
| Trigger | Positive Edge Triggered | | | Positive Edge Triggered | | | |
| Loading | | | 1 | | | 1 | LSTTL |
| Pulse Width | 50 | | | 50 | | | ns |
| High Byte Enable | Active Low, B1-B8, $\overline{B1}$ | | | Active Low, B1-B8, $\overline{B1}$ | | | |
| Low Byte Enable | Active Low, B9-B16 | | | Active Low, B9-B16 | | | |
| Propagation Delay with 1 TTL Load | | 20 | 50 | | 20 | 50 | ns |
| DIGITAL OUTPUTS | | | | | | | |
| Logic Levels | | | | | | | |
| Logic "0" | | | +0.4 | | | +0.4 | V |
| Logic "1" | +2.4 | | | +2.4 | | | V |
| Fan-Out | | | 1 | | | 0.1 | TTL Load |
| Output Coding | Binary Offset, Binary, 2's Complement, Complementary Data (see ordering guide) | | | Binary Offset, Binary, 2's Complement Complementary Data (see ordering guide) | | | |
| End of Conversion (EOC) | High during conversion, data valid 10 ns min. prior to falling edge | | | High during conversion, data valid 10 ns min. prior to falling edge | | | |
| Over/Under Flow | Active high at \pm FS, not tri-stateable | | | Active high at \pm FS, not tri-stateable | | | |
| REFERENCE | | | | | | | |
| Voltage Output Load ⁽³⁾ | | -6.5 | 1 | | -6.5 | 1 | V mA |
| Input Loading | | | | | | | |
| \pm 5V Input | 720 Ω // 10 μ F, -1.5 mA typ. | | | 720 Ω // 10 μ F, -1.5 mA typ. | | | |
| 0V to +10V Input | 607 Ω // 10 μ F, -3.5 mA typ. | | | 607 Ω // 10 μ F, -3.5 mA typ. | | | |
| Max Input W/O Damage | +0.5 | | -8.5 | +0.5 | | -8.5 | V |
| DYNAMIC CHARACTERISTICS | | | | | | | |
| Maximum Throughput Rate | 100 | | | 200 | | | kHz |
| A/D Conversion Time | 7 | | | | 4 | | μ s |
| S/H Acquisition Time | | 3 | | | 1 | | μ s |
| S/H Aperture Delay | | 30 | 60 | | 30 | 60 | ns |
| S/H Aper. Jitter | | 200 | 400 | | 100 | 200 | ps / ns |
| S/H Feedthrough ⁽⁴⁾ | | -96 | -90 | | -96 | -90 | dB |
| Sig. to Noise Ratio ⁽⁵⁾ | 92 | 95 | | 86 | 90 | | dB |
| Peak Distortion ⁽⁶⁾ | | | | | | | |
| \pm 5V Input @ 1 kHz | | -110 | -100 | | | | dB |
| \pm 5V Input @ 10 kHz | | | | | -100 | -95 | dB |
| \pm 5V Input @ 20 kHz | | -105 | -96 | | | | dB |
| \pm 5V Input @ 80 kHz | | | | | -90 | | dB |
| Total Harm. Dist. ⁽⁷⁾ | | | | | | | |
| \pm 5V Input @ 1 kHz | | -103 | -94 | | | | dB |
| \pm 5V Input @ 10 kHz | | | | | -94 | -88 | dB |
| \pm 5V Input @ 20 kHz | | -100 | -94 | | | | dB |
| \pm 5V Input @ 80 kHz | | | | | -87 | | dB |

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| ADC4355/ADC4356 | | | | ADC4357 | | | |
|------------------------------------|-----------------------------|-------|--------|-----------------------------|------|--------|------------|
| | Min. | Typ. | Max. | Min. | Typ. | Max. | Units |
| TRANSFER CHARACTERISTICS | | | | | | | |
| Resolution | 16 | | | 16 | | | Bits |
| Quantization Error | | | ±0.5 | | | ±0.5 | LSB |
| Int. Nonlinearity | | | ±0.003 | | | ±0.003 | % FSR |
| Diff. Nonlinearity | | ±0.25 | ±0.5 | | ±0.5 | ±0.75 | LSB |
| No Missing Codes | Guaranteed from 0°C to 60°C | | | Guaranteed from 0°C to 60°C | | | |
| Offset Error ⁽⁸⁾ | | | ±1 | | | ±1 | mV |
| Gain Error ⁽⁸⁾ | | | ±0.01 | | | ±0.01 | % FSR |
| Noise | | | | | | | |
| ADC4355 | | 35 | | | | | µV rms |
| ADC4356 | | 25 | | | | | µV rms |
| ADC4357 | | | | | 60 | | µV rms |
| External Offset Adjust | | 7.6 | | | 7.6 | | mV/V |
| External Gain Adjust | | 3.3 | | | 3.3 | | mV/V |
| STABILITY (0°C TO 60°C) | | | | | | | |
| Differential Nonlinearity | | | ±0.5 | | | ±0.5 | ppm /°C |
| Offset Voltage | | | ±10 | | | ±10 | ppm FSR/°C |
| Gain | | | ±10 | | | ±10 | ppm FSR/°C |
| Warm-Up Time | | | 5 | | | 5 | Mins. |
| Supply Rejection | | | | | | | |
| Offset | | ±5 | ±10 | | ±5 | ±10 | ppm FSR/% |
| Gain | | ±5 | ±10 | | ±5 | ±10 | ppm FSR/% |
| POWER REQUIREMENTS ⁽¹⁰⁾ | | | | | | | |
| ±15V Supplies ⁽⁹⁾ | ±11.65 | | ±15.45 | ±11.65 | | ±15.45 | V |
| +5V Supply | +4.75 | | +5.25 | +4.75 | | +5.25 | V |
| ±15V Current Drain | | | | | | | |
| ADC4355 | | 58 | | | | | mA |
| ADC4356 | | 51 | | | | | mA |
| ADC4357 | | | | | 62 | | mA |
| +5V Current Drain | | 55 | | | 55 | | mA |
| Power Consumption | | | | | | | |
| ADC4355 | | 2.0 | | | | | W |
| ADC4356 | | 1.8 | | | | | W |
| ADC4357 | | | | | 2.2 | | W |
| ENVIRONMENTAL & MECHANICAL | | | | | | | |
| Temperature Range | | | | | | | |
| Rated Performance | 0 | | 60 | 0 | | 60 | °C |
| Storage | -25 | | 80 | -25 | | 80 | °C |
| Relative Humidity | | | | | | | |
| Non-condensing | 0 to 85 % up to 60°C | | | 0 to 85 % up to 60°C | | | |
| | Dimensions 3" x 4" x 0.44" | | | Dimensions 3" x 4" x 0.44" | | | |
| | (76.2 x 127 x 11.18 mm) | | | (76.2 x 127 x 11.18 mm) | | | |
| Shielding | Electromagnetic 5 Sides | | | Electromagnetic 5 Sides | | | |
| | Electrostatic 6 Sides | | | Electrostatic 6 Sides | | | |
| Case Potential | Ground | | | Ground | | | |

Specifications subject to change without notice.

Notes:

1. Unless otherwise noted, all specifications apply at 25°C and power supplies are ±15V and +5V.
2. See ordering guide for factory-set input ranges.
3. Reference load must remain constant during conversion. DC load 1mA max.
4. Measured with a 20 kHz full scale sine wave input.
5. Signal-to-Noise Ratio represents the ratio between the rms value of the signal and the total rms noise below the Nyquist Rate. The total rms noise is computed by: (1) summing the noise power in all frequency bins not correlated with the test signal; (2) estimating the total noise power contained in all harmonically related frequency bins; and (3) computing the rms noise from the sum of (1) and (2).
6. Peak Distortion represents the ratio between the highest spurious frequency component below the Nyquist rate and the signal. Note that in computing Peak Distortion, the estimated noise allocated to the harmonic frequency bins in computing SNR is first removed. See Note 5.

7. Total Harmonic Distortion represents the ratio between the rms sum of all harmonics up to the 100th harmonic and the rms value of the signal. Note that in computing THD, the estimated noise allocated to the harmonic frequency bins in computing SNR is first removed. See Note 5.
8. Externally adjustable to zero.
9. For the 0V to +10V input voltage range, the minimum analog supply voltage is ±14.55V.
10. Analogic highly recommends the use of linear power supplies with its high performance, high resolution A/D converters. However, if system requirements provide only a +5V supply and limited space, the use of the Analogic SP7015 DC-to-DC converter will provide a low noise solution which will not degrade the ADC4355/ADC4356/ADC4357 performance.

SPECIFICATIONS

Output Coding and Trim Procedure

Figure 2 shows the output coding of the ADC435X A/D converter. The symbol * in Figure 2 indicates a bit that is undergoing a 0/1 or 1/0 code transition at the indicated analog input voltage.

To trim the offset of the ADC435X, apply 76 μ V to the analog input. Adjust the offset trim potentiometer such that the digital output corresponds to the truth table of Figure 2.

To trim the gain of the ADC435X apply +4.999924V for the bipolar option or +9.999772V for the unipolar option. Adjust the gain trim potentiometer such that the digital output corresponds to the truth table of Figure 2.

In addition to the internal offset and gain potentiometers, provisions have been made to externally null out DC errors by use of potentiometers or DACs. A 10V swing from a DAC on Pin 12 produces a 33 mV offset shift; a 10V swing on Pin 32 produces a 76 mV gain shift.

Timing Considerations

The timing diagram of Figure 3 shows the timing characteristics of the ADC435X A/D converter. Numbers in parentheses are figures for the ADC4357. Upon a low-to-high transition of the trigger input, the EOC (end of conversion) line also switches high. The EOC line in turn switches the internal sample-and-hold amplifier to the Hold mode; the S/H amplifier remains in the Hold mode for the duration of the A/D conversion period. At the end of the 7 μ s (4 μ s) A/D conversion period, the EOC line goes low and switches the sample-and-hold amplifier to the Sample mode. At the 100 kHz (200 kHz) throughput rate shown in figure 3, the sample-and-hold amplifier then has 3 μ s (1 μ s) to sample (acquire) a new signal level for the next conversion cycle. The TTL-level Trigger input should have a minimum pulse width of 50 ns. Note that the data for a given conversion cycle becomes valid approximately 10 ns prior to the high-to-low transition of the EOC line.

Layout Considerations

Because of the extremely high resolution of the ADC435X A/D converter, it is necessary to pay careful attention to the printed circuit layout for the device. It is, for example, important to separate the analog and digital grounds and to return them separately to the system power supply. Digital grounds are often noisy or "glitchy", and these glitches can have adverse effects on the performance of a 16-bit A/D converter if they are introduced to the analog portions of the A/D converter's circuitry. At 16-bit resolution, the size of the voltage step between one code transition and the succeeding one, is only 153 μ V, so it is evident that any noise in the analog ground return can result in erroneous or missing codes. It is therefore important to configure a low-impedance ground-plane return on the printed circuit board. Note that the ground-potential metal case used for the ADC435X provides shielding against electromagnetic interference on five sides and against electrostatic interference on six sides.

| TRUTH TABLE | | | | |
|---------------|---------------------|-----|------------------------|----------|
| INPUT VOLTAGE | DIGITAL OUTPUTS | | | |
| | COMP. OFFSET BINARY | | STRAIGHT OFFSET BINARY | |
| | MSB | LSB | MSB | LSB |
| BIPOLAR | | | | |
| 5.000000V | 0000000000000000 | | | OVERFLOW |
| 4.999924V | 0000000000000000* | | | OVERFLOW |
| 4.999848V | 0000000000000001 | | 1111111111111111 | |
| +0.000152V | 0111111111111111 | | 1000000000000001 | |
| +0.000076V | ***** | | 100000000000000* | |
| 0.000000V | 1000000000000000 | | 1000000000000000 | |
| -4.999695V | 1111111111111110 | | 0000000000000010 | |
| -4.999771V | 111111111111111* | | 000000000000000** | |
| -4.999848V | 1111111111111111 | | 0000000000000001 | |
| -5.000000V | OVERFLOW | | 0000000000000000 | |
| UNIPOLAR | | | | |
| 9.999848V | 0000000000000000 | | 1111111111111111 | |
| 9.999772V | 0000000000000000* | | 111111111111111* | |
| 9.999695V | 0000000000000001 | | 1111111111111110 | |
| 5.000000V | 0111111111111111 | | 1000000000000000 | |
| 4.999924V | ***** | | ***** | |
| 4.999848V | 1000000000000000 | | 0111111111111111 | |
| 0.000152V | 1111111111111110 | | 0000000000000001 | |
| 0.000076V | 111111111111111* | | 000000000000000* | |
| 0.000000V | 1111111111111111 | | 0000000000000000 | |

Figure 2. Output coding for the ADC435X.

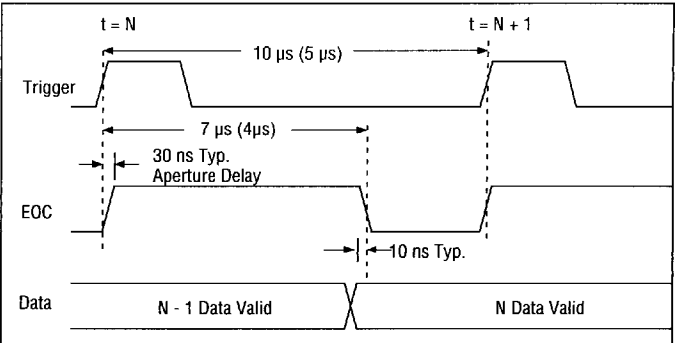


Figure 3. ADC435X Timing Diagram.

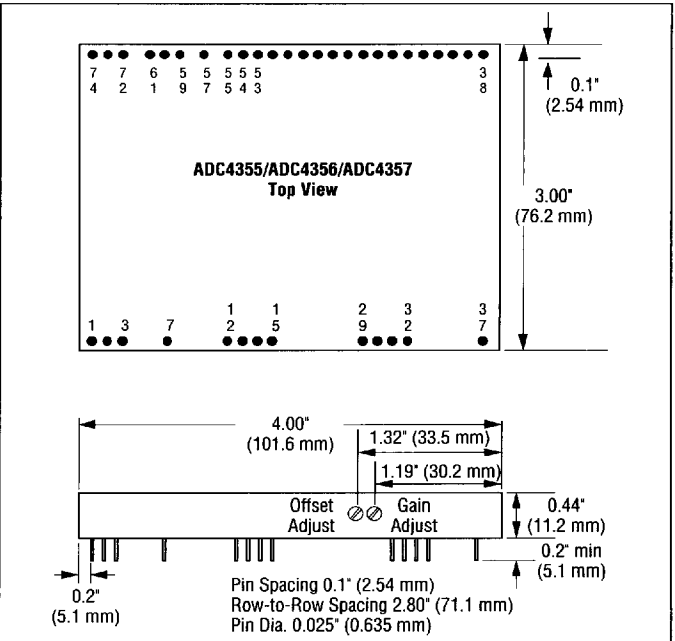


Figure 4. ADC435X Outline Drawing & Pinouts.

PRINCIPLES OF OPERATION

To understand the operating principles of the ADC435X A/D converter, refer to Figure 5. The simplified block diagrams in Paths a, b, and c in Figure 5 illustrate the three successive passes in the sub-ranging conversion scheme of the ADC435X. For all three passes, the lines labeled "From Input" come either from the output of the sample-and-hold amplifier (in the ADC4355/ADC4357) or from the output of the input buffer amplifier (in the ADC4356). In the first pass (a), a switched-gain amplifier attenuates the input signal by a factor of five. It thus converts the 10V full-scale range of the input to the 2V full-scale range of the 6-bit flash A/D converter. The 6-bit A/D converter then digitizes the six MSBs of the input signal. The outputs of the A/D converter drive the six MSBs of the D/A converter. Although not shown (for reasons of clarity) in Figure 5, the six output lines of the A/D converter are actually latched into the logic circuitry of a specialized gate array which drives the input lines of the D/A converter.

In the second pass (b), a difference amplifier subtracts the D/A converter's output voltage from the input voltage, then amplifies this difference by a factor of 3.2. The switched-gain amplifier now has a gain of two, and thus amplifies the difference voltage further. The output of the switched-gain amplifier again provides the input signal for the 6-bit flash A/D converter. The A/D converter's outputs are latched into the gate array which supplies the next lower-order bits of the D/A converter. In the gate array, the A/D converter's MSB in the second pass "overlaps" the LSB from the first pass. The resolution of the A/D conversion in the second pass is thus 11 bits (not 12).

In the third pass (c), the gain of 3.2 difference amplifier subtracts the D/A converter's output voltage from the input voltage. In this pass, an amplifier with a gain of 32 provides additional amplification of the difference signal. The six outputs of the 6-bit flash A/D converter are latched into the gate array; the MSB of this conversion cycle "overlaps" the LSB of the previous cycle. The effective resolution of the conversion is thus $5 + 5 + 6$, or 16 bits. Using the "overlap" structure, logic circuitry in the gate array adds the digital words produced in the three passes and produces the corrected output word. This digital error-correction technique thus provides an output word that is accurate and linear to within the full resolution of the A/D converter. The method helps to compensate for any gain and linearity errors in the amplifying circuitry as well as in the 6-bit flash A/D converter. Without the error-correction technique, it would be necessary that all the components in the ADC435X — the difference amplifier, the switched-gain amplifier, and the 6-bit flash A/D converter — be accurate and linear to a 16-bit level. While such a design might be possible to realize on a laboratory benchtop, it would be clearly impractical to achieve in production. The key to the ADC435X's conversion scheme is the 16-bit-linear D/A converter, which serves as a reference element for the conversion passes as well as for the error-correction mechanism.

The ADC435X has a tri-state output structure. Users can enable the eight MSBs, eight LSBs, or both by using the High-Byte Enable and Low-Byte Enable pins (both pins are active low). This feature makes it possible to transfer data from the ADC435X to an 8-bit microprocessor bus. However, to prevent the coupling of high frequency noise from the microprocessor bus into the A/D converter, the output data must be buffered; see Figure 10.

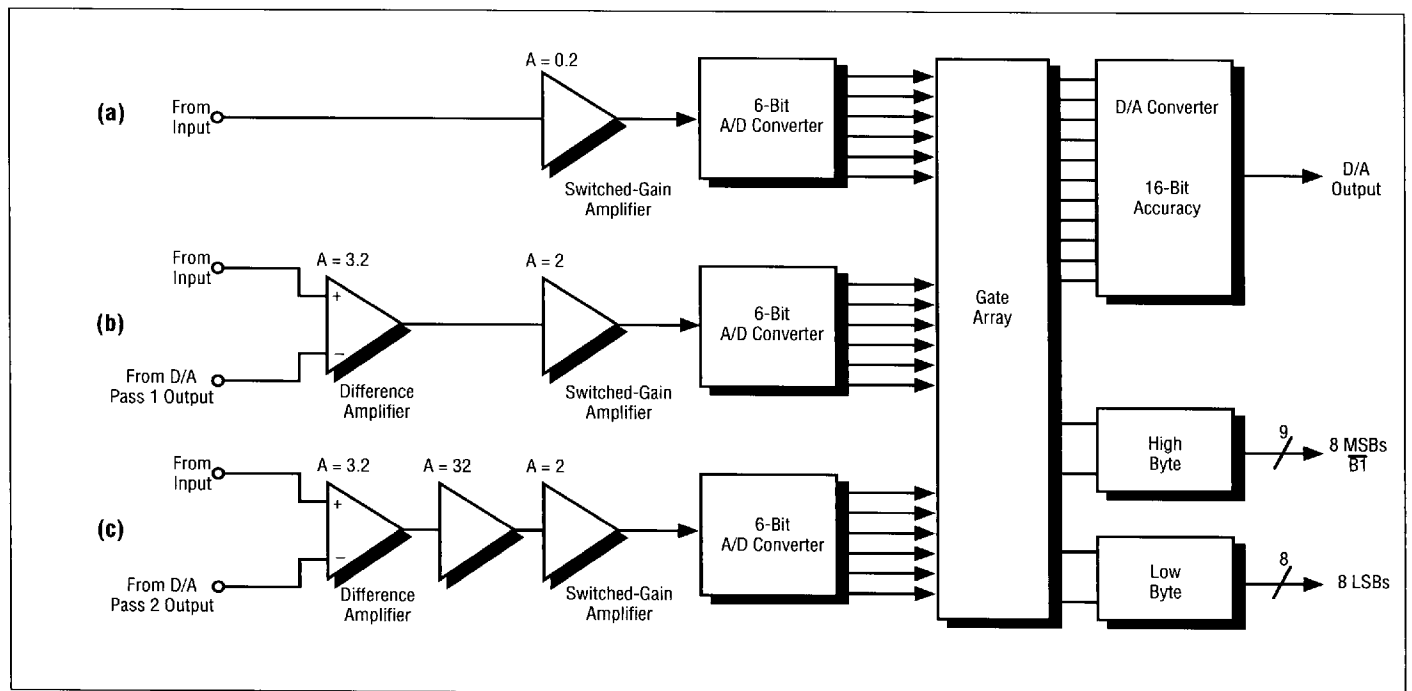


Figure 5. Operating Principle of the ADC435X.

PERFORMANCE TESTING

To further instill confidence in our customers, Analogic supplies a test data sheet with each ADC435X as proof of 100% testing performed on each device prior to shipping. Such data sheets reflect testing performed both in the "Frequency Domain" and in the "Amplitude Domain".

Amplitude Domain Testing

The Amplitude Domain Testing is performed by proprietary automatic test equipment that includes a 22-bit duty-cycle digital-to-analog converter. A simplified block diagram outlining our Amplitude Domain Test System is shown in Figure 6. The data sheet generated provides the end customer with detailed results on integral linearity, A/D converter noise, absolute accuracy, conversion time, power supply current and power supply rejection. A typical data sheet for the ADC4355 is shown in Figure 7. Analogic is meticulous not only in testing these parameters, but also in defining them so as not to mislead the customer. Following is a list of Analogic's major definitions as tested with our "Amplitude Domain" test systems.

A/D Converter Noise: Errors at the output code caused by signals present other than the signal source. In the ADC4355/ADC4357, A/D converter noise includes noise from the S/H and the A/D converter; in the ADC4356, A/D converter noise includes noise from the input buffer and the A/D converter.

Integral Linearity: A measure of the maximum deviation of the output digital codes from the best-fit straight line through the transfer function, expressed as a percentage of the full scale range. A least squares algorithm is used to determine best fit.

Differential Linearity: A measure of the maximum deviation of any particular code width from the ideal code width, expressed as a fraction of an LSB.

Differential Linearity =

$$\frac{V_{MAX} - V_{LSB}}{V_{LSB}} \text{ LSBs}$$

where: VMAX = maximum (or minimum) code width

Absolute Accuracy Error: A measure of the largest static difference between the actual output code and that predicted by the ideal transfer function, a worst case summation of all error sources, expressed as a percentage of full scale.

Absolute Accuracy measurements must be referenced to a standard traceable to the NIST with at least an order of magnitude more accuracy than the unit under test.

A/D Conversion Time: Time measured from the rising edge of TRIGGER (the time when the T/H goes into hold) to the falling edge of EOC. The maximum limit is based on allowing sampling rates up to 100 kHz including a T/H (200 kHz for the ADC4357).

Frequency Domain Testing

The Frequency Domain Testing is performed by means of proprietary automatic test equipment inclusive of an ultra-high speed Array Processor manufactured by Analogic. The power of the processor provides us with a great deal of flexibility in both gathering and formatting the data.

While a Rosenfeld window is applied on a standard basis, other types of windows such as Blackman-Harris and Blackman are available for customized testing. The number of samples can be varied from 512 to 8192, and the system can average up to 64 FFTs. A block diagram of the "Frequency Domain" test system is shown in Figure 8; a typical data sheet of an tested over frequency is shown in Figure 9.

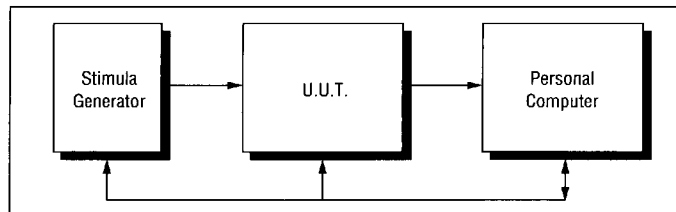


Figure 6. "Amplitude Domain" Test System.

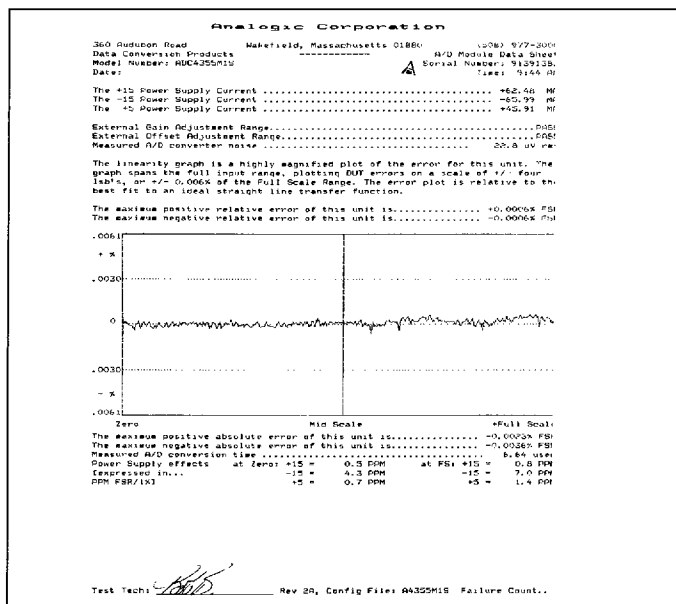


Figure 7. "Amplitude Domain" Data Sheet.

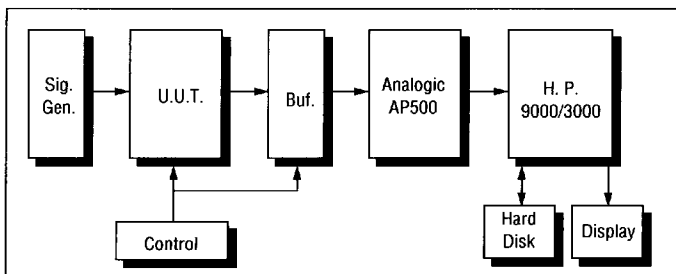


Figure 8. "Frequency Domain" Test System.

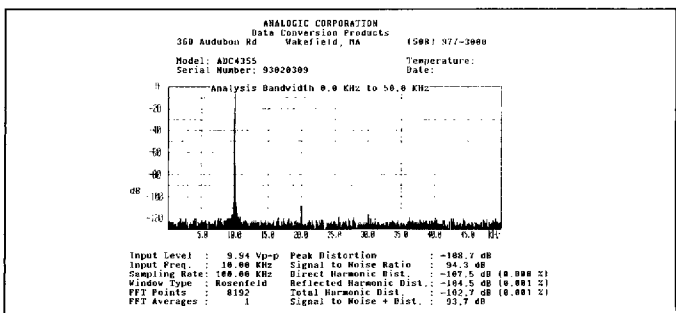


Figure 9. "Frequency Domain" Data Sheet.

TYPICAL APPLICATION

Figure 10 shows a typical application circuit for the ADC4356 16-bit A/D converter. This circuit provides simultaneous sampling of eight bipolar analog-input channels. Simultaneous sampling is a necessity in conversion systems in which the phase, as well as amplitude, relationship between different signals is an important parameter. One example is in seismic measurements, in which it is crucial to know the phase relationship between the signals generated by different sensors. This application circuit performs simultaneous sampling by "freezing" the signal levels of eight analog-input channels at the same instant of time. The differential multiplexer then presents these signal levels, either sequentially or in any user-programmed order, to the ADC4356 A/D converter via a differential amplifier. Although the input signals to this circuit are essentially single-ended, the use of a differential multiplexer and a differential amplifier eliminates the possibility of errors arising from common mode voltages.

The minicomputer or microprocessor in Figure 10 provides the sequence and timing information to the control logic. The control logic then performs the task of switching the sample-and-hold amplifiers from Sample to Hold mode and vice-versa, selecting the appropriate input channel and triggering the ADC4356 A/D converter. By using two resistors with each SHA2410 sample-and-hold amplifier, a user can program the SHA2410s to provide the gain required to match the input signals to the $\pm 5V$ full-scale range of the ADC4356 A/D converter. In the application circuit of Figure 10, for example, the four inputs shown have full-scale ranges of $\pm 1V$, $\pm 2V$, $\pm 3V$, and $\pm 5V$. The eighth input channel has the proper full-scale range of $\pm 5V$, so gain-setting resistors are not required. Because the SHA2410s provide the sample-and-hold function in this circuit, the ADC4356, which does not include a sample-and-hold amplifier, is an appropriate choice.

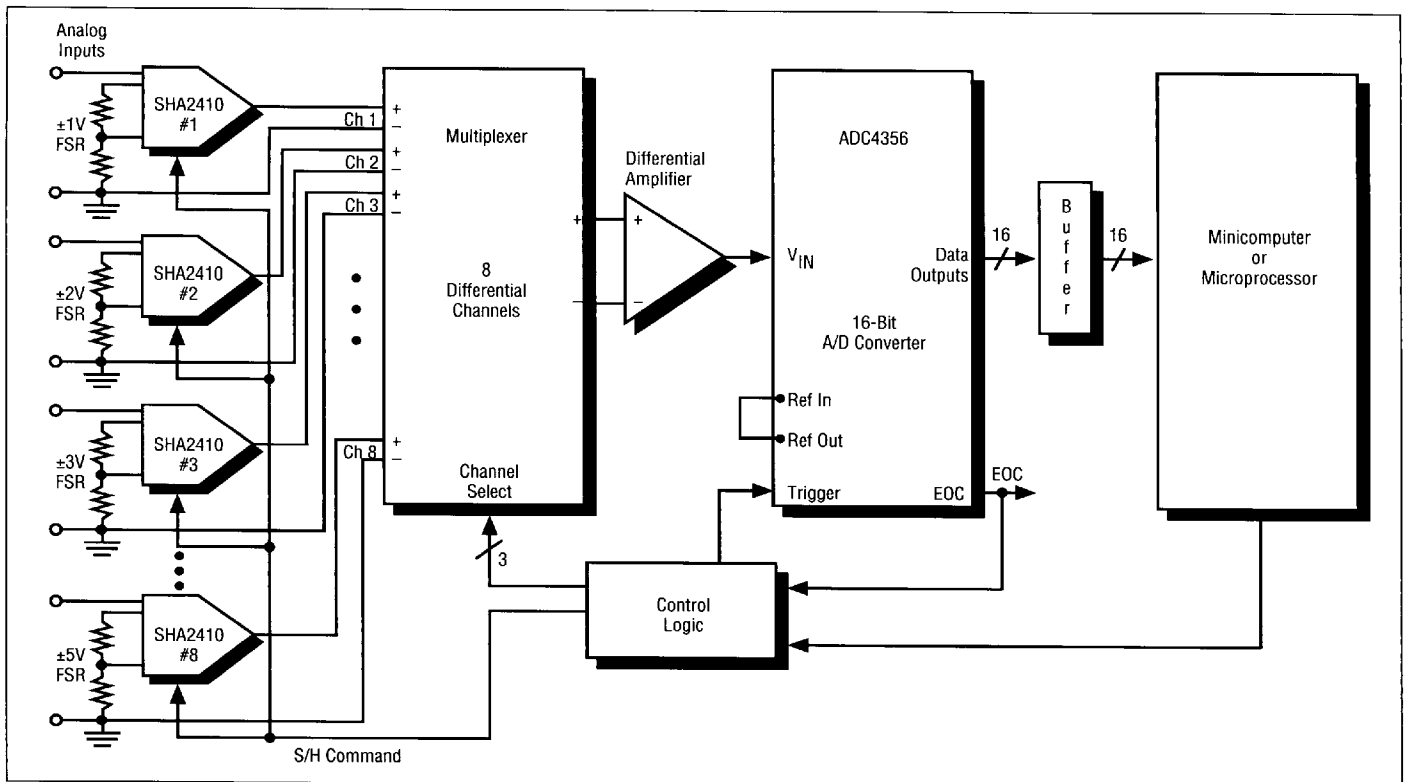


Figure 10. Typical Application Circuit for the ADC4356.

Ordering Guide

| | | ADC435 | -M |
|--------------------|----------------------------------|--------|--------|
| 5 | 100 kHz Sampling | _____ | _____ |
| 6 | 7 μ s Buffered A/D Converter | _____ | _____ |
| 7 | 200 kHz Sampling ADC | _____ | _____ |
| 1 | 0V to +10V Input | _____ | _____ |
| 4 | \pm 5V Input | _____ | _____ |
| S | Straight Data | _____ | _____ |
| C | Complementary Data | _____ | _____ |
| DC-to-DC Converter | | | SP7015 |

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