

# NJ8822, NJ8822B

# ELECTRICAL CHARACTERISTICS

Test conditions (unless otherwise stated):

$V_{DD}-V_{SS}$  5V  $\pm$  0.5V

Temperature range: NJ8822 -30°C to +70°C, NJ8822B -40°C to +85°C

T-50-09

## DC Characteristics at $V_{DD}$ = 5V

Characteristics	Value			Units	Conditions
	Min.	Typ.	Max.		
Supply current			5.5 1.5	mA mA	FOSC, FIN = 10MHz } 0 to 5V square wave FOSC, FIN = 1MHz }
<b>MODULUS CONTROL OUT</b>					
High level	4.6			V	$I_{source}$ 1mA
Low level			0.4	V	$I_{sink}$ 1mA
<b>LOCK DETECT OUT</b>					
Low level			0.4	V	$I_{sink}$ 4mA
Open drain pull-up voltage			8	V	
<b>PDB OUTPUT</b>					
High level	4.6			V	$I_{source}$ 5mA
Low level			0.4	V	$I_{sink}$ 5mA
3-state leakage			$\pm$ 0.1	$\mu$ A	

## AC Characteristics

Characteristics	Value			Units	Conditions
	Min.	Typ.	Max.		
FIN/OSC inputs	200			mV RMS	10MHz AC coupled sinewave
Max. operating freq. OSC/FIN inputs	10			MHz	$V_{DD}$ = 5V, Input squarewave $V_{DD}-V_{SS}$ , 25°C
Propagation delay, clock to modulus control		30	50	ns	Note 2
<b>Programming inputs</b>					
Clock high time, $t_{CH}$	0.5			$\mu$ s	All timing periods are referenced to the negative transition of the clock waveform
Clock low time, $t_{CL}$	0.5			$\mu$ s	
Enable set-up time, $t_{ES}$	0.2		$t_{CH}$	$\mu$ s	
Enable hold time, $t_{EH}$	0.2			$\mu$ s	
Data set-up time, $t_{DS}$	0.2			$\mu$ s	
Data hold time, $t_{DH}$	0.2			$\mu$ s	
Clock rise and fall times	0.2			$\mu$ s	
Positive going threshold, $V_{T+}$	3			V	Note 1
Negative going threshold, $V_{T-}$			2	V	
<b>Phase Detector</b>					
Digital phase detector propagation delay		500		ns	
Gain programming resistor, RB	5			k $\Omega$	Note 3
Hold capacitor, CH			1	nF	
Programming capacitor, CAP			1	nF	
Output resistance, PDA			5	k $\Omega$	

### NOTES

1. Data, Clock and Enable inputs are high impedance Schmitt buffers without ull up resistors. They are therefore not TTL compatible.
2. All counters have outputs directly synchronous with their respective clock rising edges.
3. The finite output resistance of the internal voltage follower and 'on' resistance of sample switch driving this pin will add a finite time-constant to the loop. A 1nF hold capacitor will give a maximum time-constant of 5 microseconds.
4. The inputs to the device should be at logic '0' when power is applied if latch up conditions are to be avoided. This includes the signal/osc. frequency inputs.

## ABSOLUTE MAXIMUM RATINGS

Supply voltage ( $V_{DD}-V_{SS}$ )	-0.5V to 7V	Storage temperature	-55°C to +125°C
Input voltage			(DP and MP packages, NJ8822)
Open drain O/P (pin 3 (DG) pin 4 (MP))	7V	Storage temperature	-65°C to +150°C
All other pins	$V_{SS}$ -0.3V to $V_{DD}$ +0.3V		(DG package, NJ8822B)

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T-50-09

PIN DESIGNATION

Pin No.		Name	Description
DG,DP	MP		
1	1	PDA	Analog output from the sample and hold phase comparator for use as a 'fine' error signal. Voltage increases as FV (FV is the output from the 'M' counter) phase lead increases and decreases as FR (FR is the output from the reference counter) phase lead increases. Output is linear over only a narrow phase window determined by gain (programmed by RB). In a type 2 loop, this pin is at $(V_{DD} - V_{SS})/2$ when the system is in lock.
-	3	N/C	Not connected.
2	2	PDB	Three-state output from the phase/frequency detector for use as a 'coarse' error signal. FV > FR or FV leading: positive pulses. FV < FR or FR leading: negative pulses. FV = FR and phase error within PDA window: high impedance.
3	4	LD	An open drain lock detect output at low level when phase error is within PDA window (in lock); high impedance at all other times.
4	5	FIN	The input to the main counters. It is normally driven from a prescaler which may be AC coupled or, when a full logic swing is available, may be DC coupled.
5	6	V <sub>SS</sub>	Negative supply (ground).
6	7	V <sub>DD</sub>	Positive supply (normally 5V).
-	8	N/C	Not connected.
7,8	9,10	OSC.IN/ OSC.OUT	These pins form an on-chip reference oscillator when a parallel resonant crystal is connected across them. Capacitors of an appropriate value are also required between each end of the crystal and ground to provide the necessary additional phase shift. The addition of a 220 ohm resistor between Pin 8 and the crystal will improve stability. An external reference signal may alternatively be applied to OSC.IN. This may be a low-level signal, AC coupled, or if a full logic swing is available it may be DC coupled. The program range of the reference counter is 3 to 2047 in steps of 1, with the division ratio being twice that programmed.
9	-	N/C	Not connected.
10	12	DATA	Information on this input is transferred to the internal latches during the appropriate data read time slot. Data is high for a '1' and low for a '0'. There are three data words which control the NJ8822, MSB is first in the order, 'A' - (7 bits), 'M' - (10 bits), 'R' - (11 bits).
11	13	CLK	Data is clocked in on the negative transition of the clock waveform. If less than 28 negative clock transitions have been received when the enable line goes low (i.e. only 'M' and 'A' will have been clocked in) then the 'R' counter latch will remain unchanged and only 'M' and 'A' will be transferred from the input shift register to the counter latches. This will protect the 'R' counter from being corrupted by any glitches on the clock line after only 'M' and 'A' have been loaded. If 28 negative transitions have been counted then the 'R' counter will be loaded with the new data.
12	14	ENABLE	When the enable is low the data and clock inputs are disabled internally. As soon as the enable is high the data and clock input are enabled and data may be clocked into the device. The data is transferred from the input shift register to the counter latches on the negative transition of the enable input and both inputs to the phase detector are synchronised to each other. Enable transitions only allowed when CLK is high.
13	15	CAP	This pin allows an external capacitor to be put in parallel with the ramp capacitor, and allows further programming of the device. (This capacitor is connected from CAP to V <sub>SS</sub> ).
14	16	MC	Output for controlling an external dual modulus prescaler. The modulus control level will be low at the beginning of a count cycle and will remain low until the 'A' counter completes its cycle. The modulus control then goes high and remains high until the 'M' counter completes its cycle at which point both counters are reset. This gives a total division ratio of $M \cdot N + A$ where N and N + 1 represent the dual modulus prescaler values. The program range of the 'A' counter is 0-127 and therefore can control prescalers with a division ratio up to and including $\div 128/129$ . The programming range of the 'M' counter is 3-1023 and for correct program operation $M \geq A$ . Where every possible channel is required, the minimum division ratio should be $N^2 - N$ .
15	17	RB	An external sample and hold phase comparator gain programming resistor should be connected between this pin and V <sub>SS</sub> .
16	18	CH	An external hold capacitor should be connected between this pin and V <sub>SS</sub> .

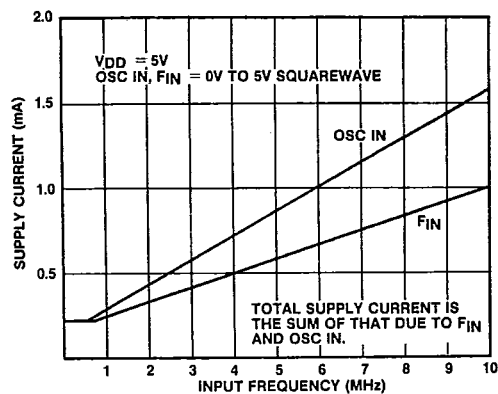


Fig.3 Typical supply current v. input frequency

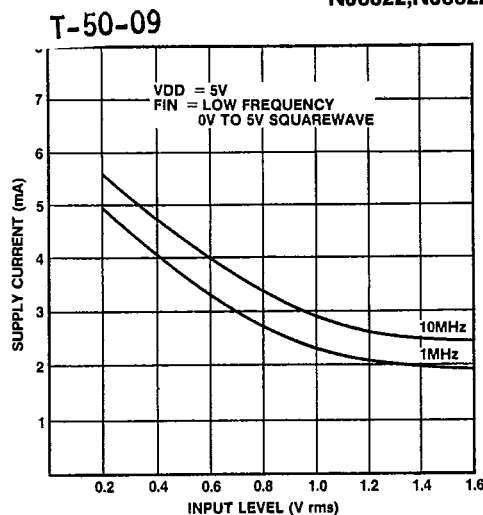


Fig.4 Typical supply current v. input level, Osc In

## PROGRAMMING

### Reference Divider Chain

The comparison frequency depends upon the crystal oscillator frequency and the division ratio of the R counter, which can be programmed in the range 3 to 2047.

$$R = \frac{f_{osc}}{2 \times f_{comp}}$$

ie where  $f_{comp}$  = comparison frequency

$f_{osc}$  = oscillator frequency

R = R counter ratio

For example where crystal frequency = 10MHz and a channel spacing comparison frequency of 12.5kHz is required,

$$R = \frac{10^7}{2 \times 12.5 \times 10^3} = 400$$

Thus the R register would be programmed to 400 expressed in binary.

NB The total divider range is from 6 to 4094 in steps of 2.

### VCO Divider Chain

The synthesised frequency of the voltage control oscillator (VCO) will depend on the division ratio of the M and A counters, the value of the external two modulus prescaler ( $N/N + 1$ ) and the value of the comparison frequency  $f_{comp}$ .

The division ratio  $P = NM + A$

where M is the ratio of the M counter in the range 3 to 1023

and A is the ratio of the A counter in the range 1 to 127.

Note  $M \geq A$

$$\text{Also } P + \frac{fv_{co}}{f_{comp}}$$

For example if the desired VCO frequency = 275MHz, the comparison frequency is 12.5kHz and a two modulus prescaler of  $\div 64/65$  is being used, then:

$$P = \frac{275 \times 10^6}{12.5 \times 10^3} = 22 \times 10^3$$

Now  $P = NM + A$

which can be rearranged to be  $P/N = M + A/N$

In our example we have

$$\frac{22 \times 10^3}{64} = M + \frac{A}{64} \text{ therefore } 343.75 = M + \frac{A}{64}$$

M is programmed to the integer part = 343 and A is programmed to the fractional part times 64

ie  $A = 0.75 \times 64 = 48$

NB The minimum ratio that can be used is  $N^2 - N$

To check  $P = 343 \times 64 + 48 = 22000$  which is the required divide ratio.

When re-programming, a reset to zero state is followed by reloading with the new counter values. This means the synthesiser loop lock up time will be well defined and less than 10msec. If shorter lock up times are required, when making only small changes in frequency, the non resettable version NJ8824 should be considered.

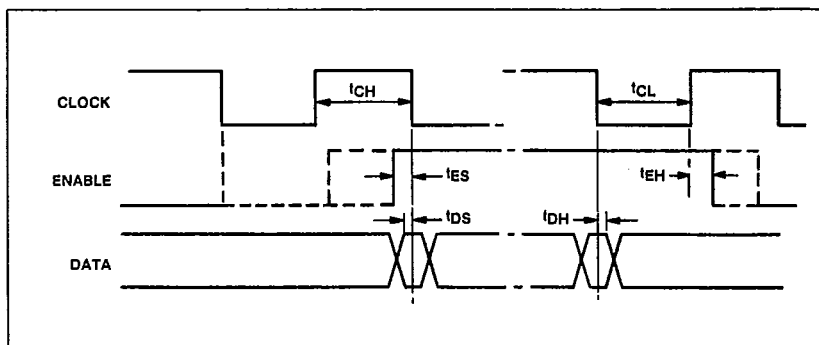


Fig.5 Timing diagram showing timing periods required for correct operation

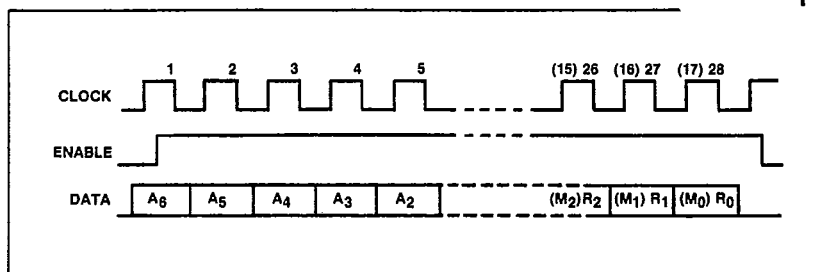


Fig.6 Timing diagram showing programming details

## PHASE COMPARATORS

Noise output from a synthesiser loop is related to loop gain  $K \cdot K_v / P$ , where  $K$  is phase detector constant (volts/rad),  $K_v$  is the VCO constant (rad-secs/volt) and  $P$  is the overall loop division ratio. When  $P$  is large and the loop gain is low, noise may be reduced by employing a phase comparator with a high gain. The sample and hold phase detector within the NJ8822 has both a high gain and uses a double sampling technique to reduce spurious outputs to a low level.

A standard digital phase/frequency detector driving a three-state output provides a 'coarse' error signal to enable fast switching between channels.

This output is active until the phase error is within the sample and hold phase detector window, when its output becomes high impedance. Phase-lock is indicated at this point with a low level on LD. The sample and hold phase detector provides a 'fine' error signal to give further phase adjustment and to hold the loop in lock.

An internally generated ramp controlled by the digital output from both the reference and main divider chains is sampled at the reference frequency to give the fine error signal, PDA. When in phase lock this output would typically be at  $(V_{DD} - V_{SS})/2$  and any offset from this would be proportional to phase error.

The relationship between this offset voltage and the phase error is the phase-comparator gain which is programmable with an external resistor,  $R_B$  and a capacitor,  $CAP$ .

An internal 50pF capacitor is used in the sample and hold comparator.

This gain is typically:

$$GAIN = \frac{10 [V_{DD} - V_{SS} - 0.7 - 89(R_B)^{-1/2}]}{2 \pi [CAP + 50 \times 10^{-12}] \times RB \times FR}$$

The value of

$R_B$  and  $CAP$  should be chosen to give the required gain at the reference frequency used. Fig.8 shows that to achieve a gain of 380V per radian at 10kHz requires  $R_B$  to be approximately 39k $\Omega$ ,  $CAP$  is zero. A hold capacitor ( $CH$ ) of non-critical value which might be typically 470pF is connected from  $CH$  to  $V_{SS}$ . A smaller value is sufficient if the sideband performance required is not high.

The output from the sample/phase detector should be combined with that of the coarse phase/frequency detector and filtered to generate a single control voltage to drive the VCO.

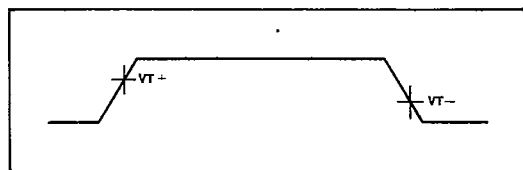


Fig.7 Timing diagram showing voltage thresholds

## CRYSTAL OSCILLATOR

When using the internal oscillator, the stability may be enhanced at high frequencies by the use of an external resistor between Pin 8 and the other components. A value of 150-270 $\Omega$  is advised.

## PROGRAMMING/POWER UP

All data and signal input pins should have no input applied to them prior to the application of  $V_{DD}$ , as otherwise 'latch up' may occur.

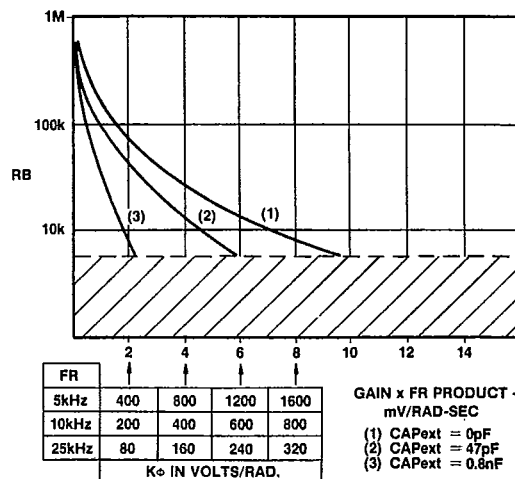


Fig.8  $R_B$  v. gain and reference frequency