



SBAS054A - MAY 2001

# Speed, 10-Bit, 20MHz, +3V Supply **ANALOG-TO-DIGITAL CONVERTER**

# **FEATURES**

- LOW POWER: 48mW at +3V ● SUPPLY RANGE: +2.7V to +3.7V
- ADJUSTABLE FULL SCALE RANGE WITH **EXTERNAL REFERENCES**
- NO MISSING CODES
- WIDEBAND TRACK/HOLD: 350MHz
- POWER DOWN: 15mW SSOP-28 PACKAGE

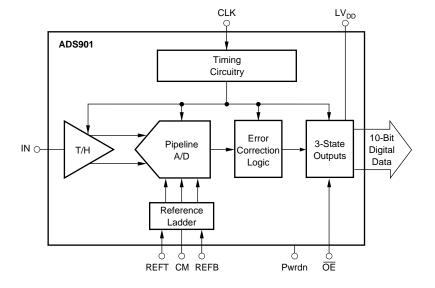
# APPLICATIONS

- BATTERY POWERED EQUIPMENT
- CAMCORDERS
- DIGITAL CAMERAS
- COMPUTER SCANNERS
- COMMUNICATIONS

# **DESCRIPTION**

The ADS901 is a high-speed pipelined analog-to-digital converter that operates from a +3V power supply. This complete converter includes a wide bandwidth track/hold and a 10-bit quantizer. The full scale input range is set by external references.

The ADS901 employs digital error correction techniques to provide excellent differential linearity for demanding imaging applications. Its low distortion and high SNR give the extra margin needed for telecommunications, video and test instrumentation applications. The ADS901 is available in an SSOP-28 package.





Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.



### **ABSOLUTE MAXIMUM RATINGS**

+V <sub>S</sub> Logic V <sub>DD</sub> Analog Input	+6V
Logic Input Case Temperature	+V <sub>S</sub> +0.3V +100°C
Junction Temperature Storage Temperature	



This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### PACKAGE/ORDERING INFORMATION

PRODUCT	PACKAGE	PACKAGE DRAWING NUMBER	SPECIFIED TEMPERATURE RANGE	PACKAGE MARKING	ORDERING NUMBER <sup>(1)</sup>	TRANSPORT MEDIA
ADS901E	SSOP-28	324	-40°C to +85°C	ADS901E	ADS901E	Rail
ADS901E	SSOP-28	324	-40°C to +85°C	ADS901E	ADS901E/1K	Tape and Reel

NOTES: (1) Models with a slash (/) are available only in Tape and Reel in the quantities indicated (e.g., /1K indicates 1000 devices per reel). Ordering 1000 pieces of "ADS901E/1K" will get a single 1000-piece Tape and Reel.

# **ELECTRICAL CHARACTERISTICS**

At  $T_A = +25^{\circ}C$ ,  $V_S = LV_{DD} = +3V$ , REFB = 1V, REFT = 2V, Specified Input Range = 1V to 2V, Sampling Rate = 20MHz, unless otherwise specified.

			ADS901E			
PARAMETER	CONDITIONS	TEMP	MIN	TYP	MAX	UNITS
Resolution Specified Temperature Range	Ambient Air		-40	10	+85	Bits ∘C
ANALOG INPUT Specified Full Scale Input Range <sup>(1)</sup> Common-Mode Voltage (Midscale) Analog Input Bias Current Input Impedance				1Vp-p 1.5 1 1.25    5		V V μΑ MΩ    pF
DIGITAL INPUT Logic Family Convert Command (Start Conversion)	Start Conversion		CMOS Compatible Rising Edge of Convert Clock			
CONVERSION CHARACTERISTICS Sample Rate Data Latency		Full	10k	5	20M	Samples/s Clk Cyc



# **ELECTRICAL CHARACTERISTICS (Cont.)**

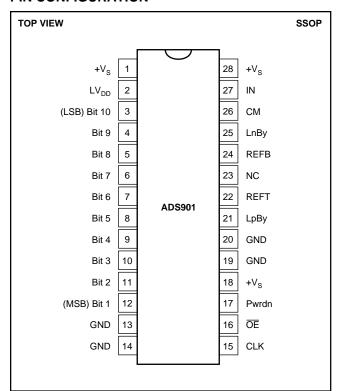
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			ADS901E			
PARAMETER	CONDITIONS	TEMP	MIN	TYP	MAX	UNITS
DYNAMIC CHARACTERISTICS						
Differential Linearity Error (Largest Code Error)						
f = 500kHz		Full		±0.8		LSB
f = 9MHz		Full		±0.9	±1.0	LSB
No Missing Codes		Full		Guaranteed		
Integral Nonlinearity Error, f = 500kHz		Full		±3.5		LSB
Spurious Free Dynamic Range <sup>(2)</sup>						
$f = 500kHz (-1dBFS^{(3)} input)$		Full		50		dBFS <sup>(3)</sup>
f = 9MHz (-1dBFS input)		Full	45	49		dBFS
Signal-to-Noise Ratio (SNR)	Referred to Sinewave Input Signal					
f = 500kHz (-1dBFS input)		Full		53		dB
f = 9MHz (-1dBFS input)		Full	48	53		dB
Maximum SNR	Referred to DC Full Scale Input Signal					
f = 9MHz (-1dBFS input)				62		dB
Signal-to-(Noise + Distortion) (SINAD)						
f = 500kHz (-1dBFS input)		Full		50		dB
f = 3.58MHz (-1dBFS input)		Full		50		dB
f = 9MHz (-1dBFS input)		Full	45	49		dB
Effective Number of Bits <sup>(4)</sup>	f <sub>IN</sub> = 3.58MHz			8.0		Bits
Differential Gain Error	NTSC, PAL			2.3		%
Differential Phase Error	NTSC, PAL			1.0		degrees
Output Noise	Input Grounded			0.2		LSB rms
Aperture Delay Time				3		ns
Aperture Jitter				7		ps rms
Analog Input Bandwidth						
Small Signal	-20dBFS Input			350		MHz
Full Power	0dBFS Input			100		MHz
Overvoltage Recovery Time <sup>(5)</sup>				2		ns
DIGITAL OUTPUTS	C <sub>L</sub> = 15pF					
Logic Family	'		C	MOS Compatib	le	
Logic Coding			Str	aight Offset Bin	ary	
High Output Voltage, V <sub>OH</sub>			+2.4		LV <sub>DD</sub>	V
Low Output Voltage, V <sub>OL</sub>					+0.4	V
3-State Enable Time	OE = L			20	40	ns
3-State Disable Time	ŌE = H			18	10	ns
Internal Pull-Down to Gnd				50		kΩ
Power-Down Enable Time	Pwrdn = L			133		ns
Power-Down Disable Time	Pwrdn = H			18		ns
Internal Pull-Down to Gnd				50		kΩ
ACCURACY	f <sub>S</sub> = 2.5MHz					
Gain Error	IS - 2.5WII IZ	Full		2.5		%FS
Input Offset <sup>(6)</sup>		Full		0.4		%FS
Power Supply Rejection (Gain)	Δ V <sub>S</sub> = +10%	Full		56		dB
Power Supply Rejection (Offset)	1 VS - +10/0	Full		68		dB
External REFT Voltage Range		Full	REFB +0.5	2	V <sub>S</sub> -0.8	V
External REFB Voltage Range		Full	0.8	1	REFT -0.5	V
Reference Input Resistance		ı un	0.0	4	11211 0.0	kΩ
·				•		
POWER SUPPLY REQUIREMENTS						
Supply Voltage: +V <sub>S</sub>	Operating	Full	+2.7	+3.0	+3.7	V
Supply Current: +I <sub>S</sub>	Operating	Full		16		mA
Power Dissipation	Operating	Full		49	60	mW
Power Dissipation (Power Down)	Operating	Full		15		mW
Thermal Resistance, $\theta_{JA}$						00.000
28-Lead SSOP				89		°C/W

NOTES: (1) The single-ended input range is set by REFB and REFT values. (2) Spurious Free Dynamic Range refers to the magnitude of the largest harmonic. (3) dBFS is dB relative to full scale. (4) Based on (SINAD - 1.76)/6.02. (5) No "Rollover" of bits. (6) Offset Deviation from Ideal Negative Full Scale.



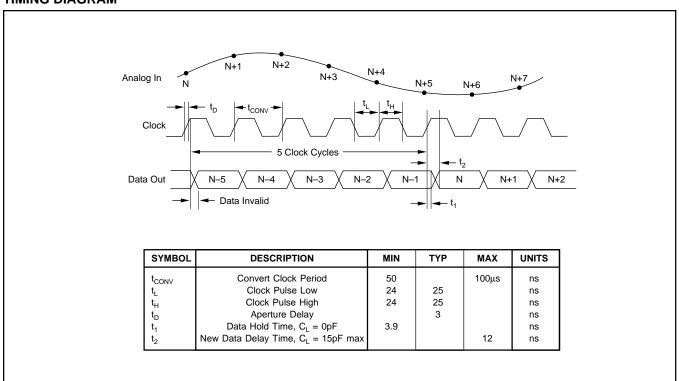
## **PIN CONFIGURATION**



### **PIN DESCRIPTIONS**

PIN	DESIGNATOR	DESCRIPTION
1	+V <sub>S</sub>	Analog Supply
2	$LV_DD$	Output Logic Driver Supply Voltage
3	Bit 10	Data Bit 10 (D0) (LSB)
4	Bit 9	Data Bit 9 (D1)
5	Bit 8	Data Bit 8 (D2)
6	Bit 7	Data Bit 7 (D3)
7	Bit 6	Data Bit 6 (D4)
8	Bit 5	Data Bit 5 (D5)
9	Bit 4	Data Bit 4 (D6)
10	Bit 3	Data Bit 3 (D7)
11	Bit 2	Data Bit 2 (D8)
12	Bit 1	Data Bit 1 (D9) (MSB)
13	GND	Analog Ground
14	GND	Analog Ground
15	CLK	Convert Clock Input
16	ŌĒ	Output Enable, Active Low
17	Pwrdn	Power Down Pin
18	+V <sub>S</sub>	Analog Supply
19	GND	Analog Ground
20	GND	Analog Ground
21	LpBy	Positive Ladder Bypass
22	REFT	Top Reference Input
23	NC	No Connection
24	REFB	Bottom Reference Input
25	LnBy	Negative Ladder Bypass
26	СМ	Common-Mode Voltage Output
27	IN	Analog Input
28	+V <sub>S</sub>	Analog Supply

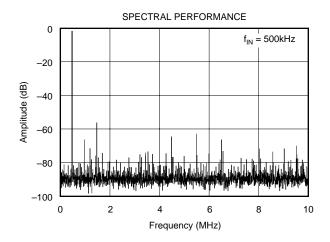
## **TIMING DIAGRAM**

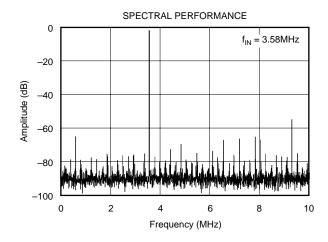


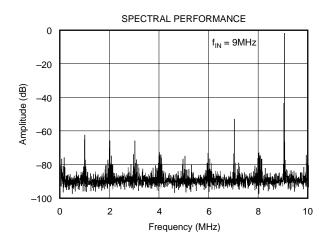


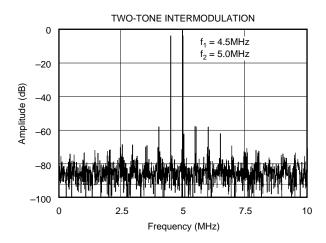
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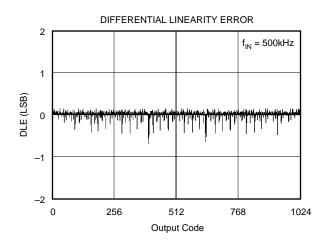
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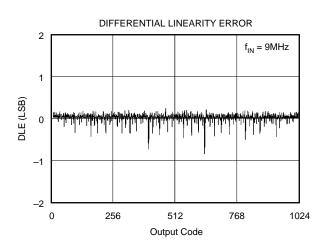










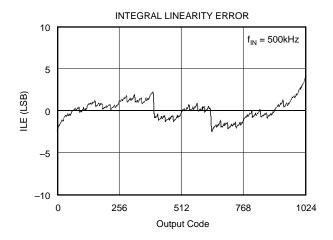


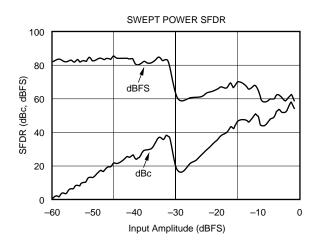


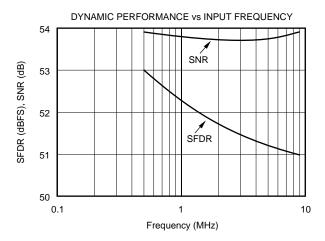


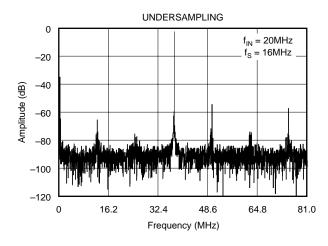
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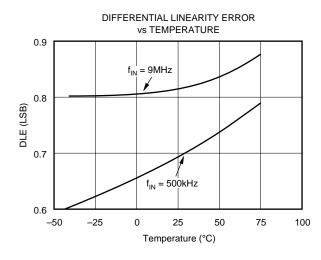
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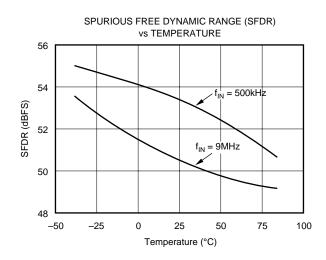








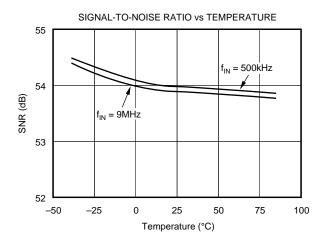


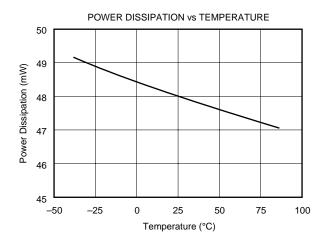


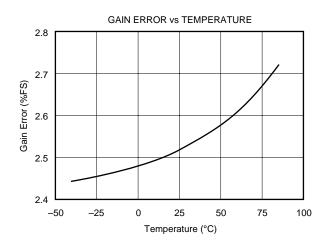


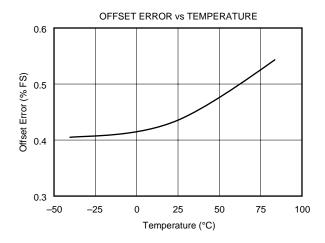
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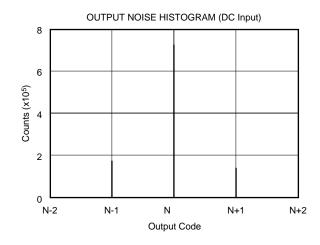
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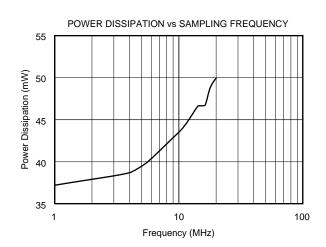














## THEORY OF OPERATION

The ADS901 is a high speed sampling analog-to-digital converter that utilizes a pipeline architecture. The fully differential topology and digital error correction guarantee 10-bit resolution. The differential track/hold circuit is shown in Figure 1. The switches are controlled by an internal clock which has a non-overlapping two phase signal,  $\phi 1$  and  $\phi 2$ . At the sampling time the input signal is sampled on the bottom plates of the input capacitors. In the next clock phase, \$1, the bottom plates of the input capacitors are connected together and the feedback capacitors are switched to the op amp output. At this time the charge redistributes between C<sub>I</sub> and C<sub>H</sub>, completing one track/hold cycle. The differential output is a held DC representation of the analog input at the sample time. The track/hold circuit can also convert a single-ended input signal into a fully differential signal for the quantizer. Consequently, the input signal-to-noise performance. Other parameters such as small-signal and full-power bandwidth, and wideband noise are also defined in this stage.

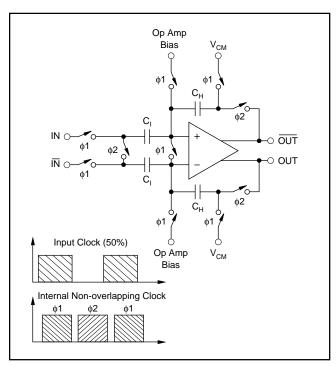


FIGURE 1. Input Track/Hold Configuration with Timing Signals.

The pipelined quantizer architecture has 9 stages with each stage containing a two-bit quantizer and a two bit digital-to-analog converter, as shown in Figure 2. Each two-bit quantizer stage converts on the edge of the sub-clock, which is the same frequency of the externally applied clock. The output of each quantizer is fed into its own delay line to time-align it with the data created from the following quantizer stages. This aligned data is fed into a digital error correction circuit which can adjust the output data based on the information found on the redundant bits. This technique provides the ADS901 with excellent differential linearity and guarantees no missing codes at the 10-bit level.

To accommodate a bipolar signal swing, the ADS901 operates with a common-mode voltage ( $V_{CM}$ ) which is derived from the external references. Due to the symmetric resistor ladder inside the ADS901, the  $V_{CM}$  is situated between the top and bottom reference voltage. Equation (1) can be used for calculating the common-mode voltage level.

$$V_{CM} = (REFT + REFB)/2 \tag{1}$$

There is a 5.0 clock cycle data latency from the start convert signal to the valid output data. The standard output coding is Straight Offset Binary where a full scale input signal corresponds to all "1's" at the output. The digital outputs of the ADS901 can be set to a high impedance state by driving the three-state (pin 16) with a logic "HI". Normal operation is achieved with pin 16 "LO" or Floating due to internal pull-down resistors. This function is provided for testability purposes but is not recommended to be used dynamically.

## **APPLICATIONS**

# SIGNAL SWING AND COMMON-MODE CONSIDERATIONS

The ADS901 is designed to operate on a +3V single supply voltage. The nominal input signal swing is 1Vp-p, situated between +1V and +2V. This means that the signal swings  $\pm 0.5$ V around a common-mode voltage of +1.5V, which is half the supply voltage ( $V_{CM} = V_S/2$ ). In some applications it might be advantageous to increase the input signal swing. This will improve the achievable signal-to-noise performance. However, considerations should be made to keep the signal swing within the linear range of operation of the driving circuitry to avoid any excessive distortion. In extreme situations the performance of the converter will start to degrade due to variations of the input's switch onresistance over the input voltage. Therefore, the signal swing should remain approximately 0.5V away from each rail during normal operation.

# DRIVING THE ANALOG INPUTS AC-COUPLED DRIVER

Figure 2 shows an example of an ac-coupled, single-ended interface circuit using a high-speed op amp that operates on

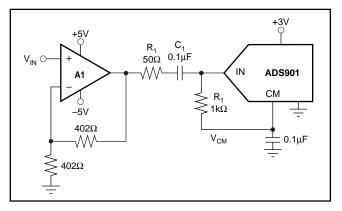


FIGURE 2. AC-Coupled, Single-Ended Interface Circuit.



dual supplies (OPA650, OPA658). The mid-point reference voltage,  $V_{CM}$ , biases the bipolar, ground-referenced input signal. The capacitor  $C_1$  and resistor  $R_1$  form a high-pass filter with the -3dB frequency set at

$$f_{-3dB} = 1/(2 \pi R_1 C_1)$$
 (2)

The values for  $C_1$  and  $R_1$  are not critical in most applications and can be set freely. The values shown correspond to a frequency of 1.6kHz.

Figure 3 depicts a circuit that can be used in single-supply applications. The mid-reference voltage biases the op amp up to the appropriate common-mode voltage, for example  $V_{CM} = +1.5V$ . With the use of capacitor  $C_G$  the DC gain for the non-inverting op amp input is set to +1V/V. As a result the transfer function is modified to

$$V_{OUT} = V_{IN} \{ (1 + R_F/R_G) + V_{CM} \}$$
 (3)

Again, the input coupling capacitor  $C_1$  and resistor  $R_1$  form a high-pass filter. At the same time the input impedance is defined by  $R_1$ . Resistor  $R_S$  isolates the op amp's output from the capacitive load to avoid gain peaking or even oscillation. It can also be used to establish a defined bandwidth to reduce the wideband noise. The recommended value is usually between  $10\Omega$  and  $100\Omega$ .

#### **DC-COUPLED INTERFACE CIRCUIT**

Many systems are now requiring +3V single supply capability of both the A/D converter and its driver. Figure 4 shows an example for DC-coupled configuration operating solely

on a +3V supply voltage. The OPA632 provides excellent performance in this demanding application. Its wide input and output voltage ranges, an low distortion, supports the ADS901 well. The OPA632 is configured for a gain of +2. The 374 $\Omega$  and 2.26k $\Omega$  resistors at the input level-shift  $V_{IN}$  so that  $V_{OUT}$  is within the allowed output voltage range when  $V_{IN}=0$ . The input impedance of the driver circuit is set to match to a  $50\Omega$  source impedance. The input level-shifting was designed that  $V_{IN}$  can be between 0V and 5V, while delivering an output voltage of 1V to 2V into the ADS901. Both the OPA632 and ADS901 have a power-down function pin with the same polarity for those systems the need to conserve power.

#### **EXTERNAL REFERENCE**

The ADS901 requires external references on pin 22 (REFT) and 24 (REFB). Internally those pins are connected through a resistor ladder, which has a nominal resistance of  $4k\Omega$  ( $\pm 15\%$ ). In order to establish a correct voltage drop across the ladder the external reference circuit must be able to typically supply  $250\mu A$  of current. With this current the full-scale input range of the ADS901 is set between +1V and +2V, or 1Vp-p. In general, the voltage drop across REFT and REFB determines the input full-scale range (FSR) of the ADS901. Equation (4) can be used to calculate the span.

$$FSR = REFT - REFB$$
 (4)

Depending on the application, several options are possible to supply the external reference voltages to the ADS901 without degrading the typical performance.

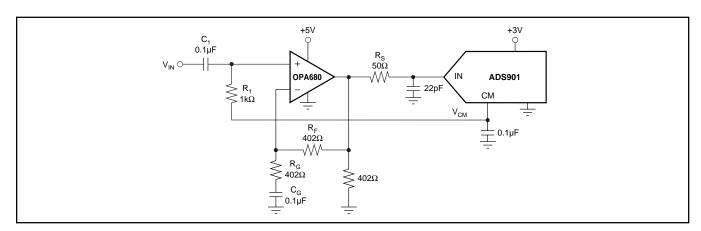


FIGURE 3. Interface Circuit. Example using the voltage feedback amplifier OPA680.

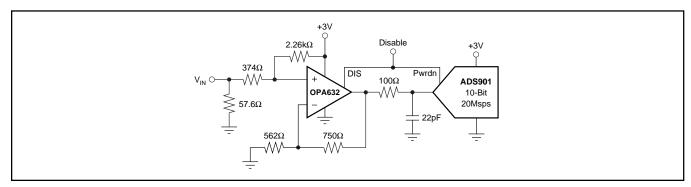


FIGURE 4. DC-Coupled Interface Circuit for +3V Single-Supply Operation.





#### LOW-COST REFERENCE SOLUTION

The easiest way to achieve the required reference voltages is to place the reference ladder of the ADS901 between the supply rails, as shown in Figure 5. Two additional resistors (R<sub>T</sub>, R<sub>B</sub>) are necessary to set the correct current through the ladder. However depending on the desired full-scale swing and supply voltage different resistor values might be selected.

The trade-offs, when selecting this reference circuit, are variations in the reference voltages due to component tolerances and power supply variations. In any case, it is recommended to bypass the reference ladder with at least  $0.1\mu F$  ceramic capacitors, as shown in Figure 5. The capacitors serve a dual purpose. They will bypass most of the high frequency transient noise which results from feedthrough of the clock and switching noise from the T/H stages. Secondly, they serve as a charge reservoir to supply instantaneous current to internal nodes.

SINGLE-ENDED INPUT	STRAIGHT OFFSET BINARY (SOB) PIN 12 FLOATING or LO
+FS (IN = +2V)	111111111
+FS -1LSB	111111111
+FS -2LSB	111111110
+3/4 Full Scale	1110000000
+1/2 Full Scale	1100000000
+1/4 Full Scale	101000000
+1LSB	100000001
Bipolar Zero (IN +1.5V)	100000000
-1LSB	011111111
-1/4 Full Scale	0110000000
-1/2 Full Scale	010000000
-3/4 Full Scale	0010000000
-FS +1LSB	000000001
-FS (IN = +1V)	000000000

TABLE I. Coding Table for the ADS901.

### PRECISE REFERENCE SOLUTION

For those applications requiring a higher level of dc accuracy and drift, a reference circuit with a precision reference element might be used (see Figure 6). A stable +1.2V reference voltage is established by a two terminal bandgap reference diode, the REF1004-1.2. Using a general-purpose single-supply dual operational amplifier (A1), like an OPA2237, OPA2234 or OPA2343, the two required reference voltages for the ADS901 can be generated by setting each op amp to the appropriate gain; for example: set REFT to +2V and REFB to +1V.

#### **CLOCK INPUT**

The clock input of the ADS901 is designed to accommodate either +5V or +3V CMOS logic levels. To drive the clock input with a minimum amount of duty cycle variation and support maximum sampling rates (20Msps), high speed or advanced CMOS logic should be used (HC/HCT, AC/ACT). When digitizing at high sampling rates, a 50% duty cycle clock with fast rise and fall times (2ns or less) are recommended to meet the rated performance specifications. However, the ADS901 performance is tolerant to duty cycle variations of as much as ±10% without degradation. For applications operating with input frequencies up to Nyquist or undersampling applications, special consideration must be made to provide a clock with very low jitter. Clock jitter leads to aperture jitter (t<sub>A</sub>) which can be the ultimate limitation to achieving good SNR performance. Equation (5) shows the relationship between aperture jitter, input frequency and the signal-to-noise ratio:

$$SNR = 20\log_{10} \left[ 1/(2 \pi f_{IN} t_{A}) \right]$$
 (5)

For example, with a 10MHz full-scale input signal and an aperture jitter of  $t_A$  = 20ps, the SNR is clock jitter limited to 58dB.

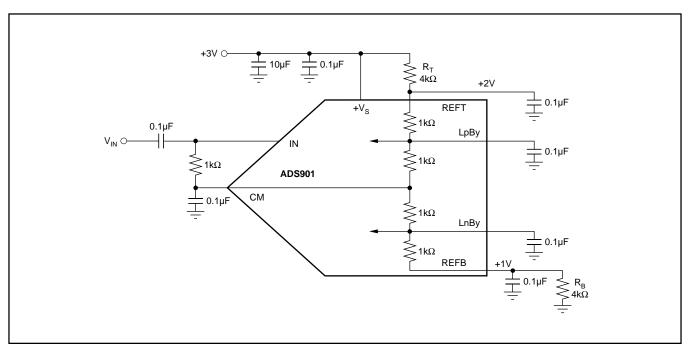


FIGURE 5. Low Cost Solution to Supply External Reference Voltages and Recommended Reference Bypassing.



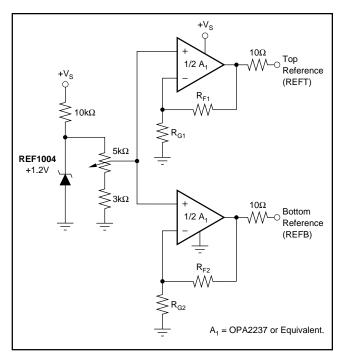


FIGURE 6. Precise Solution to Supply External Reference Voltages.

#### **DIGITAL OUTPUTS**

There is a 5.0 clock cycle data latency from the start convert signal to the valid output data. The standard output coding is Straight Offset Binary where a full scale input signal corresponds to all "1's" at the output. The digital outputs of the ADS901 can be set to a high impedance state by driving the three-state (pin 16) with a logic "HI". Normal operation is achieved with pin 16 "LO" or Floating due to internal pull-down resistors. This function is provided for testability purposes but is not recommended to be used dynamically.

The digital outputs of the ADS901 are standard CMOS stages and designed to be compatible to both high speed TTL and CMOS logic families. The logic thresholds are for low-voltage CMOS:  $V_{OL} = 0.4V$ ,  $V_{OH} = 2.4V$ , which allows the ADS901 to directly interface to 3V-logic. The digital outputs of the ADS901 use a dedicated digital supply pin (pin 2,  $LV_{DD}$ ). By adjusting the voltage on  $LV_{DD}$ , the digital output levels will vary respectively. In any case, it is recommended to limit the fan-out to one, to keep the capacitive loading on the data lines below the specified 15pF. If necessary, external buffers or latches may be used to provide the added benefit of isolating the A/D converter from any digital activities on the bus coupling back high frequency noise and degrading the performance.

#### **POWER-DOWN MODE**

The ADS901's low power consumption can be further reduced by initiating a power down mode. For this, the Pwrdn-Pin (Pin 17) must be tied to a logic "High" reducing the current drawn from the supply by approximately 70%. In normal operation the power-down mode is disabled by an internal pull-down resistor ( $50k\Omega$ ).

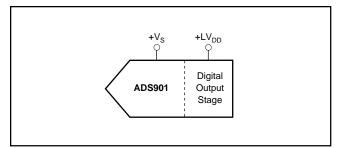


FIGURE 7. Independent Supply Connection for Output Stage.

During power-down the digital outputs are set in 3-state. With the clock applied, the converter does not accurately process the sampled signal. After removing the power-down condition the output data from the following 5 clock cycles is invalid (data latency).

# DECOUPLING AND GROUNDING CONSIDERATIONS

The ADS901 converter have several supply pins, one of which is dedicated to supply only the output driver. The remaining supply pins are not, as is often the case, divided into analog and digital supply pins since they are internally connected on the chip. For this reason it is recommended to treat the converter as an analog component and to power it from the analog supply only. Digital supply lines often carry high levels of noise which can couple back into the converter and limit the achievable performance.

Because of the pipeline architecture, the converter also generates high frequency transients and noise that are fed back into the supply and reference lines. This requires that the supply and reference pins be sufficiently bypassed. Figure 8 shows the recommended decoupling scheme for the analog supplies. In most cases  $0.1\mu F$  ceramic chip capacitors are adequate to keep the impedance low over a wide frequency range. Their effectiveness largely depends on the proximity to the individual supply pin. Therefore they should be located as close to the supply pins as possible.

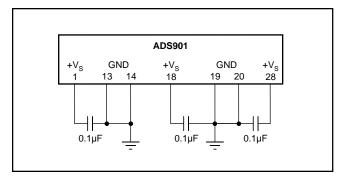


FIGURE 8. Recommended Bypassing for Analog Supply Pins.



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