## - Description

ROHM's highly-efficient step-up/down switching regulator BD8305MUV produces step-up/down output including 3.3 V from 1 cell of lithium battery with just one coil.This IC adopts an original step-up/down drive system and creates a higher efficient power supply than conventional Sepic-system or H -bridge system switching regulators.

## -Features

1) Highly-efficient step-up/down DC/DC converter to be constructed just with one inductor.
2) Input voltage $\quad 2.5 \mathrm{~V}-5.5 \mathrm{~V}$
3) Output current 1 A at 3.3 V

800 mA at 5.0 V
4) Incorporates soft-start function.
5) Incorporates timer latch system short protecting function.
6) High heat radiation surface mounted package VQFN020V4040

## -Application

General portable equipment like portable audio or DSC/DVC

- Absolute Maximum Ratings

| Parameter | Symbol | BD8305MUV | Unit |
| :--- | :---: | :---: | :---: |
| Maximum applied power voltage | Vcc,PVCC | 7.0 | V |
| Maximum input current | linmax | 2.0 | A |
| Maximum input voltage | Lx 1 | 7.0 | V |
|  | Lx 2 | 7.0 | V |
| Power dissipation | Pd | 700 | mW |
| Operating temperature range | Topr | -25 to +85 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature range | Tstg | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |
| Junction temperature | Tjmax | 150 | ${ }^{\circ} \mathrm{C}$ |

*1 When installed on a $70.0 \mathrm{~mm} \times 70.0 \mathrm{~mm} \times 1.6 \mathrm{~mm}$ glass epoxy board. The rating is reduced by $5.6 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ at $\mathrm{Ta}=25^{\circ} \mathrm{C}$ or more .

## - Operating Conditions $\left(\mathbf{T a}=\mathbf{2 5}{ }^{\circ} \mathrm{C}\right)$

| Parameter | Symbol | Voltage range | Unit |
| :--- | :---: | :---: | :---: |
| Power supply voltage | Vcc | 2.5 to 5.5 | V |
| Output voltage | OUT | 2.8 to 5.2 | V |

## - Electrical Characteristics

(Unless otherwise specified, $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{VCC}=3.7 \mathrm{~V}$ )

| Parameter |  | Symbol | Target Value |  |  | Unit | Conditions |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Typ | Max |  |  |
| [Low voltage input malfunction preventing circuit] |  |  |  |  |  |  |  |
| Detection threshold voltage |  |  | VUV | - | 2.25 | 2.45 | V | Vcc monitor |
| Hysteresis range |  | $\Delta \mathrm{VUVhy}$ | 50 | 100 | 150 | mV |  |
| [Oscillator] |  |  |  |  |  |  |  |
| Oscillation frequency |  | fosc | 0.8 | 1.0 | 1.2 | MHz | $\mathrm{RT}=47 \mathrm{k} \Omega$ |
| [Error AMP] |  |  |  |  |  |  |  |
| INV threshold voltage |  | VINV | 0.790 | 0.800 | 0.810 | V |  |
| Input bias current |  | IINV | -50 | 0 | 50 | nA | Vcc=7.0V, VINV=3.5V |
| Soft-start time |  | Tss | 0.6 | 1.00 | 1.4 | msec | RT $=47 \mathrm{k} \Omega$ |
| Output source current |  | IEO | 10 | 20 | 30 | uA | $\mathrm{VINV}=0.5 \mathrm{~V}, \mathrm{VFB}=1.5 \mathrm{~V}$ |
| Output sink current |  | IEI | 0.7 | 1.5 | 3.0 | mA | $\mathrm{VINV}=1.1 \mathrm{~V}, \mathrm{VFB}=1.5 \mathrm{~V}$ |
| [PWM comparator] |  |  |  |  |  |  |  |
| LX1 Max Duty |  | Dmax1 | - | - | 100 | \% |  |
| LX2 Max Duty |  | Dmax2 | 77 | 85 | 93 | \% |  |
| [Output] |  |  |  |  |  |  |  |
| LX1 PMOS ON resistance |  | RON1p | - | 120 | 200 | $\mathrm{m} \Omega$ | VGS $=3.0 \mathrm{~V}$ |
| LX1 NMOS ON resistance |  | RON1n | - | 100 | 160 | $\mathrm{m} \Omega$ | VGS $=3.0 \mathrm{~V}$ |
| LX2 PMOS ON resistance |  | RON2p | - | 120 | 200 | $\mathrm{m} \Omega$ | VGS $=3.0 \mathrm{~V}$ |
| LX2 NMOS ON resistance |  | RON2n | - | 100 | 160 | M ת | VGS $=3.0 \mathrm{~V}$ |
| LX1 OCP threshold |  | locp | 1.6 | 2.4 | - | A | PVCC=3.0V |
| LX1 leak current |  | 1 leak1 | -1 | 0 | 1 | uA |  |
| LX2 leak current |  | \| leak2 | -1 | 0 | 1 | uA |  |
| [STB] |  |  |  |  |  |  |  |
| STB pin control voltage | Operation | VSTBH | 1.5 | - | 5.5 | V |  |
|  | No-operation | VSTBL | -0.3 | - | 0.3 | V |  |
| STB pin pull-down resistance |  | RSTB | 250 | 400 | 700 | k $\Omega$ |  |
| [Circuit current] |  |  |  |  |  |  |  |
| Standby current | VCC pin | ISTB1 | - | - | 1 | uA |  |
|  | PVCC pin | ISTB2 | - | - | 1 | uA |  |
|  | VOUT pin | ISTB3 | - | - | 1 | uA |  |
| Circuit current at operation VCC |  | Icc1 | - | 500 | 750 | uA | VINV $=1.2 \mathrm{~V}$ |
| Circuit current at operation PVCC |  | Icc2 | - | 10 | 20 | uA | $\mathrm{VINV}=1.2 \mathrm{~V}$ |

## -Description of Pins



| Pin No. | Pin Name | Function |
| :---: | :---: | :--- |
| 1 | FB | Error AMP output terminal |
| 2 | INV | Error AMP input terminal |
| $3 \sim 4$ | GND | Ground terminal |
| $5 \sim 6$ | Vout | Output voltage terminal |
| $7 \sim 8$ | Lx2 | Output side coil connecting terminal |
| $9 \sim 12$ | PGND | Power transistor ground terminal |
| $13 \sim 14$ | Lx1 | Input side coil connecting terminal |
| $15 \sim 17$ | PVCC | DC/DC converter input terminal |
| 18 | VCC | Control part power supply input <br> terminal |
| 19 | STB | ON/OFF terminal |
| 20 | RT | Oscillation frequency set terminal |

Fig. 1 Pin layout

## -Block Diagram



Fig. 2 Block diagram

## - Description of Blocks

1.VREF

This block generates ERROR AMP reference voltage. The reference voltage is 0.8 V .
2.UVLO

Circuit for preventing low voltage malfunction
Prevents malfunction of the internal circuit at activation of the power supply voltage or at low power supply voltage. Monitors VCC pin voltage to turn off all output FET and DC/DC converter output when VCC voltage is lower than 2.2 V , and reset the timer latch of the internal SCP circuit and soft-start circuit.
3.SCP

Timer latch system short-circuit protection circuit
When the INV pin is the set 0.8 V or lower voltage, the internal SCP circuit starts counting.
The internal counter is in synch with OSC, the latch circuit activates after the counter counts about 8200 oscillations to turn off DC/DC converter output (about 8.2 msec when $\mathrm{RT}=47 \mathrm{~K} \Omega$ ).
To reset the latch circuit, turn off the STB pin once. Then, turn it on again or turn on the power supply voltage again.

## 4.OSC

Oscillation circuit to change frequency by external resistance of the RT pin (20 pin).
When RT $=47 \mathrm{k} \Omega$, operation frequency is set at 1 MHz .
5.ERROR AMP

Error amplifier for detecting output signals and output PWM control signals.
The internal reference voltage is set at 0.8 V .
6.PWM COMP

Voltage-pulse width converter for controlling output voltage corresponding to input voltage.
Comparing the internal SLOPE waveform with the ERROR AMP output voltage, PWM COMP controls the pulse width and outputs to the driver.
Max Duty and Min Duty are set at the primary side and the secondary side of the inductor respectively, which are as follows:

| Primary side (Lx1) | Max Duty : $100 \%$, |
| :--- | :--- |
| Secondary side (Lx2) | Min Duty : $0 \%$ |
|  | Max Duty $: 100 \%$, |
|  | Min Duty : About $15 \%$ |

## 7.SOFT START

Circuit for preventing in-rush current at startup by bringing the output voltage of the DC/DC converter into a soft-start Soft-start time is in synch with the internal OSC, and the output voltage of the DC/DC converter reaches the set voltage after about 1000 oscillations (About 1 msec when RT $=47 \mathrm{k} \Omega$ ).
8.PRE DRIVER

CMOS inverter circuit for driving the built-in Pch/Nch FET.Dead time is provided for preventing feedthrough during switching. The dead time is set at about 15 nsec for each individual SWs.
9. STBY_IO

Voltage applied on STB pin (19 pin) to control ON/OFF of IC.
Turned ON when a voltage of 1.5 V or higher is applied and turned OFF when the terminal is open or 0 V is applied. Incorporates approximately $400 \mathrm{k} \Omega$ pull-down resistance.
10. Pch/Nch FET SW

Built-in SW for switching the coil current of the DC/DC converter. Pch FET is about $120 \mathrm{~m} \Omega$ and Nch is $100 \mathrm{~m} \Omega$. Since the current rating of this FET is 2 A , it should be used within 1.6 A in total including the DC current and ripple current of the coil.

## -Reference Data

(Unless otherwise specified, $\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{VCC}=3.7 \mathrm{~V}$ )


Fig. 3 INV threshold


Fig. 6 Oscillation frequency (power supply property)


Fig. 9 FB source current


Fig. 4 INV threshold (power supply property)


Fig. 5 Oscillation frequency


Fig. 8 FB sink current


Fig. 11 Lx1 Nch FET ON resistance


Fig. 7 UVLO threshold


Fig. 10 Lx1 Pch FET ON resistance


Fig. 12 Lx2 Pch FET ON resistance


Fig. 15 PVCC input current


Fig. 18 OCP detect threshold -VCC


Fig. 13 Lx2 Nch FET ON resistance


Fig. 16 VOUT input current


Fig. 14 VCC input current


Fig. 17 OCP detect threshold -Ta

## - Example of Application1 Input: 2.8 to 5.5 V , output: $3.3 \mathrm{~V} / 1.0 \mathrm{~A}$, frequency 600 kHz



- Example of Application2 Input: 2.8 to 5.5 V , output: $4.0 \mathrm{~V} / 1.0 \mathrm{~A}$, frequency 1 MHz



## - Example of Board Layout



Fig. 21 Example of Board Layout

## -Reference Application Data

(Example of application 1)


Fig. 22 Power conversion efficiency


Fig. 23 Line regulation


Fig. 24 Load regulation
(Example of application2)


Fig. 25 Maximum output current

Fig. 26 Power conversion efficiency



Fig. 27 Line regulation


Fig. 28 Load regulation

## -Selection of Parts for Applications

(1) Output inductor

A shielded inductor that satisfies the current rating (current value, Ipeak as shown in the drawing below) and has a low DCR (direct current resistance component) is recommended. Inductor values affect output ripple current greatly.
Ripple current can be reduced as the coil $L$ value becomes larger and the switching frequency becomes higher as the equations shown below.

$$
\begin{equation*}
\text { Ipeak }=\text { lout } \times(\text { Vout } / \mathrm{VIN}) / \eta+\Delta \mathrm{IL} / 2[\mathrm{~A}] \tag{1}
\end{equation*}
$$



Fig. 29 Ripple current
$\Delta I L=\frac{(\text { Vin-Vout })}{L} \times \frac{\text { Vout }}{\text { Vin }} \times \frac{1}{f}[A] \quad$ (in step-down mode)
$\Delta I L=\frac{\mid(\text { Vin-Vout)| }}{L} \times \frac{\text { Vout } \times 2 \times 0.85}{(\text { Vin }+ \text { Vout })} \times \frac{1}{f}[A] \quad$ (in step-up/down mode)
$\Delta I L=\frac{(\text { Vout-Vin })}{L} \times \frac{\text { Vin }}{\text { Vout }} \times \frac{1}{f}[A] \quad$ (in step-up mode)
( $\eta$ : Efficiency, $\Delta \mathrm{IL}$ : Output ripple current, f: Switching frequency)
As a guide, output ripple current should be set at about 20 to $50 \%$ of the maximum output current.

* Current over the coil rating flowing in the coil brings the coil into magnetic saturation, which may lead to lower efficiency or output oscillation. Select an inductor with an adequate margin so that the peak current does not exceed the rated current of the coil.
(2) Output capacitor

A ceramic capacitor with low ESR is recommended for output in order to reduce output ripple.
There must be an adequate margin between the maximum rating and output voltage of the capacitor, taking the DC bias property into consideration.
Output ripple voltage when ceramic capacitor is used is obtained by the following equation.

$$
\mathrm{Vpp}=\Delta \mathrm{IL} \times \frac{1}{2 \pi \times f \times \mathrm{Co}}+\Delta \mathrm{IL} \times \mathrm{R}_{\mathrm{ESR}} \quad[\mathrm{~V}] \quad \cdots(5)
$$

Setting must be performed so that output ripple is within the allowable ripple voltage.
(3) Setting of oscillation frequency

Oscillation frequency can be set using a resistance value connected to the RT pin (1 pin).
Oscillation frequency is set at 1 MHz when $\mathrm{RT}=47 \mathrm{k} \Omega$, and frequency is inversely proportional to RT value.
See Fig. 30 for the relationship between RT and frequency.
Soft-start time changes along with oscillation frequency.
See Fig. 31 for the relationship between RT and soft-start time.


Fig. 30 Oscillation frequency - RT pin resistance


Fig. 31 Soft-start time - RT pin resistance

[^0](4) Output voltage setting

The internal reference voltage of the ERROR AMP is 0.8 V . Output voltage should be obtained by referring to Equation (8) of Fig. 32.


(5) Determination of phase compensation

Condition for stable application
The condition for feedback system stability under negative feedback is as follows:

- Phase delay is $135^{\circ}$ or less when gain is $1(0 \mathrm{~dB})$ (Phase margin is $45^{\circ}$ or higher) Since DC/DC converter application is sampled according to the switching frequency, the GBW of the whole system (frequency at which gain is 0 dB ) must be set to be equal to or lower than $1 / 5$ of the switching frequency. In summary, target property of applications is as follows:
- Phase delay must be $135^{\circ}$ or lower when gain is $1\left(0 \mathrm{~dB}\right.$ ) (Phase margin is $45^{\circ}$ or higher).
- The GBW at that time (frequency when gain is 0 dB ) must be equal to or lower than $1 / 5$ of the switching frequency. For this reason, switching frequency must be increased to improve responsiveness.

One of the points to secure stability by phase compensation is to cancel secondary phase delay $\left(-180^{\circ}\right)$ generated by LC resonance by the secondary phase lead (i.e. put two phase leads).
Since GBW is determined by the phase compensation capacitor attached to the error amplifier, when it is necessary to reduce GBW, the capacitor should be made larger.


Fig. 33 General integrator
Error AMP is a low-pass filter because phase compensation such as (1) and (2) is performed. For DC/DC converter application, $R$ is a parallel feedback resistance.


Fig. 34 Frequency property of integrator

Phase compensation when output capacitor with low ESR such as ceramic capacitor is used is as follows: When output capacitor with low ESR (several tens of $\mathrm{m} \Omega$ ) is used for output, secondary phase lead (two phase leads) must be put to cancel secondary phase lead caused by LC. One of the examples of phase compensation methods is as follows:


Fig. 35 Example of setting of phase compensation
For setting of phase-lead frequency, both of them should be put near LC resonance frequency. When GBW frequency becomes too high due to the secondary phase lead, it may get stabilized by setting the primary phase delay to a frequency slightly higher than the LC resonance frequency by R3 to compensate it.

## - I/O Equivalence Circuit



Fig. 36 I/O Equivalence Circuit

## - Notes for use

1) Absolute Maximum Rating

We dedicate much attention to the quality control of these products, however the possibility of deterioration or destruction exists if the impressed voltage, operating temperature range, etc., exceed the absolute maximum ratings. In addition, it is impossible to predict all destructive situations such as short-circuit modes, open circuit modes, etc. If a special mode exceeding the absolute maximum rating is expected, please review matters and provide physical safety means such as fuses, etc.
2) GND Potential

Keep the potential of the GND pin below the minimum potential at all times.
3) Thermal Design

Work out the thermal design with sufficient margin taking power dissipation (Pd) in the actual operation condition into account.
4) Short Circuit between Pins and Incorrect Mounting

Attention to IC direction or displacement is required when installing the IC on a PCB. If the IC is installed in the wrong way, it may break. Also, the threat of destruction from short-circuits exists if foreign matter invades between outputs or the output and GND of the power supply.
5) Operation under Strong Electromagnetic Field

Be careful of possible malfunctions under strong electromagnetic fields.
6) Common Impedance

When providing a power supply and GND wirings, show sufficient consideration for lowering common impedance and reducing ripple (i.e., using thick short wiring, cutting ripple down by LC, etc.) as much as you can.
7) Thermal Protection Circuit (TSD Circuit)

This IC contains a thermal protection circuit (TSD circuit). The TSD circuit serves to shut off the IC from thermal runaway and does not aim to protect or assure operation of the IC itself. Therefore, do not use the TSD circuit for continuous use or operation after the circuit has tripped.
8) Rush Current at the Time of Power Activation

Be careful of the power supply coupling capacity and the width of the power supply and GND pattern wiring and routing since rush current flows instantaneously at the time of power activation in the case of CMOS IC or ICs with multiple power supplies.
9) IC Terminal Input

This is a monolithic IC and has $\mathrm{P}+$ isolation and a P substrate for element isolation between each element. $\mathrm{P}-\mathrm{N}$ junctions are formed and various parasitic elements are configured using these $P$ layers and $N$ layers of the individual elements.
For example, if a resistor and transistor are connected to a terminal as shown on Fig.37:
O The P-N junction operates as a parasitic diode
when GND > (Terminal A) in the case of a resistor or when GND > (Pin B) in the case of a transistor (NPN)
OAlso, a parasitic NPN transistor operates using the N layer of another element adjacent to the previous diode in the case of a transistor (NPN) when GND > (Pin B).
The parasitic element consequently rises under the potential relationship because of the IC's structure. The parasitic element pulls interference that could cause malfunctions or destruction out of the circuit. Therefore, use caution to avoid the operation of parasitic elements caused by applying voltage to an input terminal lower than the GND ( P board), etc.


Fig. 37 Example of simple structure of Bipolar IC

## -Ordering part number




Package
MUV: VQFN020V4040


Packaging and forming specification E2: Embossed tape and reel

## VQFN020V4040



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[^0]:    * Note that the above example of frequency setting is just a design target value, and may differ from the actual equipment.

