Data Sheet

CADEKA®
Amplify the Human Experience

COMLINEAR® CLC1605, CLC3605
Single and Triple, 1.5GHz Amplifiers

FEATURES

- 0.1dB gain flatness to 120MHz
- 0.01%/0.01° differential gain/phase
- 1.2GHz -3dB bandwidth at G = 2
- 700MHz large signal bandwidth
- 2,500V/µs slew rate
- 3.7nV/√Hz input voltage noise
- 120mA output current
- Triple offers disable
- Fully specified at 5V and ±5V supplies
- CLC1605: Pb-free SOT23-5
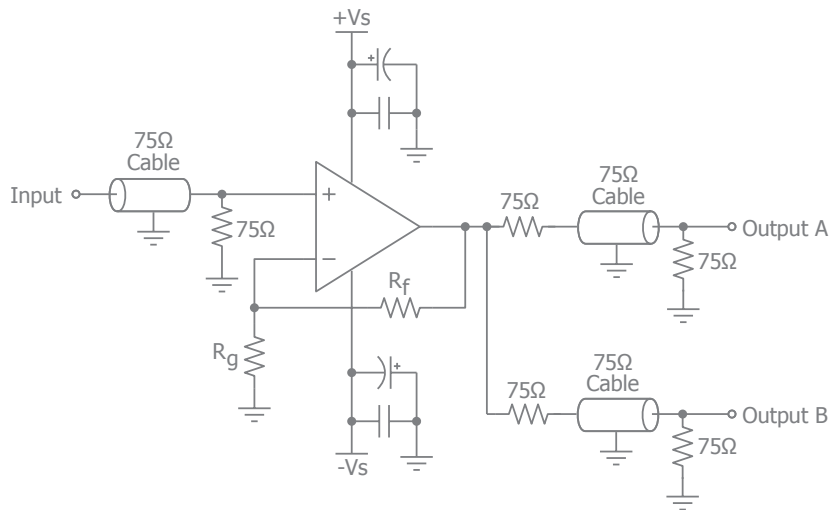- CLC3605: Pb-free SOIC-16

APPLICATIONS

- RGB video line drivers
- High definition video driver
- Video switchers and routers
- ADC buffer
- Active filters
- High-speed instrumentation
- Wide dynamic range IF amp
- Radar/communication receivers

General Description

The COMLINEAR CLC1605 (single) and CLC3605 (triple) are high-performance, current feedback amplifiers that provide 1.5GHz unity gain bandwidth, ±0.1dB gain flatness to 120MHz, and 2,500V/µs slew rate. This high performance exceeds the requirements of high-definition television (HDTV) and other multimedia applications. These COMLINEAR high-performance amplifiers also provide ample output current to drive multiple video loads.

The COMLINEAR CLC1605 and CLC3605 are designed to operate from ±5V or +5V supplies. The CLC3605 offers a fast enable/disable feature to save power. While disabled, the outputs are in a high-impedance state to allow for multiplexing applications. The combination of high-speed, low-power, and excellent video performance make these amplifiers well suited for use in many general purpose, high-speed applications including high-definition video, imaging applications, and radar/communications receivers.

Typical Application - Driving Dual Video Loads

Ordering Information

| Part Number	Package	Pb-Free	RoHS Compliant	Operating Temperature Range	Packaging Method
CLC1605IST5X	SOT23-5	Yes	Yes	-40°C to +85°C	Reel
CLC3605ISO16X	SOIC-16	Yes	Yes	-40°C to +85°C	Reel
CLC3605ISO16	SOIC-16	Yes	Yes	-40°C to +85°C	Rail

Moisture sensitivity level for all parts is MSL-1.

CLC1605 Pin Configuration

CLC3605 Pin Configuration
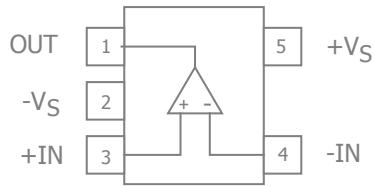
CLC1605 Pin Assignments

Pin No.	Pin Name	Description
1	OUT	Output
2	$-V_S$	Negative supply
3	+IN	Positive input
4	-IN	Negative input
5	$+V_S$	Positive supply
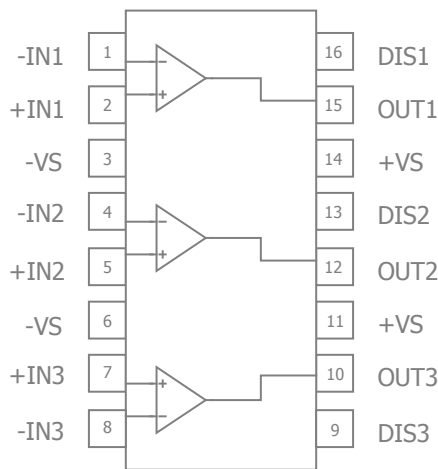
CLC3605 Pin Configuration

Pin No.	Pin Name	Description
1	-IN1	Negative input, channel 1
2	+IN1	Positive input, channel 1
3	$-V_S$	Negative supply
4	-IN2	Negative input, channel 2
5	+IN2	Positive input, channel 2
6	$-V_S$	Negative supply
7	+IN3	Positive input, channel 3
8	-IN3	Negative input, channel 3
9	DIS3	Disable pin. Enabled if pin is grounded, left floating or pulled below V_{ON}, disabled if pin is pulled above V_{OFF}.
10	OUT3	Output, channel 3
11	$+V_S$	Positive supply
12	OUT2	Output, channel 2
13	DIS2	Disable pin. Enabled if pin is grounded, left floating or pulled below V_{ON}, disabled if pin is pulled above V_{OFF}.
14	$+V_S$	Positive supply
15	OUT1	Output, channel 1
16	DIS1	Disable pin. Enabled if pin is grounded, left floating or pulled below V_{ON}, disabled if pin is pulled above V_{OFF}.

Disable Pin Truth Table

Pin	High	Low*
DIS	Disabled	Enabled

*Default Open State

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Absolute Maximum Ratings

The safety of the device is not guaranteed when it is operated above the "Absolute Maximum Ratings". The device should not be operated at these "absolute" limits. Adhere to the "Recommended Operating Conditions" for proper device function. The information contained in the Electrical Characteristics tables and Typical Performance plots reflect the operating conditions noted on the tables and plots.

Parameter	Min	Max	Unit
Supply Voltage	0	14	V
Input Voltage Range	$-V_S$ -0.5V	$+V_S$ +0.5V	V
Continuous Output Current		120	mA

Reliability Information

Parameter	Min	Typ	Max	Unit
Junction Temperature			150	°C
Storage Temperature Range	-65		150	°C
Lead Temperature (Soldering, 10s)			260	°C
Package Thermal Resistance				
5-Lead SOT23		221		°C/W
16-Lead SOIC		68		°C/W

Notes:
Package thermal resistance (θ_{JA}), JDEC standard, multi-layer test boards, still air.

ESD Protection

Product	SOT23-5	SOIC-16
Human Body Model (HBM)	2kV	2kV
Charged Device Model (CDM)	1kV	1kV

Recommended Operating Conditions

Parameter	Min	Typ	Max	Unit
Operating Temperature Range	-40		+85	°C
Supply Voltage Range	4.5		12	V

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Electrical Characteristics at +5V

$T_A = 25°C$, $V_S = +5V$, $R_f = R_g = 330Ω$, $R_L = 150Ω$ to $V_S/2$, G = 2; unless otherwise noted.

Symbol	Parameter	Conditions	Min	Typ	Max	Units
Frequency Domain Response						
UGBW	Unity Gain Bandwidth	G = +1, V_{OUT} = 0.5V_{pp}, R_f = 499Ω		1250		MHz
BW_{SS}	-3dB Bandwidth	G = +2, V_{OUT} = 0.5V_{pp}		1000		MHz
BW_{LS}	Large Signal Bandwidth	G = +2, V_{OUT} = 1V_{pp}		825		MHz
$BW_{0.1dBSS}$	0.1dB Gain Flatness	G = +2, V_{OUT} = 0.5V_{pp}		100		MHz
$BW_{0.1dBLS}$	0.1dB Gain Flatness	G = +2, V_{OUT} = 1V_{pp}		100		MHz
Time Domain Response						
t_R, t_F	Rise and Fall Time	V_{OUT} = 1V step; (10% to 90%)		0.6		ns
t_S	Settling Time to 0.1%	V_{OUT} = 1V step		10		ns
OS	Overshoot	V_{OUT} = 0.2V step		1		%
SR	Slew Rate	2V step		1350		V/μs
Distortion/Noise Response						
HD2	2nd Harmonic Distortion	V_{OUT} = 1V_{pp}, 5MHz		-75		dBc
HD3	3rd Harmonic Distortion	V_{OUT} = 1V_{pp}, 5MHz		-85		dBc
THD	Total Harmonic Distortion	V_{OUT} = 1V_{pp}, 5MHz		74		dB
D_G	Differential Gain	NTSC (3.58MHz), AC-coupled, R_L = 150Ω		0.04		%
D_P	Differential Phase	NTSC (3.58MHz), AC-coupled, R_L = 150Ω		0.01		°
IP3	Third Order Intercept	V_{OUT} = 1V_{pp}, 10MHz		37		dBm
SFDR	Spurious Free Dynamic Range	V_{OUT} = 1V_{pp}, 5MHz		61		dBc
e_n	Input Voltage Noise	> 1MHz		3.7		nV/√Hz
i_n	Input Current Noise	> 1MHz, Inverting		20		pA/√Hz
		> 1MHz, Non-Inverting		30		pA/√Hz
X_{TALK}	Crosstalk	Channel-to-channel 5MHz, V_{OUT} = 2V_{pp}		60		dB
DC Performance						
V_{IO}	Input Offset Voltage			0		mV
dV_{IO}	Average Drift			1.6		μV/°C
I_{bn}	Input Bias Current - Non-Inverting			3		μA
dI_{bn}	Average Drift			7		nA/°C
I_{bi}	Input Bias Current - Inverting			6		μA
dI_{bi}	Average Drift			20		nA/°C
PSRR	Power Supply Rejection Ratio	DC		58		dB
I_S	Supply Current	per channel		11		mA
Disable Characteristics - CLC3605 only						
T_{ON}	Turn On Time			23		ns
T_{OFF}	Turn Off Time			350		ns
OFF_{IOS}	Off Isolation	5MHz, V_{OUT} = 2V_{pp}		75		dB
V_{OFF}	Power Down Input Voltage	DIS pin, disabled if pin is pulled above V_{OFF}	Disabled if DIS > 1.5V			V
V_{ON}	Enable Input Voltage	DIS pin, enabled if pin is grounded, left open or pulled below V_{ON}	Enabled if DIS < 0.5V			V
I_{SD}	Disable Supply Current	DIS pin is pulled to V_S		0.09		mA
Input Characteristics						
R_{IN}	Input Resistance	Non-inverting		150		kΩ
		Inverting		70		Ω
C_{IN}	Input Capacitance			1.0		pF
CMIR	Common Mode Input Range			1.5 to 3.5		V
CMRR	Common Mode Rejection Ratio	DC		50		dB

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Electrical Characteristics at +5V continued

T_A = 25°C, V_S = +5V, R_f = R_g =330Ω, R_L = 150Ω to V_S/2, G = 2; unless otherwise noted.

Symbol	Parameter	Conditions	Min	Typ	Max	Units
Output Characteristics						
R_O	Output Resistance	Closed Loop, DC		0.1		Ω
V_{OUT}	Output Voltage Swing	R_L = 150Ω		1.5 to 3.5		V
I_{OUT}	Output Current			±120		mA

Notes:

1. 100% tested at 25°C

Electrical Characteristics at ±5V

T_A = 25°C, V_S = ±5V, R_f = R_g =330Ω, R_L = 150Ω to GND, G = 2; unless otherwise noted.

Symbol	Parameter	Conditions	Min	Typ	Max	Units
Frequency Domain Response						
UGBW	Unity Gain Bandwidth	G = +1, V_{OUT} = 0.5V_{pp}, R_f = 499Ω		1500		MHz
BW_{SS}	-3dB Bandwidth	G = +2, V_{OUT} = 0.5V_{pp}		1200		MHz
BW_{LS}	Large Signal Bandwidth	G = +2, V_{OUT} = 2V_{pp}		700		MHz
$BW_{0.1dBSS}$	0.1dB Gain Flatness	G = +2, V_{OUT} = 0.5V_{pp}		120		MHz
$BW_{0.1dBLS}$	0.1dB Gain Flatness	G = +2, V_{OUT} = 2V_{pp}		120		MHz
Time Domain Response						
t_R, t_F	Rise and Fall Time	V_{OUT} = 2V step; (10% to 90%)		0.65		ns
t_S	Settling Time to 0.1%	V_{OUT} = 2V step		13		ns
OS	Overshoot	V_{OUT} = 0.2V step		1		%
SR	Slew Rate	2V step		2500		V/µs
Distortion/Noise Response						
HD2	2nd Harmonic Distortion	V_{OUT} = 2V_{pp}, 5MHz		-73		dBc
HD3	3rd Harmonic Distortion	V_{OUT} = 2V_{pp}, 5MHz		-85		dBc
THD	Total Harmonic Distortion	V_{OUT} = 2V_{pp}, 5MHz		72		dB
D_G	Differential Gain	NTSC (3.58MHz), AC-coupled, R_L = 150Ω		0.01		%
D_P	Differential Phase	NTSC (3.58MHz), AC-coupled, R_L = 150Ω		0.01		°
IP3	Third Order Intercept	V_{OUT} = 2V_{pp}, 10MHz		42		dBm
SFDR	Spurious Free Dynamic Range	V_{OUT} = 1V_{pp}, 5MHz		73		dBc
e_n	Input Voltage Noise	> 1MHz		3.7		nV/√Hz
i_n	Input Current Noise	> 1MHz, Inverting		20		pA/√Hz
		> 1MHz, Non-Inverting		30		pA/√Hz
X_{TALK}	Crosstalk	Channel-to-channel 5MHz		60		dB
DC Performance						
V_{IO}	Input Offset Voltage [1]		-10	0	10	mV
dV_{IO}	Average Drift			1.6		µV/°C
I_{bn}	Input Bias Current - Non-Inverting [1]		-40	19	40	µA
dI_{bn}	Average Drift			7		nA/°C
I_{bi}	Input Bias Current - Inverting [1]		-35	6	35	µA
dI_{bi}	Average Drift			20		nA/°C
PSRR	Power Supply Rejection Ratio [1]	DC	40	60		dB
I_S	Supply Current [1]	per channel		12	18	mA
Disable Characteristics - CLC3605 only						
T_{ON}	Turn On Time			35		ns
T_{OFF}	Turn Off Time			410		ns
OFF_{IOS}	Off Isolation	5MHz, V_{OUT} = 2V_{pp}		75		dB
V_{OFF}	Power Down Input Voltage	DIS pin, disabled if pin is pulled above V_{OFF}	Disabled if DIS > 3V			V
V_{ON}	Enable Input Voltage	DIS pin, enabled if pin is grounded, left open or pulled below V_{ON}	Enabled if DIS < 1V			V
I_{SD}	Disable Supply Current [1]	per channel, DIS pin is pulled to V_S		0.1	0.3	mA
Input Characteristics						
R_{IN}	Input Resistance	Non-inverting		150		kΩ
		Inverting		70		Ω
C_{IN}	Input Capacitance			1.0		pF
CMIR	Common Mode Input Range			±4.0		V
CMRR	Common Mode Rejection Ratio [1]	DC	40	55		dB

COMLINEAR CLC1605, CLC3605 Single and Triple, 1.5GHz Amplifiers Rev 1A

Electrical Characteristics at ±5V continued

$T_A = 25°C$, $V_S = ±5V$, $R_f = R_g = 330Ω$, $R_L = 150Ω$ to GND, $G = 2$; unless otherwise noted.

Symbol	Parameter	Conditions	Min	Typ	Max	Units
Output Characteristics						
R_O	Output Resistance	Closed Loop, DC		0.1		Ω
V_{OUT}	Output Voltage Swing	$R_L = 150Ω$ [1]	±3.0	±3.8		V
I_{OUT}	Output Current			±280		mA

Notes:

1. 100% tested at 25°C

Typical Performance Characteristics

T_A = 25°C, V_S = ±5V, R_f = R_g =330Ω, R_L = 150Ω to GND, G = 2; unless otherwise noted.

Non-Inverting Frequency Response
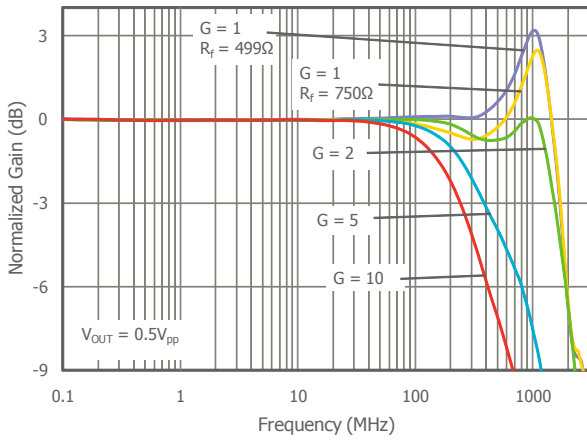
Inverting Frequency Response
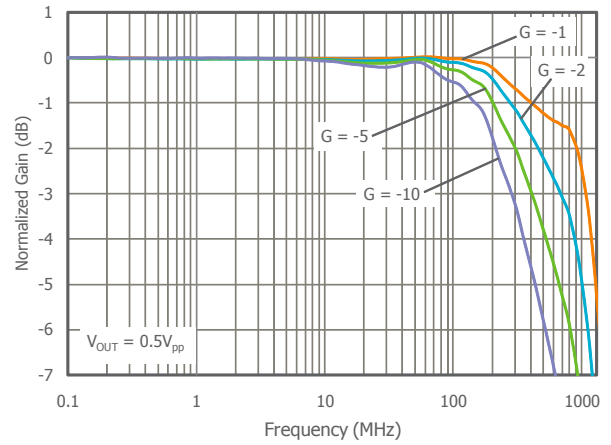
Frequency Response vs. C_L
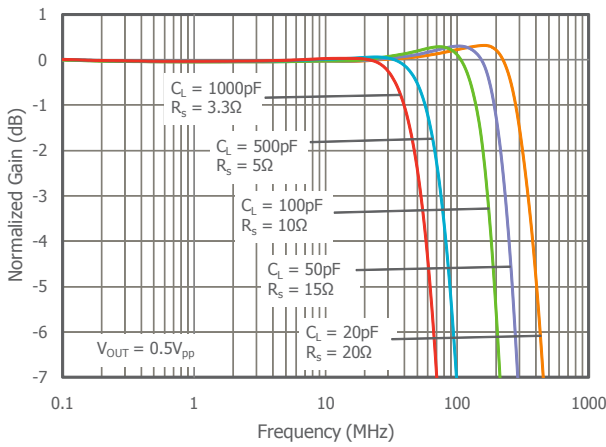
Frequency Response vs. R_L
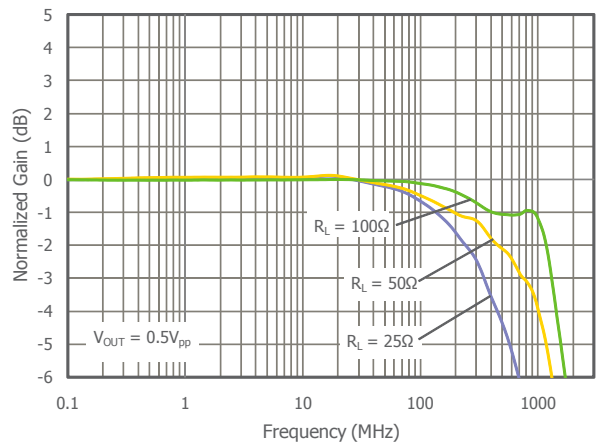
Frequency Response vs. V_{OUT}
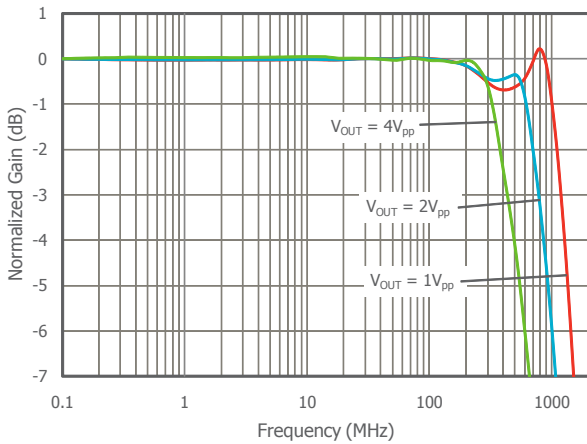
Frequency Response vs. Temperature
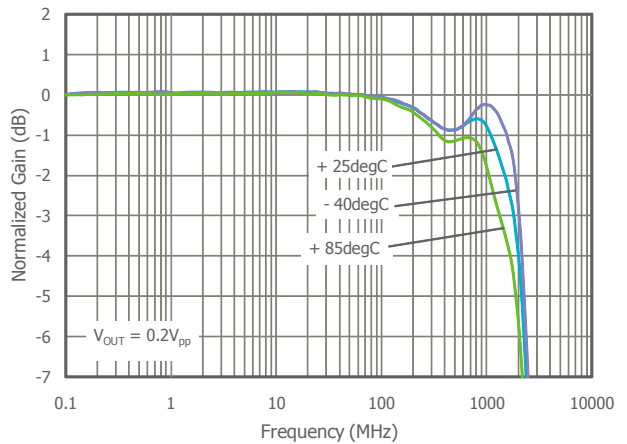
COMLINEAR CLC1605, CLC3605 Single and Triple, 1.5GHz Amplifiers Rev 1A

Typical Performance Characteristics

$T_A = 25°C$, $V_S = ±5V$, $R_f = R_g = 330Ω$, $R_L = 150Ω$ to GND, G = 2; unless otherwise noted.

Non-Inverting Frequency Response at $V_S = 5V$
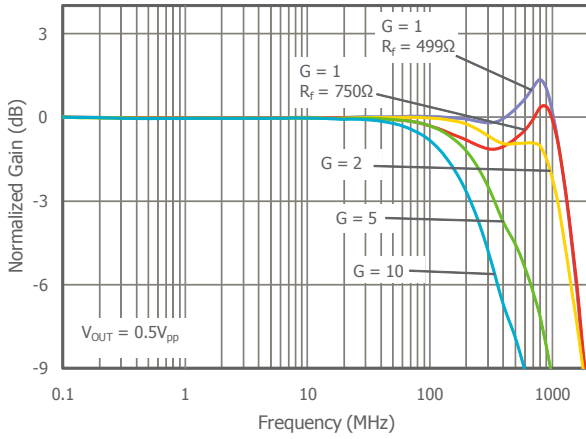
Inverting Frequency Response at $V_S = 5V$
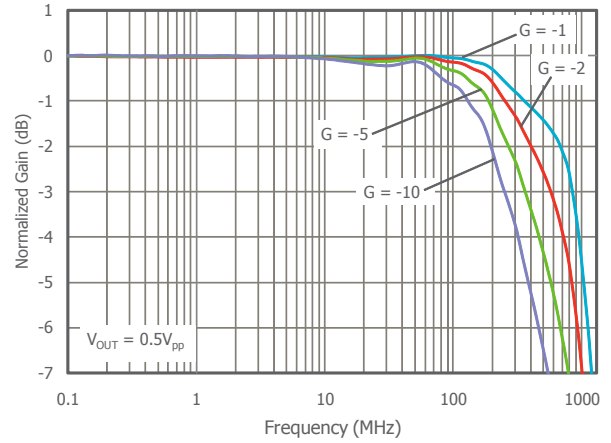
Frequency Response vs. C_L at $V_S = 5V$
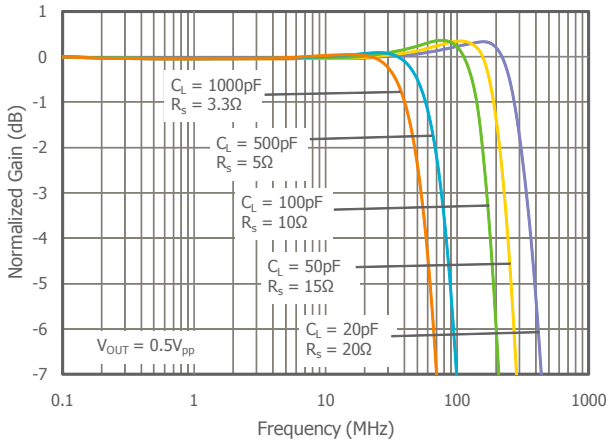
Frequency Response vs. R_L at $V_S = 5V$
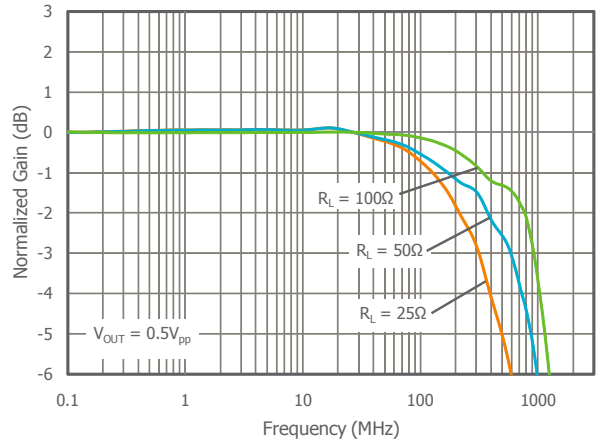
Frequency Response vs. V_{OUT} at $V_S = 5V$
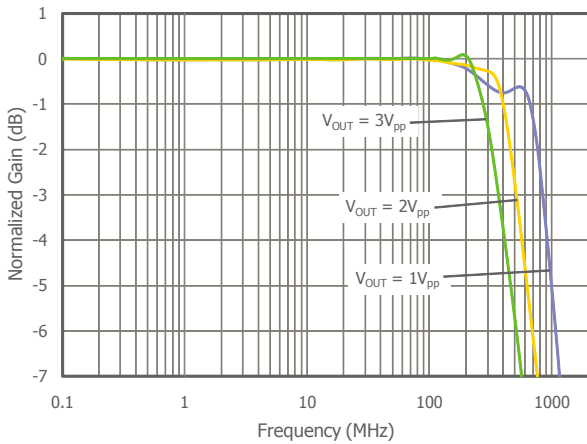
Frequency Response vs. Temperature at $V_S = 5V$
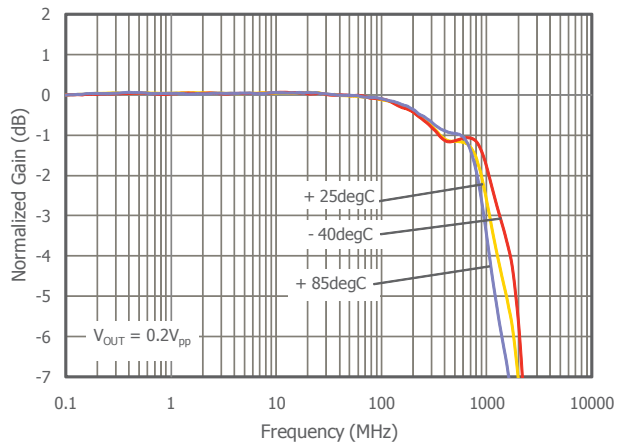
Typical Performance Characteristics - Continued

$T_A = 25°C$, $V_S = ±5V$, $R_f = R_g = 330Ω$, $R_L = 150Ω$ to GND, G = 2; unless otherwise noted.

Gain Flatness

Normalized Gain (dB) vs. Frequency (MHz)

$V_{OUT} = 2V_{pp}$
$R_L = 150Ω$
$R_f = 330Ω$

Gain Flatness at $V_S = 5V$

Nomalized Gain (dB) vs. Frequency (MHz)

$V_{OUT} = 2V_{pp}$
$R_L = 150Ω$
$R_f = 330Ω$
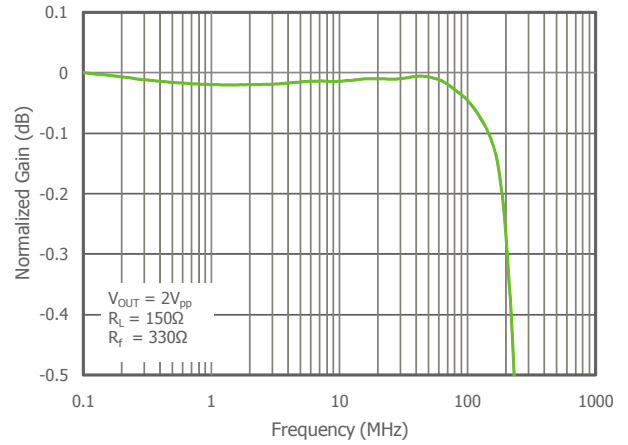
-3dB Bandwidth vs. V_{OUT}

-3dB Bandwidth (MHz) vs. V_{OUT} (V_{PP})
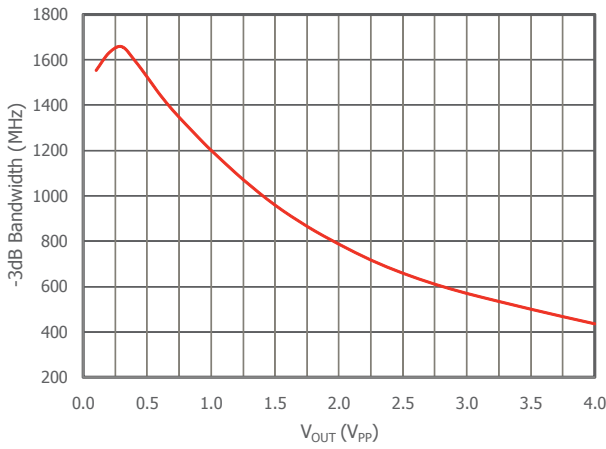
-3dB Bandwidth vs. V_{OUT} at $V_S = 5V$

-3dB Bandwidth (MHz) vs. V_{OUT} (V_{PP})
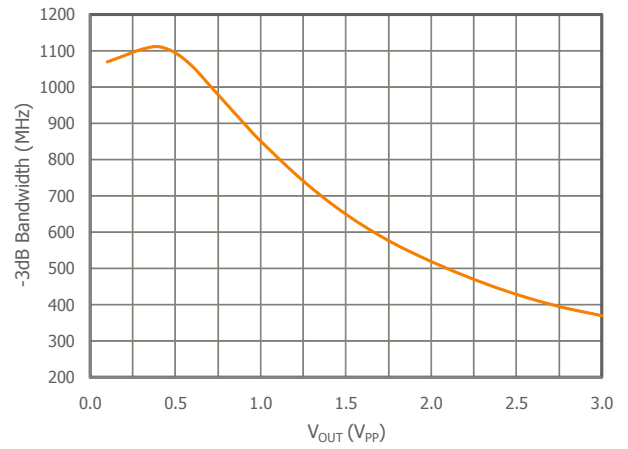
Closed Loop Output Impedance vs. Frequency
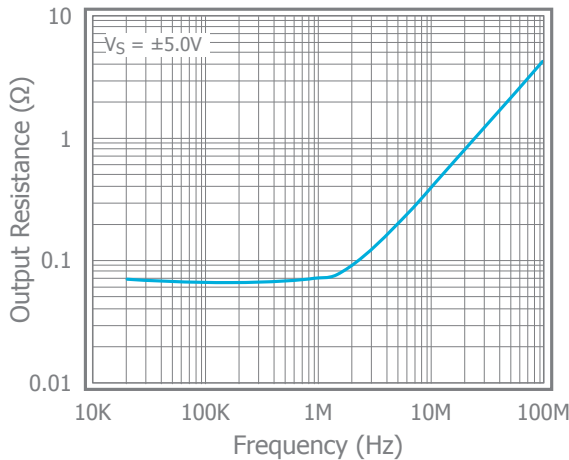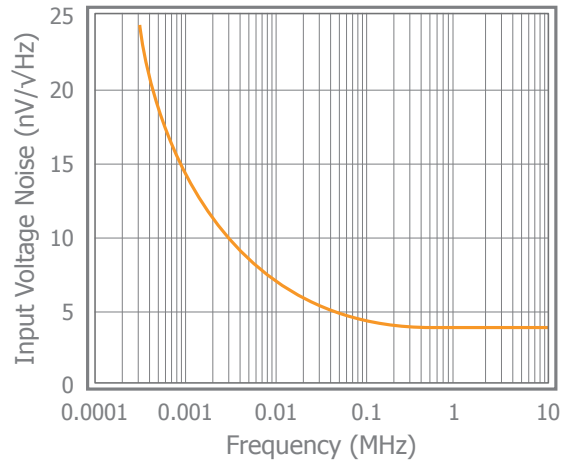
Output Resistance (Ω) vs. Frequency (Hz)

$V_S = ±5.0V$

Input Voltage Noise

Input Voltage Noise (nV/√Hz) vs. Frequency (MHz)

COMLINEAR CLC1605, CLC3605 Single and Triple, 1.5GHz Amplifiers Rev 1A

Typical Performance Characteristics - Continued

$T_A = 25°C$, $V_S = \pm5V$, $R_f = R_g = 330Ω$, $R_L = 150Ω$ to GND, $G = 2$; unless otherwise noted.

2nd Harmonic Distortion vs. R_L
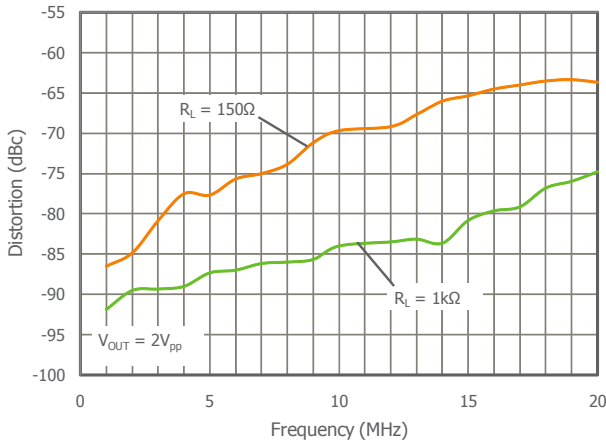
3rd Harmonic Distortion vs. R_L
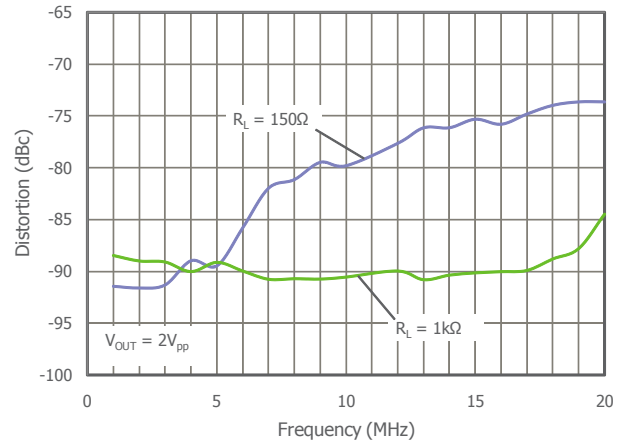
2nd Harmonic Distortion vs. V_{OUT}
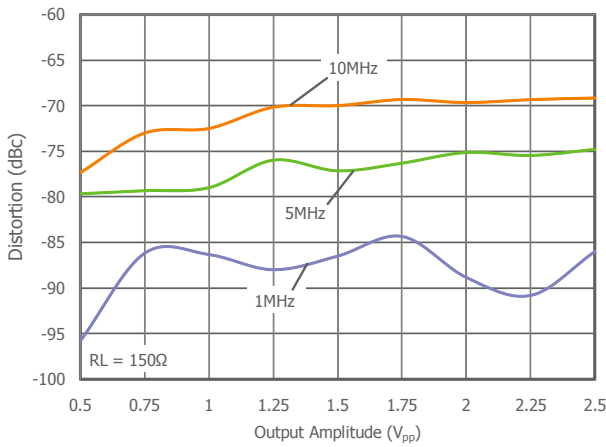
3rd Harmonic Distortion vs. V_{OUT}
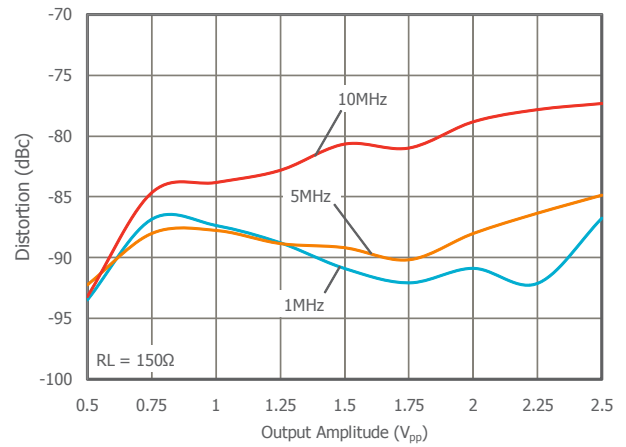
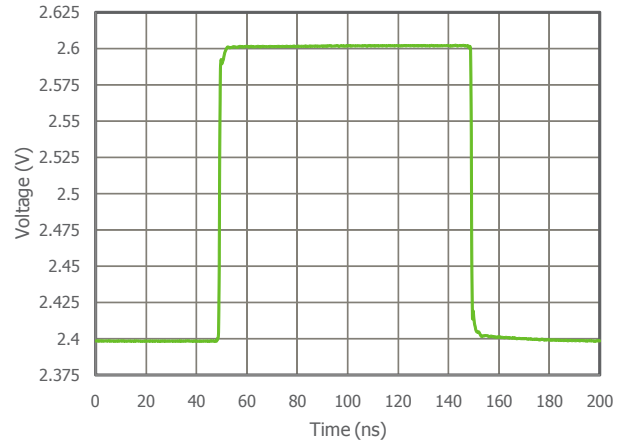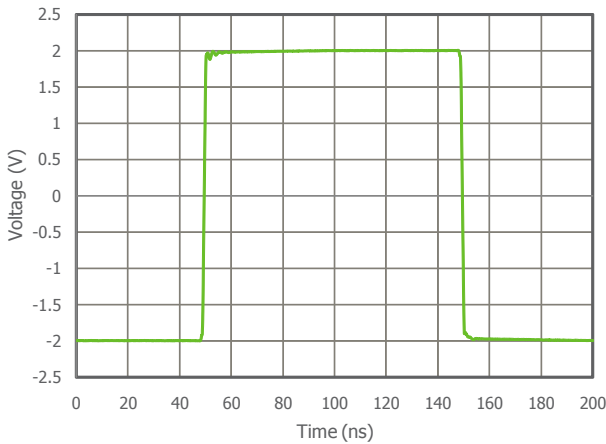### CMRR vs. Frequency
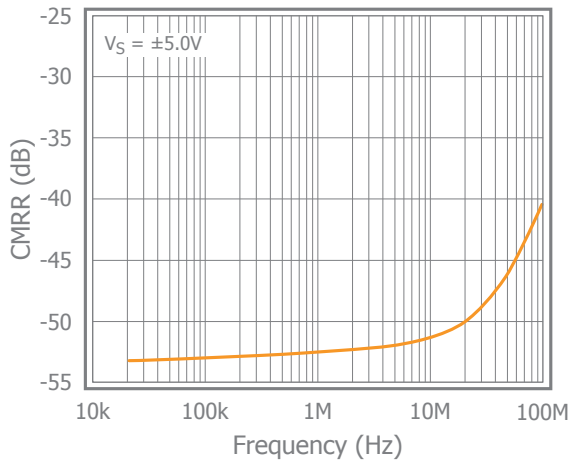
PSRR vs. Frequency
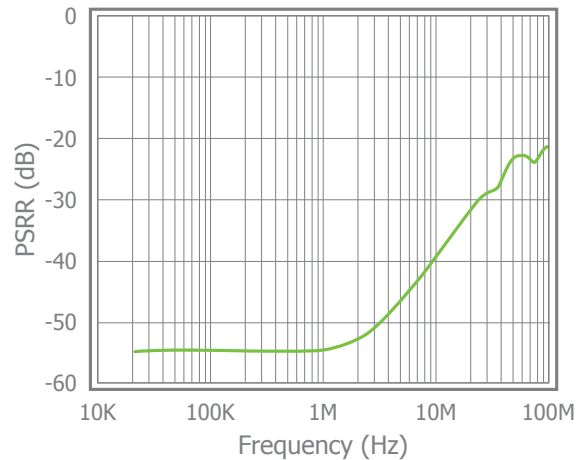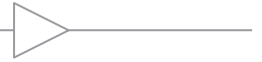
COMLINEAR CLC1605, CLC3605 Single and Triple, 1.5GHz Amplifiers Rev 1A

Typical Performance Characteristics - Continued

$T_A = 25°C$, $V_S = ±5V$, $R_f = R_g = 330Ω$, $R_L = 150Ω$ to GND, $G = 2$; unless otherwise noted.

Small Signal Pulse Response
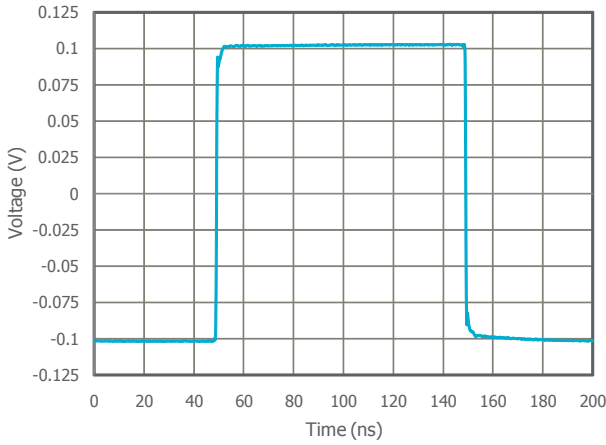
Small Signal Pulse Response at $V_S = 5V$

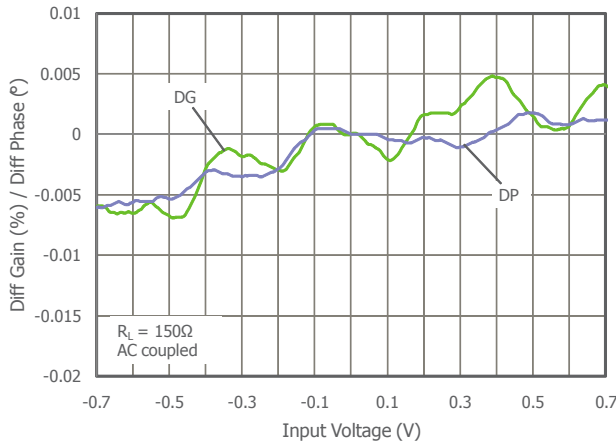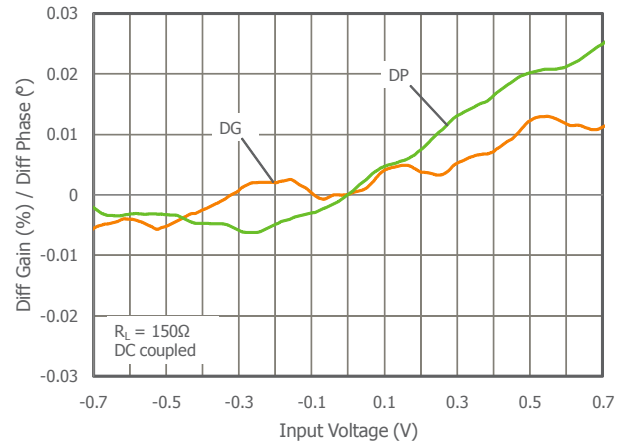
Large Signal Pulse Response

Large Signal Pulse Response at $V_S = 5V$
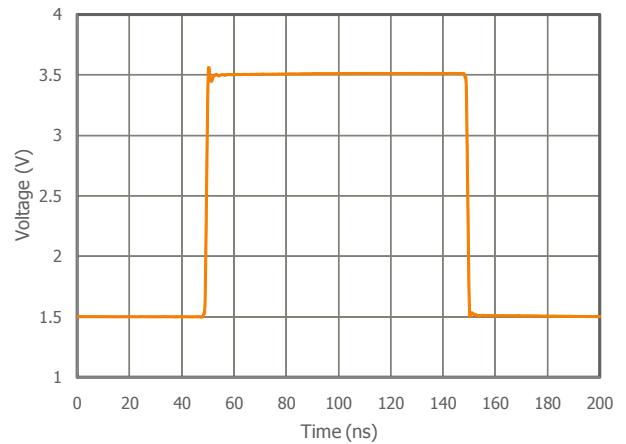
Differential Gain & Phase AC Coupled Output
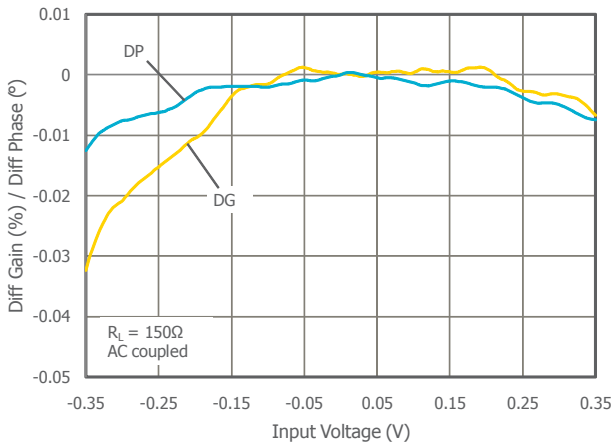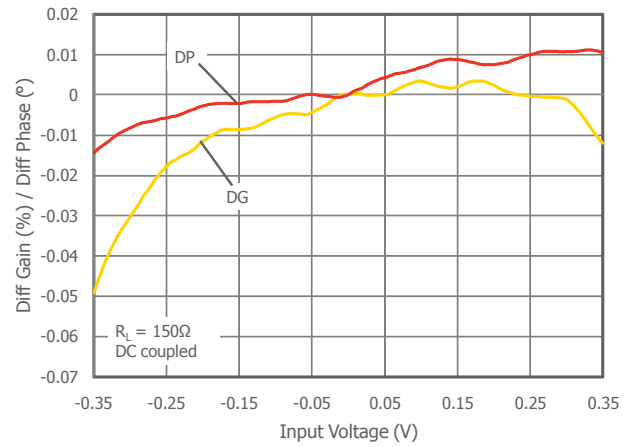

Differential Gain & Phase DC Coupled Output

COMLINEAR CLC1605, CLC3605 Single and Triple, 1.5GHz Amplifiers Rev 1A

Typical Performance Characteristics - Continued

$T_A = 25°C$, $V_S = ±5V$, $R_f = R_g = 330Ω$, $R_L = 150Ω$ to GND, G = 2; unless otherwise noted.

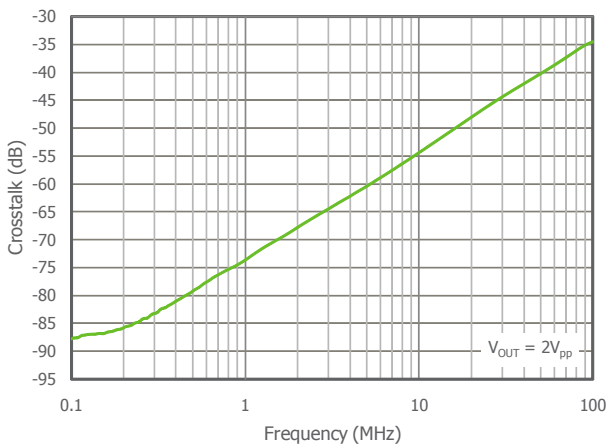### Differential Gain & Phase AC Coupled Output at $V_S = ±2.5V$

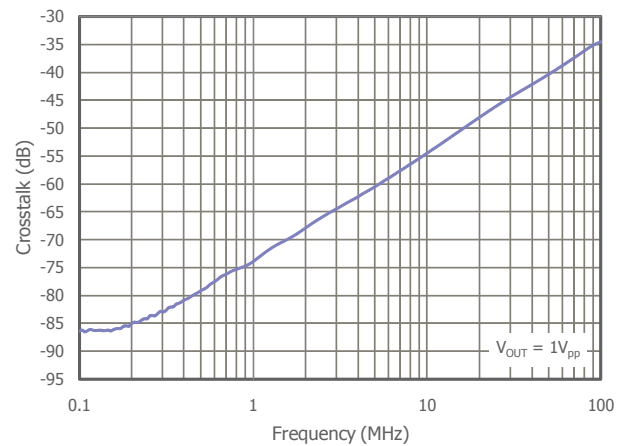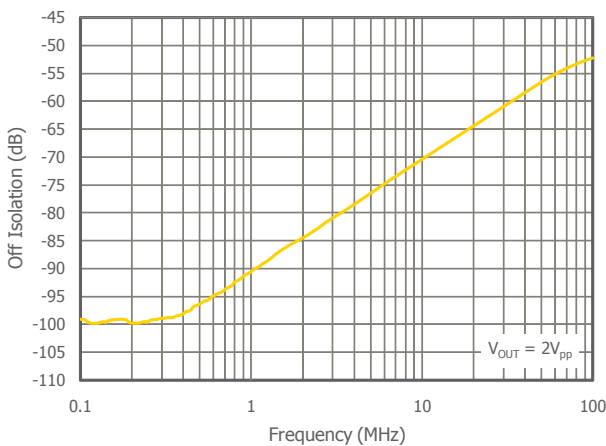### Differential Gain & Phase DC Coupled at $V_S = ±2.5V$
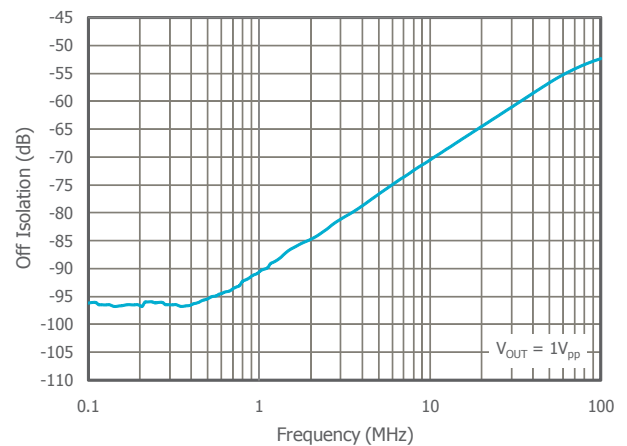
Crosstalk vs. Frequency (CLC3605)

Crosstalk vs. Frequency at $V_S=5V$ (CLC3605)

Off Isolation vs. Frequency

Off Isolation vs. Frequency at $V_S=5V$

General Information - Current Feedback Technology

Advantages of CFB Technology

The CLC1605 Family of amplifiers utilize current feedback (CFB) technology to achieve superior performance. The primary advantage of CFB technology is higher slew rate performance when compared to voltage feedback (VFB) architecture. High slew rate contributes directly to better large signal pulse response, full power bandwidth, and distortion.

CFB also alleviates the traditional trade-off between closed loop gain and usable bandwidth that is seen with a VFB amplifier. With CFB, the bandwidth is primarily determined by the value of the feedback resistor, R_f. By using optimum feedback resistor values, the bandwidth of a CFB amplifier remains nearly constant with different gain configurations.

When designing with CFB amplifiers always abide by these basic rules:

• Use the recommended feedback resistor value

• Do not use reactive (capacitors, diodes, inductors, etc.) elements in the direct feedback path

• Avoid stray or parasitic capacitance across feedback resistors

• Follow general high-speed amplifier layout guidelines

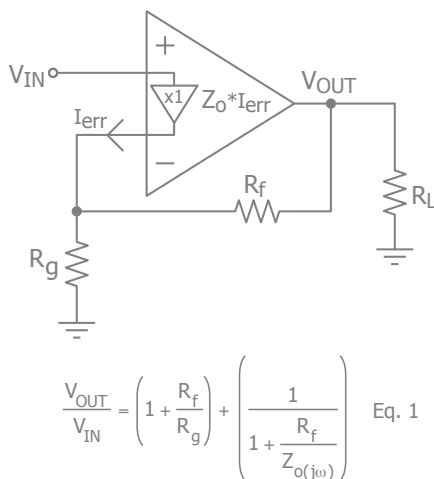• Ensure proper precautions have been made for driving capacitive loads

$$\frac{V_{OUT}}{V_{IN}} = \left(1 + \frac{R_f}{R_g}\right) + \left(\frac{1}{1 + \frac{R_f}{Z_{o(j\omega)}}}\right) \quad \text{Eq. 1}$$

Figure 1. Non-Inverting Gain Configuration with First Order Transfer Function

$$\frac{V_{OUT}}{V_{IN}} = \left(-\frac{R_f}{R_g}\right) + \left(\frac{1}{1 + \frac{R_f}{Z_{o(j\omega)}}}\right) \quad \text{Eq. 2}$$
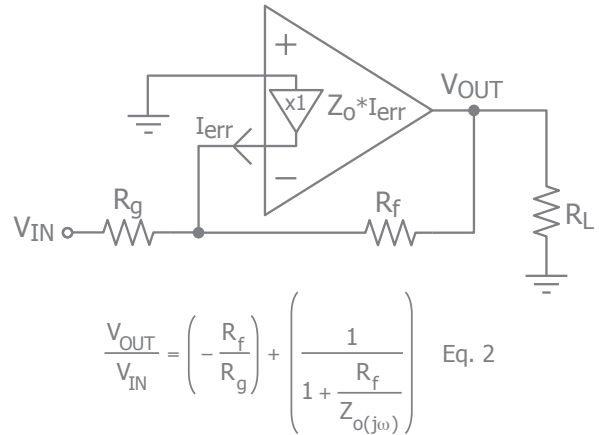
Figure 2. Inverting Gain Configuration with First Order Transfer Function

CFB Technology - Theory of Operation

Figure 1 shows a simple representation of a current feedback amplifier that is configured in the traditional non-inverting gain configuration.

Instead of having two high-impedance inputs similar to a VFB amplifier, the inputs of a CFB amplifier are connected across a unity gain buffer. This buffer has a high impedance input and a low impedance output. It can source or sink current (I_{err}) as needed to force the non-inverting input to track the value of Vin. The CFB architecture employs a high gain trans-impedance stage that senses Ierr and drives the output to a value of ($Z_o(j\omega) * I_{err}$) volts. With the application of negative feedback, the amplifier will drive the output to a voltage in a manner which tries to drive Ierr to zero. In practice, primarily due to limitations on the value of $Z_o(j\omega)$, Ierr remains a small but finite value.

A closer look at the closed loop transfer function (Eq.1) shows the effect of the trans-impedance, $Z_o(j\omega)$ on the gain of the circuit. At low frequencies where $Z_o(j\omega)$ is very large with respect to R_f, the second term of the equation approaches unity, allowing R_f and R_g to set the gain. At higher frequencies, the value of $Z_o(j\omega)$ will roll off, and the effect of the secondary term will begin to dominate. The -3dB small signal parameter specifies the frequency where the value $Z_o(j\omega)$ equals the value of R_f causing the gain to drop by 0.707 of the value at DC.

For more information regarding current feedback amplifiers, visit www.cadeka.com for detailed application notes, such as AN-3: *The Ins and Outs of Current Feedback Amplifiers*.

Application Information

Basic Operation

Figures 3, 4, and 5 illustrate typical circuit configurations for non-inverting, inverting, and unity gain topologies for dual supply applications. They show the recommended bypass capacitor values and overall closed loop gain equations.
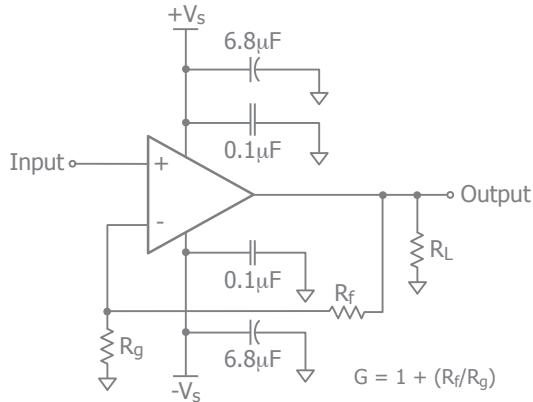

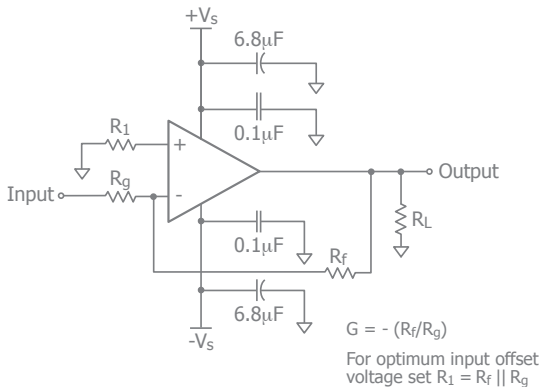Figure 3. Typical Non-Inverting Gain Circuit

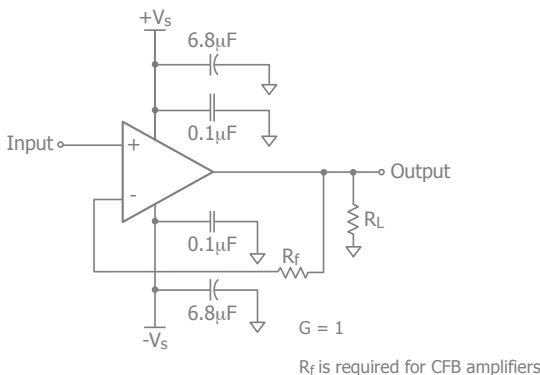Figure 4. Typical Inverting Gain Circuit

Figure 5. Typical Unity Gain (G=1) Circuit

CFB amplifiers can be used in unity gain configurations. Do not use the traditional voltage follower circuit, where the output is tied directly to the inverting input. With a CFB amplifier, a feedback resistor of appropriate value must be used to prevent unstable behavior. Refer to figure 5 and Table 1. Although this seems cumbersome, it does allow a degree of freedom to adjust the passband characteristics.

Feedback Resistor Selection

One of the key design considerations when using a CFB amplifier is the selection of the feedback resistor, R_f. R_f is used in conjunction with R_g to set the gain in the traditional non-inverting and inverting circuit configurations. Refer to figures 3 and 4. As discussed in the Current Feedback Technology section, the value of the feedback resistor has a pronounced effect on the frequency response of the circuit.

Table 1, provides recommended R_f and associated R_g values for various gain settings. These values produce the optimum frequency response, maximum bandwidth with minimum peaking. Adjust these values to optimize performance for a specific application. The typical performance characteristics section includes plots that illustrate how the bandwidth is directly affected by the value of R_f at various gain settings.

Gain (V/V)	R_f (Ω)	R_g (Ω)	±0.1dB BW (MHz)	-3dB BW (MHz)
1	499	-	167	1500
2	330	330	120	1200
5	330	82.5	66	385
10	330	33	38	245

Table 1: Recommended R_f vs. Gain

In general, lowering the value of R_f from the recommended value will extend the bandwidth at the expense of additional high frequency gain peaking. This will cause increased overshoot and ringing in the pulse response characteristics. Reducing R_f too much will eventually cause oscillatory behavior.

Increasing the value of R_f will lower the bandwidth. Lowering the bandwidth creates a flatter frequency response and improves 0.1dB bandwidth performance. This is important in applications such as video. Further increase in R_f will cause premature gain rolloff and adversely affect gain flatness.

Driving Capacitive Loads

Increased phase delay at the output due to capacitive loading can cause ringing, peaking in the frequency response, and possible unstable behavior. Use a series resistance, R_S, between the amplifier and the load to help improve stability and settling performance. Refer to Figure 6.
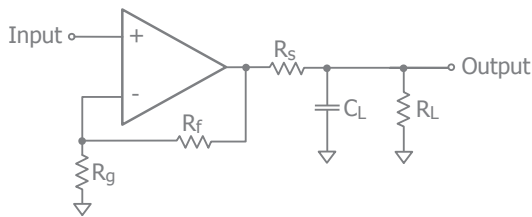

Figure 6. Addition of R_S for Driving Capacitive Loads

Table 2 provides the recommended R_S for various capacitive loads. The recommended R_S values result in <=0.5dB peaking in the frequency response. The Frequency Response vs. C_L plot, on page 5, illustrates the response of the CLC1605 Family.

C_L (pF)	R_S (Ω)	-3dB BW (MHz)
20	20	350
50	15	235
100	10	170
500	5	75
1000	3.3	52

Table 1: Recommended R_S vs. C_L

For a given load capacitance, adjust R_S to optimize the tradeoff between settling time and bandwidth. In general, reducing R_S will increase bandwidth at the expense of additional overshoot and ringing.

Parasitic Capacitance on the Inverting Input

Physical connections between components create unintentional or parasitic resistive, capacitive, and inductive elements.

Parasitic capacitance at the inverting input can be especially troublesome with high frequency amplifiers. A parasitic capacitance on this node will be in parallel with the gain setting resistor R_g. At high frequencies, its impedance can begin to raise the system gain by making R_g appear smaller.

In general, avoid adding any additional parasitic capacitance at this node. In addition, stray capacitance across the R_f resistor can induce peaking and high frequency ringing. Refer to the **Layout Considerations** section for additional information regarding high speed layout techniques.

Overdrive Recovery

An overdrive condition is defined as the point when either one of the inputs or the output exceed their specified voltage range. Overdrive recovery is the time needed for the amplifier to return to its normal or linear operating point. The recovery time varies, based on whether the input or output is overdriven and by how much the range is exceeded. The CLC1605 Family will typically recover in less than 10ns from an overdrive condition. Figure 7 shows the CLC1605 in an overdriven condition.
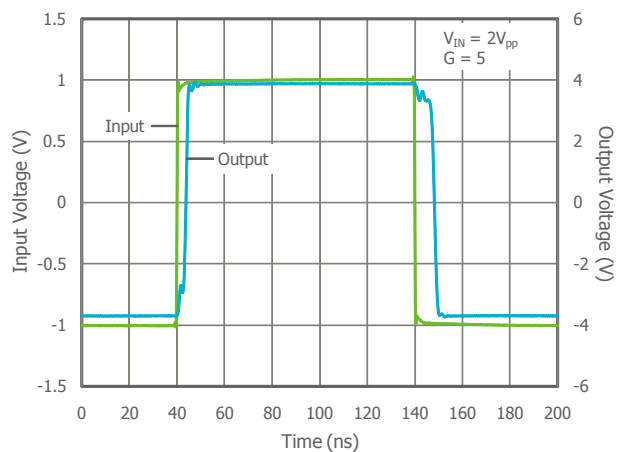

Figure 7. Overdrive Recovery

Power Dissipation

Power dissipation should not be a factor when operating under the stated 1000 ohm load condition. However, applications with low impedance, DC coupled loads should be analyzed to ensure that maximum allowed junction temperature is not exceeded. Guidelines listed below can be used to verify that the particular application will not cause the device to operate beyond it's intended operating range.

Maximum power levels are set by the absolute maximum junction rating of 150°C. To calculate the junction temperature, the package thermal resistance value Theta$_{JA}$ (Θ_{JA}) is used along with the total die power dissipation.

$$T_{Junction} = T_{Ambient} + (\Theta_{JA} \times P_D)$$

Where $T_{Ambient}$ is the temperature of the working environment.

In order to determine P_D, the power dissipated in the load needs to be subtracted from the total power delivered by the supplies.

$$P_D = P_{supply} - P_{load}$$

Supply power is calculated by the standard power equation.

$$P_{supply} = V_{supply} \times I_{RMS\ supply}$$

$$V_{supply} = V_{S+} - V_{S-}$$

Power delivered to a purely resistive load is:

$$P_{load} = ((V_{LOAD})_{RMS}^2)/Rload_{eff}$$

The effective load resistor ($Rload_{eff}$) will need to include the effect of the feedback network. For instance,

$Rload_{eff}$ in figure 3 would be calculated as:

$$R_L\ ||\ (R_f + R_g)$$

These measurements are basic and are relatively easy to perform with standard lab equipment. For design purposes however, prior knowledge of actual signal levels and load impedance is needed to determine the dissipated power. Here, P_D can be found from

$$P_D = P_{Quiescent} + P_{Dynamic} - P_{Load}$$

Quiescent power can be derived from the specified I_S values along with known supply voltage, V_{Supply}. Load power can be calculated as above with the desired signal amplitudes using:

$$(V_{LOAD})_{RMS} = V_{PEAK} / \sqrt{2}$$

$$(\ I_{LOAD})_{RMS} = (\ V_{LOAD})_{RMS} / Rload_{eff}$$

The dynamic power is focused primarily within the output stage driving the load. This value can be calculated as:

$$P_{DYNAMIC} = (V_{S+} - V_{LOAD})_{RMS} \times (\ I_{LOAD})_{RMS}$$

Assuming the load is referenced in the middle of the power rails or $V_{supply}/2$.

Figure 8 shows the maximum safe power dissipation in the package vs. the ambient temperature for the available packages.
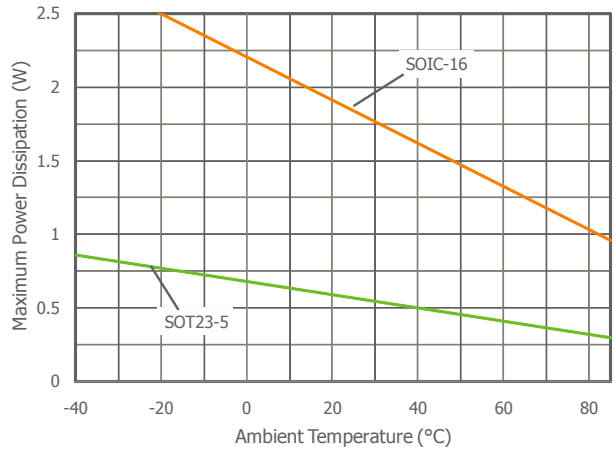

Figure 8. Maximum Power Derating

Better thermal ratings can be achieved by maximizing PC board metallization at the package pins. However, be careful of stray capacitance on the input pins.

In addition, increased airflow across the package can also help to reduce the effective Θ_{JA} of the package.

In the event the outputs are momentarily shorted to a low impedance path, internal circuitry and output metallization are set to limit and handle up to 65mA of output current. However, extended duration under these conditions may not guarantee that the maximum junction temperature (+150°C) is not exceeded.

Layout Considerations

General layout and supply bypassing play major roles in high frequency performance. CADEKA has evaluation boards to use as a guide for high frequency layout and as aid in device testing and characterization. Follow the steps below as a basis for high frequency layout:

• Include 6.8µF and 0.1µF ceramic capacitors for power supply decoupling

• Place the 6.8µF capacitor within 0.75 inches of the power pin

• Place the 0.1µF capacitor within 0.1 inches of the power pin

• Remove the ground plane under and around the part, especially near the input and output pins to reduce parasitic capacitance

• Minimize all trace lengths to reduce series inductances

Refer to the evaluation board layouts below for more information.

Evaluation Board Information

The following evaluation boards are available to aid in the testing and layout of these devices:

Evaluation Board	Products
CEB002	CLC1605
CEB013	CLC3605

Evaluation Board Schematics

Evaluation board schematics and layouts are shown in Figures 9-14. These evaluation boards are built for dual- supply operation. Follow these steps to use the board in a single-supply application:

1. Short -Vs to ground.

2. Use C3 and C4, if the -V$_S$ pin of the amplifier is not directly connected to the ground plane.
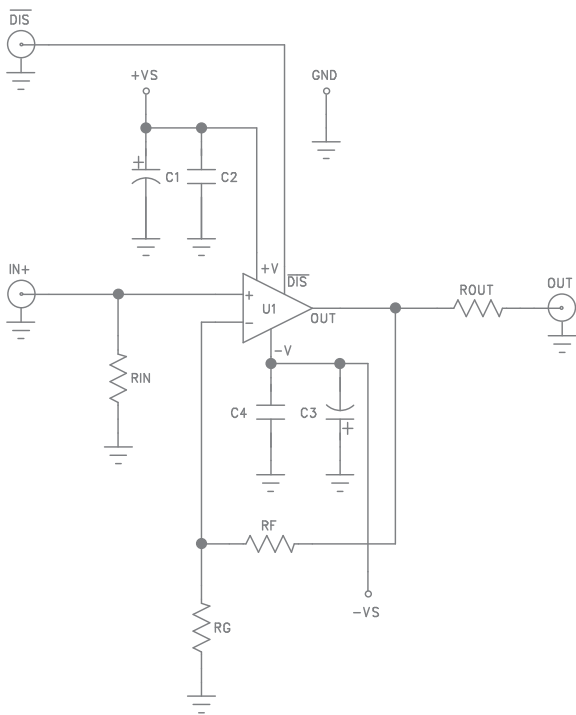
Figure 9. CEB002 Schematic
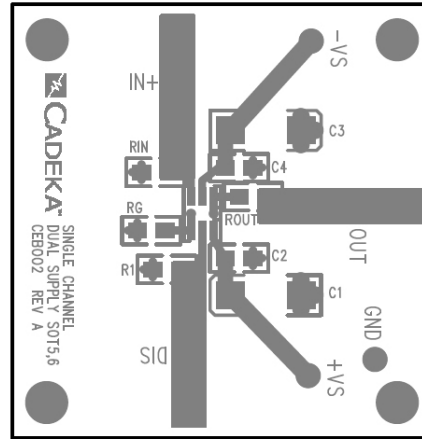
Figure 10. CEB002 Top View
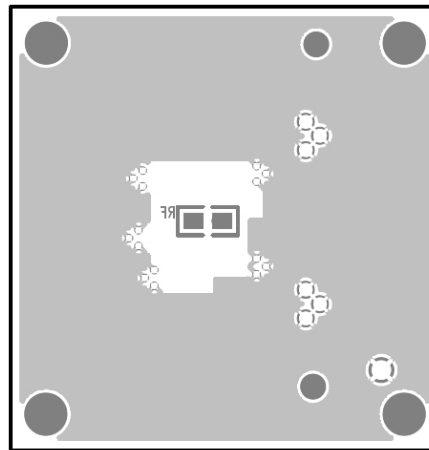
Figure 11. CEB002 Bottom View
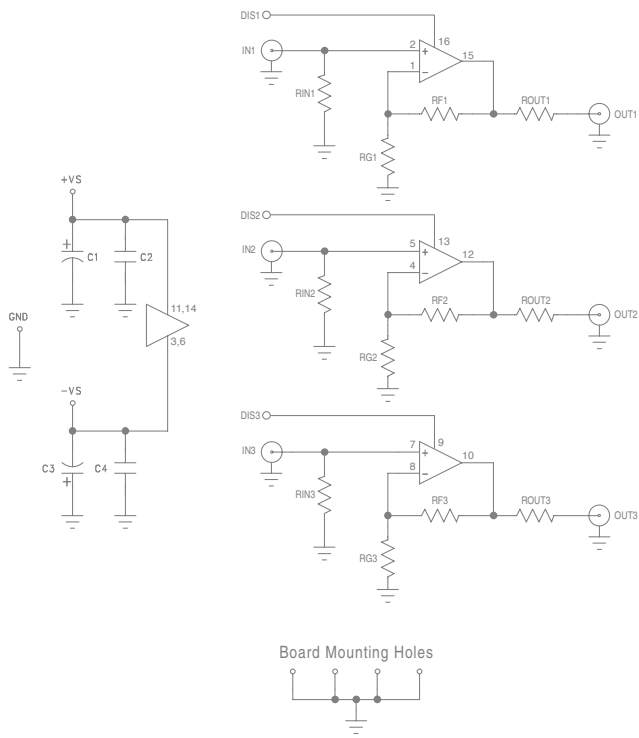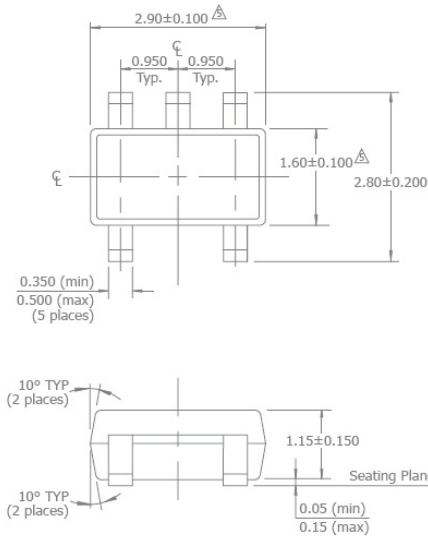
Figure 12. CEB013 Schematic
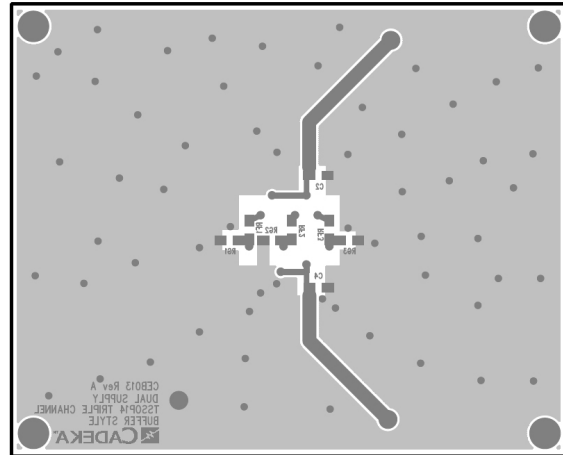
Figure 14. CEB013 Bottom View
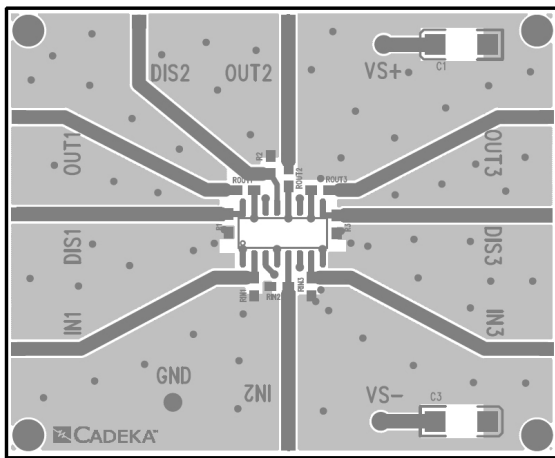
Figure 13. CEB013 Top View

Mechanical Dimensions

SOT23-5 Package

NOTES:
1. Dimensions and tolerances are as per ANSI Y14.5M-1982.
2. Package surface to be matte finish VDI 11~13.
3. Die is facing up for mold. Die is facing down for trim/form, ie. reverse trim/form.
4. The footlength measuring is based on the guage plane method.
⚠ Dimension are exclusive of mold flash and gate burr.
⚠ Dimension are exclusive of solder plating.
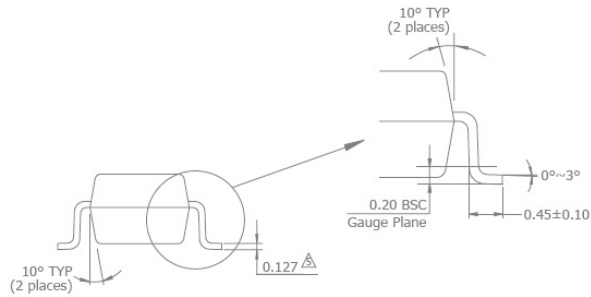
SOIC-16 Package
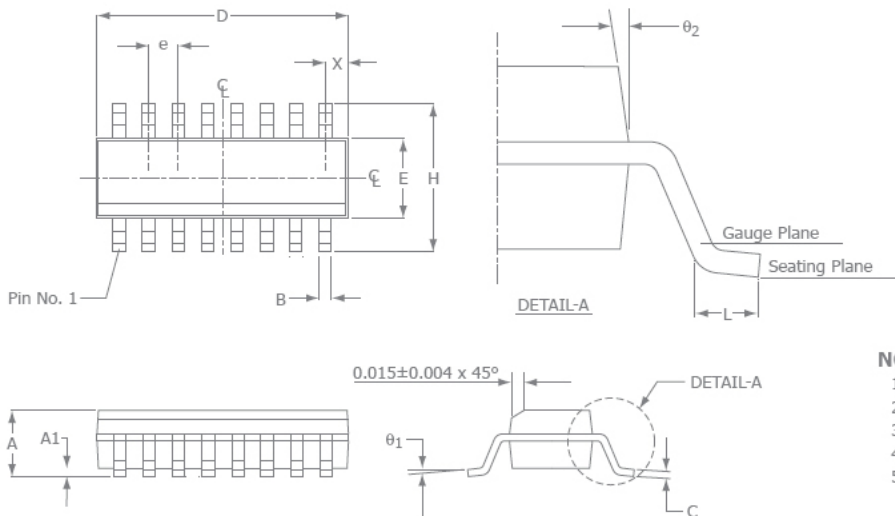
SOIC-16		
SYMBOL	MIN	MAX
A	0.054	0.068
A1	0.004	0.0098
B	0.014	0.019
D	0.386	0.393
E	0.150	0.157
H	0.229	0.244
e	0.050 BSC	
C	0.0075	0.0098
L	0.016	0.034
X	0.020 Ref	
θ1	0°	8°
θ2	7° BSC	

NOTE:
1. All dimensions are in inches.
2. Lead coplanarity should be 0" to 0.004" max.
3. Package surface finishing: VDI 24~27
4. All dimension excluding mold flashes.
5. The lead width, B to be determined at 0.0075" from the lead tip.

For additional information regarding our products, please visit CADEKA at: cadeka.com

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