# THREE PHASE POWER/ENERGY METERING IC WITH INSTANTANEOUS PULSE OUTPUT 

## FEATURES

- Output frequency represents the absolute sum of energy on all three phases
- Performs one, two or three phase power and energy measurement
- Meets the IEC 521/1036 Specification requirements for Class 1 AC Watt hour meters
- Operates over a wide temperature range
- Current transformers for sensing
- Excellent long term stability
- Easily adaptable to different signal levels
- Precision voltage reference onchip
- Pin selectable pulse rates
- Support tamper detection


## FUNCTIONAL DESCRIPTION:

The IL19006 Three Phase Power/Energy metering integrated circuit generates a pulse rate output, the frequency of which is proportional to the absolute power consumption. The IL19006 performs the calculations of active power.
The method of calculation takes the power factor into account.
Energy consumption is determined by the power measurement being integrated over time.
The output of this universal three phase power/energy metering integrated circuit, is ideally suited for applications such as residential and industrial energy metering and control.

The IL19006 Three Phase Power/Energy metering integrated circuit is a CMOS mixed signal Analog/Digital integrated circuit, which performs three phase power/energy calculations over a range of 1000:1, to an overall accuracy of better than Class 1.
The integrated circuit includes all the required functions for 3-phase power and energy measurement such as oversampling A/D converters for the voltage and current sense inputs, power calculation and energy integration. Internal offsets are eliminated through the use of cancellation procedures.
The IL19006 generates pulses, the frequency of which is proportional to the power consumption. Two frequency outputs (FOUT1 and FOUT2) are available. The pulse rate follows the instantaneous power measured.

## BLOCK DIAGRAM



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## ABSOLUTE MAXIMUM RATINGS*

| Parameter | Symbol | Min | Max | Unit |
| :--- | :---: | :---: | :---: | :---: |
| Supply Voltage | $\mathrm{V}_{\text {DD }}-\mathrm{V}_{\text {SS }}$ | -0.3 | 6.0 | V |
| Current on anv Pin | $\mathrm{I}_{\mathrm{PIN}}$ | -150 | +150 | mA |
| Storaqe Temperature | $\mathrm{T}_{\text {STG }}$ | -40 | +125 | ${ }^{\circ} \mathrm{C}$ |
| Operating Temperature | $\mathrm{T}_{\mathrm{O}}$ | -40 | +85 | ${ }^{\circ} \mathrm{C}$ |
| Current at any pin | $\mathrm{I}_{\mathrm{p}}$ | -100 | 100 | mA |

* Stresses above those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress rating only. Functional operation of the device at these or any other conditions above those indicated in the operation sections of this specification, is not implied. Exposure to Absolute Maximum Ratings for extended periods may affect device reliability.


## ELECTRICAL CHARACTERISTICS

( $\mathrm{V}_{\mathrm{DD}}=2.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{SS}}=-2.5 \mathrm{~V}$, over the temperature range $-10^{\circ} \mathrm{C}$ to $+70^{\circ} \mathrm{C}$, unless otherwise specified.)

| Parameter | Svmbol | Min | Tvp | Maxf | Uni | Condition |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Operating Temperature Ranges | To | -25 |  | +85 | ${ }^{0} \mathrm{C}$ |  |
| Supply Voltage | $\mathrm{V}_{\mathrm{DD}}-\mathrm{V}_{\text {SS }}$ | 4.5 |  | 5.5 | V |  |
| Supplv Current | 1 n |  |  | 15 | mA |  |
| Nonlinearity of Power Calculation |  | -0.3 |  | +0.3 | \% | $1 \%-100 \%$ of rated power |
| Current Sensor Inputs (Differential) |  |  |  |  |  |  |
| Input Current Range | $I_{11}$ | -25 |  | +25 | $\mu \mathrm{A}$ | Peak value |
| Voltage Sensor Induts (Asvmmetric) |  |  |  |  |  |  |
| Input Current Range | IV | -25 |  | +25 | $\mu \mathrm{A}$ | Peak value |
| Pins FOUT1, FOUT2, DIR <br> Output Low Voltage Output High Voltage | $\begin{aligned} & \mathrm{V}_{\mathrm{OL}} \\ & \mathrm{~V}_{\mathrm{OH}} \end{aligned}$ | $\mathrm{V}_{\mathrm{DD}-1}$ |  | $\mathrm{V}_{\text {ss }}+1$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \end{aligned}$ | $\begin{aligned} & \mathrm{l}_{\mathrm{OL}}=5 \mathrm{~mA} \\ & \mathrm{l}_{\mathrm{OH}}=-2 \mathrm{~mA} \end{aligned}$ |
| Pulse Rate: FOUT1 | fp | 10 |  | $\begin{aligned} & 1160 \\ & 3000 \end{aligned}$ | $\begin{aligned} & \mathrm{Hz} \\ & \mathrm{~Hz} \end{aligned}$ | Specified linearity Min and max limits |
| FOUT2 |  |  |  |  |  | User selectable |
| Oscillator | Recomm TV colou | mended ur bur | crysta cryst | $\mathrm{f}=3 .$ | $5795$ | MHz |
| $\begin{aligned} \hline \text { Pin VREF } & \\ & \text { Ref. Current } \\ & \text { Ref. Voltage } \end{aligned}$ | $\begin{aligned} & -I_{R} \\ & V_{R} \end{aligned}$ | $\begin{aligned} & 45 \\ & 1.1 \end{aligned}$ | 50 | $\begin{aligned} & 55 \\ & 1.3 \end{aligned}$ | $\begin{gathered} \mu \mathrm{A} \\ \mathrm{~V} \end{gathered}$ | With $\mathrm{R}=24 \mathrm{k} \Omega$ connected to $\mathrm{V}_{\mathrm{SS}}$ Referred to $\mathrm{V}_{\mathrm{Ss}}$ |

ILA19006
PIN DESCRIPTION

| Pin | Designation | Description |  |
| :---: | :---: | :--- | :---: |
| 16 | GND | Ground |  |
| 6 | VDD | Positive Supply Voltage |  |
| 14 | VSS | Negative Supply Voltage |  |
| 17 | IVN1 | Analog Input for Voltage: Phase 1 |  |
| 20 | IVN2 | Analog Input for Voltage: Phase 2 |  |
| 3 | IVN3 | Analog Input for Voltage: Phase 3 |  |
| 19 | IIN1 | Inputs for current sensor-: Phase 1 |  |
| 18 | IIP1 |  |  |
| 2 | IIN2 | Inputs for current sensor : Phase 2 |  |
| 1 | IIP2 |  |  |
| 5 | IIN3 | Inputs for current sensor: Phase 3 |  |
| 4 | IIP3 |  |  |
| 10 | OSC1 | Connections for crystal or ceramic resonator |  |
| 11 | OSC2 | (OSC1=Input; OSC2=Output) |  |
| 7 | FOUT1 | Pulse rate outputs |  |
| 8 | FOUT2 |  |  |
| 9 | DIR | Direction indicator |  |
| 12 | PGM0 | FOUT2 Frequency select pins |  |
| 13 | PGM1 |  |  |
| 15 | VREF | Connection for current setting resistor |  |

Note: arrangement of pins according to analog SA9605A (Sames)

## FUNCTIONAL DESCRIPTION

The IL19006 is a CMOS mixed signal Analog/Digital integrated circuit, which performs three phase power/energy calculations over a range of 1000:1, to an overall accuracy of better than Class 1.
The IL19006 in both DIP-20 and SOIC-20 package options is functionally similar to the SA9105E and SA9105F with the advantage of no external loop capacitors.
The integrated circuit includes all the required functions for 3-phase power and energy measurement such as oversampling A/D converters for the voltage and current sense inputs, power calculation and energy integration. Internal offsets are eliminated through the use of cancellation procedures.
The IL19006 generates pulses, the frequency of which is proportional to the power consumption. Two frequency outputs (FOUT1 and FOUT2) are available. The pulse rate follows the instantaneous power measured.

## 1. Power Calculation

In the Application Circuit (Figure 1), the mains voltages from Line 1, Line 2 and Line 3 , are converted to currents and applied to the voltage sense inputs IVN1, IVN2 and

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IVN3.
The current levels on the voltage sense inputs are derived from the mains voltage ( $3 \times 230 \mathrm{VAC}$ ) being divided down through voltage dividers to 14 V . The resulting input currents into the A/D converters are $14 \mu \mathrm{~A}$ through the resistors $\mathrm{R}_{15}, \mathrm{R}_{16}$ and $\mathrm{R}_{17}$.
For the current sense inputs the voltage drop across the current transformers terminating resistors are converted to currents of $16 \mu \mathrm{~A}$ for rated conditions, by means of resistors $\mathrm{R}_{8}, \mathrm{R}_{9}$ (Phase 1); $\mathrm{R}_{10}, \mathrm{R}_{11}$ (Phase 2); and $\mathrm{R}_{12}, \mathrm{R}_{13}$ (Phase 3). The signals providing the current information are applied to the current sensor inputs: IIN1, IIP1; IIN2, IIP2; and IIN3, IIP3.
In this configuration, with the mains voltage of $3 \times 230 \mathrm{~V}$ and rated currents of 80A, the output frequency of the IL19006 energy metering integrated circuit at FOUT1 is 1.16 kHz . In this case 1 pulse will correspond to an energy consumption of $3 \times 18.4$ $\mathrm{kW} / 1160 \mathrm{~Hz}=47.6 \mathrm{Ws}$.
The output frequency at FOUT1 and FOUT2 represents the absolute sum of the energy measured on all three phases, regardless of the direction of energy flow through the current sensors. This measurement method will assist meter manufacturers to circumvent meter tampering by reversal of the phases.

## 2. Analog Input Configuration

The current and voltage sensor inputs are illustrated below.
These inputs are protected against electrostatic discharge through clamping diodes, in conjunction with the amplifiers input configuration.
The feedback loops from the outputs of the amplifiers $A_{l}$ and $A_{V}$ generate virtual shorts on the signal inputs. Exact duplications of the input currents are generated for the analog processing circuitry.


## 3. Electrostatic Discharge (ESD) Protection

The IL19006 integrated circuit's inputs/outputs are protected against ESD.

## 4. Power Consumption

The overall power consumption rating of the IL19006 integrated circuit is less than 75 mW with a 5 V supply.

## 5. Pulse Output Signals

Waveforms displaying the DIR and FOUT1 signal information for each of the three phases are shown below.

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These waveforms demonstrate how to establish the direction of energy flow as well as the phase from which the energy is measured. The direction of energy indicated on pin DIR is HIGH for POSITIVE energy flow and LOW for NEGATIVE energy flow, for the entire LOW period of the FOUT1 pulse. The phase to which the direction indication on the DIR pin refers can be ascertained by counting the number of falling edges on the DIR pin prior to the falling edge of the FOUT1 pulse. The supervision of the DIR pin can be accomplished with a $\mu$ Controller.
Although FOUT1 has a fixed frequency output, the table below shows the various frequencies selectable for rated condition on FOUT2.

| User Selectable Output Frequency |  |  |
| :---: | :---: | :---: |
| PGM1 | PGM0 | FOUT2 <br> (Hz) |
| 0 | 0 | 5.11 |
| 0 | 1 | 3.83 |
| 1 | 0 | 2.55 |
| 1 | 1 | N/A |

The frequencies shown in the above table were chosen to allow a 4-3-2 scaling ratio for Belarus Belar
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rated conditions. This facility provides ease of interface with applications which use the same post divider with mechanical counter or unchanged microcontroller software for different current rated kWh meters.
For example, a meter manufacturer may wish to build meters for 3 system configurations with rated current loading of $80 A_{\text {RMS }}, 60 A_{R M S}$ and $40 A_{R M S}$. The rated line voltage is $230 \mathrm{~V}_{\text {RMs }}$.

## FOUT1 Frequency

Consider the case where FOUT1 is the output of the energy counting block. For each of the three rated conditions, the input current sensing resistors are chosen to ensure that $16 \mu A_{\text {RMS }}$ flows into the current sensing pins.

Case $1 I_{L}=80 A_{R M S}$
1 pulse on FOUT1 $=(80 * 230 * 3) / 1160=47.6 \mathrm{Ws}$
Case $2 I_{L}=60 A_{\text {RMS }}$
1 pulse on FOUT1 $=(60 * 230 * 3) / 1160=35.7 \mathrm{Ws}$
Case $3 I_{L}=40 A_{\text {RMS }}$
1 pulse on FOUT1 $=(40 * 230 * 3) / 1160=23.8 \mathrm{Ws}$
The amount of energy represented by one pulse for each of the three cases is different. In addition to changing the current sensing resistor network, the energy counting block must also be altered.

## FOUT2 Frequency

Now consider the advantage of the user selectable frequency available on FOUT2. Again the input current sensing resistors must be chosen to ensure that $16 \mu \mathrm{~A}$ RMS flows into the current sensing pins.

Case $1 \mathrm{I}_{\mathrm{L}}=80 \mathrm{~A}_{\mathrm{RMS}}, \quad \mathrm{PGM} 1=0 \quad \mathrm{PGM0}=0$
1 pulse on FOUT2 $=(80 * 230 * 3) / 5.11=10.8 \mathrm{kWs}$
Case $2 I_{L}=60 A_{\text {RMS }}, \quad P G M 1=0 \quad P G M 0=1$
1 pulse on FOUT2 $=(60 * 230 * 3) / 3.83=10.8 \mathrm{kWs}$
Case $3 I_{L}=40 A_{\text {RMS }}, \quad P G M 1=1 \quad$ PGM0 $=0$ 1 pulse on FOUT2 $=(40 * 230 * 3) / 2.55=10.8 \mathrm{kWs}$

The only changes which now have to be implemented to interface the device to different rated systems are: change the current sense resistors; and select the required PGM0 and PGM1.
No change to the post divider or micro-controller software is required if the FOUT2 pin is used as described.

## TYPICAL APPLICATION

In the Application Circuit (Figure 1), the components required for a three phase power metering application are shown.
Terminated current sensors (current transformers) are connected to the current sensor inputs of the IL19006 through current setting resistors ( $\mathrm{R}_{8} . . \mathrm{R}_{13}$ ).

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## ILA19006

The resistor values for standard operation are selected for an input current of $16 \mu \mathrm{~A}$ into the IL19006, at the rated line current.
The values of these resistors are calculated as follows:
Phase 1:
$\mathrm{R}_{8}=\mathrm{R}_{9}=\left(\mathrm{I}_{\mathrm{L} 1} / 16 \mu \mathrm{~A}\right) * \mathrm{R}_{18} / 2$
Phase 2:
$\mathrm{R}_{10}=\mathrm{R}_{11}=\left(\mathrm{I}_{\mathrm{L} 2} / 16 \mu \mathrm{~A}\right){ }^{*} \mathrm{R}_{19} / 2$
Phase 3:
$R_{12}=R_{13}=\left(\mathrm{I}_{\mathrm{L} 3} / 16 \mu \mathrm{~A}\right) * \mathrm{R}_{20} / 2$
Where $\mathrm{I}_{\mathrm{LX}} \quad=$ Secondary CT current at rated conditions.
$\mathrm{R}_{18}, \mathrm{R}_{19}$ and $\mathrm{R}_{20}=$ Current transformer termination resistors for the three phases.
$R_{1}+R_{1 A}, R_{4}$ and $R_{15}$ set the current for the phase 1 voltage sense input. $R_{2}+R_{2 A}, R_{5}+P_{5}$ and $R_{16}$ set the current for phase 2 and $R_{3}+R_{3 A}, R_{6}+P_{6}$ and $R_{17}$ set the current for phase 3 . The values should be selected so that the input currents into the voltage sense inputs (virtual ground) are set to $14 \mu \mathrm{~A}$ for rated line voltage. Capacitors C1, C2 and C3 are for decoupling and phase compensation.
$R_{14}+P_{14}$ defines all on-chip bias and reference currents. With $R_{14}+P_{14}=24 \mathrm{~kW}$, optimum conditions are set. $R_{14}+P_{14}$ may be varied within $\pm 10 \%$ for calibration purposes. Any changes to $\mathrm{R} 14+\mathrm{P} 14$ will affect the output quadratically
(i.e: $\Delta R=+5 \%, \Delta f=+10 \%$ ).

The formula for calculating the Output Frequency (f) is given below:
$f=11.16 *$ FOUTX $* \frac{F O S C}{3.5795 M \Gamma u} * \frac{\left(I_{I 1} I_{V 1}\right)+\left(I_{I 2} I_{V 2}\right)+\left(I_{I 3} I_{V 3}\right)}{3 * I_{R}^{2}}$
Where FOUTX = Nominal rated frequency (1160Hz)
FOSC = Oscillator frequency $(2 \mathrm{MHz} \ldots . .4 \mathrm{MHz})$
$I_{11}, I_{12}, I_{I_{3}} \quad=$ Input currents for current inputs (16 $\mu \mathrm{A}$ at rated)
$\mathrm{I}_{\mathrm{V} 1}, \mathrm{I}_{\mathrm{V} 2}, \mathrm{I}_{\mathrm{V} 3} \quad=$ Input currents for voltage inputs ( $14 \mu \mathrm{~A}$ at rated)
$I_{R} \quad=$ Reference current (typically $50 \mu \mathrm{~A}$ )
XTAL is a colour burst TV crystal ( $\mathrm{f}=3.5795 \mathrm{MHz}$ ) for the oscillator. The oscillator frequency is divided down to 1.78975 MHz on-chip, to supply the digital circuitry and the A/D converters.

Figure 1: Application Circuit for Three Phase Power/Energy Measurement.
MAINS VOLTAGES


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## Parts List for Application Circuit: Figure 1

| Item | Symbol | Description | Detail |
| :---: | :---: | :---: | :---: |
| 1 | IC-1 | Integrated IL19006 | DIP-20, SOIC-20 |
| 2 | XTAL | Crystal, 3.5795 MHz | Colour burst TV |
| 3 | R1 | Resistor, 200k, 1\%, 1/4W |  |
| 4 | R1A | Resistor, 180k, 1\%, 1/4W |  |
| 5 | R2 | Resistor, 200k, 1\%, 1/4W |  |
| 6 | R2A | Resistor, 200k, 1\%, 1/4W |  |
| 7 | R3 | Resistor, 200k, 1\%, 1/4W |  |
| 8 | R3A | Resistor, 180k, 1\%, 1/4W |  |
| 9 | R4 | Resistor, 24k, 1\%, 1/4W |  |
| 10 | R5 | Resistor, 22k, 1\%, 1/4W |  |
| 11 | R6 | Resistor, 22k, 1\%, 1/4W |  |
| 12 | R7 | Resistor, 820W, 1\%, 1/4W |  |
| 13 | R8 | Resistor | Note 1 |
| 14 | R9 | Resistor | Note 1 |
| 15 | R10 | Resistor | Note 1 |
| 16 | R11 | Resistor | Note 1 |
| 17 | R12 | Resistor | Note 1 |
| 18 | R13 | Resistor | Note 1 |
| 19 | R14 | Resistor, 22k, 1\%, 1/4W |  |
| 20 | R15 | Resistor, 1M, 1\%, 1/4W |  |
| 21 | R16 | Resistor, 1M, 1\%, 1/4W |  |
| 22 | R17 | Resistor, 1M, 1\%, 1/4W |  |
| 23 | R18 | Resistor | Note 1 |
| 24 | R19 | Resistor | Note 1 |
| 25 | R20 | Resistor | Note 1 |
| 26 | R21 | Resistor, 820W, 1\%, 1/4W |  |
| 27 | P5 | Potentiometer, 4.7k | Multi turn |
| 28 | P6 | Potentiometer, 4.7k | Multi turn |
| 29 | P14 | Potentiometer, 4.7k | Multi turn |
| 30 | C1 | Capacitor, electrolytic, $1 \mu \mathrm{~F}, 6 \mathrm{~V}$ | Note 2 |
| 31 | C2 | Capacitor, electrolytic, $1 \mu \mathrm{~F}, 6 \mathrm{~V}$ | Note 2 |
| 32 | C3 | Capacitor, electrolytic, $1 \mu \mathrm{~F}, 6 \mathrm{~V}$ | Note 2 |
| 33 | C12 | Capacitor, 820nF | Note 3 |
| 34 | C13 | Capacitor, 100nF |  |
| 35 | C14 | Capacitor, 100nF |  |

Note 1: Resistor ( $\mathrm{R}_{8}, \mathrm{R}_{9}, \mathrm{R}_{10}, \mathrm{R}_{11}, \mathrm{R}_{12}$ and $\mathrm{R}_{13}$ ) values are dependant upon the selected values of the current transformer termination resistors $\mathrm{R}_{18}, \mathrm{R}_{19}$ and $\mathrm{R}_{20}$.
Note 2: Capacitor values may be selected to compensate for phase errors caused by the current transformers.
Note 3: Capacitor (C12) to be positioned as close to Supply Pins ( $\mathrm{V}_{\mathrm{DD}}$ \& $\mathrm{V}_{\mathrm{Ss}}$ ) of IC-1, as possible.

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