

## Laser Driver Oscillator



The EL6206 is a push-pull oscillator used to reduce laser noise. It uses the standard interface to existing ROM

controllers. The frequency and amplitude are each set with a separate resistor connected to ground. The tiny package and harmonic reduction allow the part to be placed close to a laser with low RF emissions. An auto turn-off feature allows it to easily be used on combo CD-RW plus DVD-ROM pick-ups.

One external resistor sets the oscillator frequency. Another external resistor sets the oscillator amplitude. If the APC current is reduced such that the average laser voltage drops to less than 1.1V, the output and oscillator are disabled, reducing power consumption to a minimum.

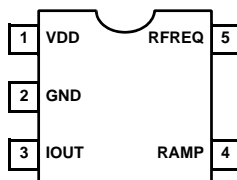
The current drawn by the oscillator consists of a small bias current, plus the peak output amplitude in the positive cycle. In the negative cycle the oscillator subtracts peak output amplitude from the laser APC current.

This part is pin-compatible to the EL6201. It is superior to the EL6201 in several ways: It has up to 100mA output capability, it is faster (up to 600MHz), it is more power-efficient, it has less harmonic content, and it has an auto shut-off feature activated at 1.1V.

The part is available in the space-saving 5-pin SOT23 package. It is specified for operation from 0°C to +85°C.

## Pinout

**EL6206**  
**(5-PIN SOT23)**  
TOP VIEW



## Features

- Low power dissipation
- User-selectable frequency from 100MHz to 600MHz controlled with a single resistor
- User-specified amplitude from 10mA<sub>PK-PK</sub> to 100mA<sub>PK</sub> controlled with a single resistor
- Auto turn-off threshold
- Soft edges for reduced EMI
- Small 5-pin SOT23 package

## Applications

- DVD players
- DVD-ROM drives
- CD-RW drives
- MO drives
- General purpose laser noise reduction

## Ordering Information

PART NUMBER	PACKAGE	TAPE & REEL	PKG. DWG. #
EL6206CW-T7	5-Pin SOT23	7" (3K pcs)	MDP0038
EL6206CW-T7A	5-Pin SOT23	7" (250 pcs)	MDP0038

**Absolute Maximum Ratings** ( $T_A = 25^\circ\text{C}$ )

Voltages Applied to:

$V_{DD}$	-0.5V to +6.0V
$I_{OUT}$	-0.5V to +6.0V
$R_{FREQ}, R_{AMP}$	-0.5V to +6.0V

Operating Ambient Temperature Range	..... $0^\circ\text{C}$ to $+85^\circ\text{C}$
Maximum Junction Temperature	..... $+150^\circ\text{C}$
Storage Temperature Range	..... $-65^\circ\text{C}$ to $+150^\circ\text{C}$
Output Current	..... 100mA <sub>PK-PK</sub>
Power Dissipation (max)	..... See Curves

*CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.*

*IMPORTANT NOTE: All parameters having Min/Max specifications are guaranteed. Typical values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore:  $T_J = T_C = T_A$*

**Supply & Reference Voltage Characteristics**  $V_{DD} = +5V, T_A = 25^\circ\text{C}, R_L = 10\Omega, R_{FREQ} = 3.5k\Omega (F_{OSC} = 550\text{MHz}), R_{AMP} = 2540\Omega$   
 $(I_{OUT} = 50\text{mA}_{P-P}$  measured at 100MHz),  $V_{OUT} = 2.2V$

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
PSOR	Power Supply Operating Range		4.5		5.5	V
$I_{SO}$	Supply Current Disabled	$V_{OUT} < V_{CUTOFF}$		550	750	$\mu\text{A}$
$I_{STYP}$	Supply Current Typical Conditions	$R_{FREQ} = 3.5k\Omega, R_{AMP} = 2.54k\Omega$		22	TBD	mA
$I_{SLO}$	Supply Current Low Conditions	$R_{FREQ} = 18.2k\Omega, R_{AMP} = 12.7k\Omega$		6		mA
$V_{FREQ}$	Voltage at $R_{FREQ}$ Pin			1.27		V
$V_{RAMP}$	Voltage on RAMP Pin			1.27		V
$V_{CUTOFF}$	Monitoring Voltage of $I_{OUT}$ Pin		1.1		1.4	V

**Oscillator Characteristics**  $V_{DD} = +5V, T_A = 25^\circ\text{C}, R_L = 10\Omega, R_{FREQ} = 3.5k\Omega (F_{OSC} = 550\text{MHz}), R_{AMP} = 2540\Omega (I_{OUT} = 50\text{mA}_{P-P}$   
measured at 100MHz),  $V_{OUT} = 2.2V$

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
$F_{OSC}$	Frequency Tolerance	Unit-unit frequency variation	TBD	550	TBD	MHz
$F_{LOW}$	Frequency Range Low	$R_{FREQ} = 18.2k\Omega$		100		MHz
$T_{COSC}$	Frequency Temperature Sensitivity	$-40^\circ\text{C}$ to $+85^\circ\text{C}$ ambient		50		ppm/ $^\circ\text{C}$
$PSRR_{OSC}$	Frequency Change $\Delta F/F$	$V_{DD}$ from 4.5V to 5.5V		1		%

**Driver Characteristics**  $V_{DD} = +5V, T_A = 25^\circ\text{C}, R_L = 10\Omega, R_{FREQ} = 18.2k\Omega (F_{OSC} = 100\text{MHz}), R_{AMP} = 2540\Omega (I_{OUT} = 50\text{mA}_{P-P}$   
measured at 100MHz),  $V_{OUT} = 2.2V$

PARAMETER	DESCRIPTION	CONDITIONS	MIN	TYP	MAX	UNIT
$AMP_{HIGH}$	Amplitude Range High	$R_{AMP} = 1.27k\Omega$		100		mA <sub>P-P</sub>
$AMP_{LOW}$	Amplitude Range Low	$R_{AMP} = 12.7k\Omega$		10		mA <sub>P-P</sub>
$I_{OSNOM}$	Offset Current @ 2.2V	$R_{FREQ} = 3.5k\Omega, V_{OUT} = 2.2V$		TBD		mA
$I_{OSHIGH}$	Offset Current @ 2.8V	$R_{FREQ} = 3.5k\Omega, V_{OUT} = 2.8V$		TBD		mA
$I_{OSLOW}$	Offset Current @ 1.8V	$R_{FREQ} = 3.5k\Omega, V_{OUT} = 1.8V$		TBD		mA
$I_{OUTP-P}$	Output Current Tolerance	Defined as one standard deviation		2		%
Duty Cycle	Output Push Time/Cycle Time	$R_{FREQ} = 3.5k\Omega$		43		%
$PSRR_{AMP}$	Amplitude Change of Output $\Delta I/I$	$V_{DD}$ from 4.5V to 5.5V		-54		dB
$T_{ON}$	Auto Turn-on Time	Output voltage step from 0V to 2.2V		15		$\mu\text{s}$
$T_{OFF}$	Auto Turn-off Time	Output voltage step from 2.2V to 0V		0.5		$\mu\text{s}$
$I_{OUTN}$	Output Current Noise Density	$R_{FREQ} = 5210\Omega$ , measured @ 10MHz		2.5		nA/ $\sqrt{\text{Hz}}$

**Pin Descriptions**

PIN NAME	PIN TYPE	PIN DESCRIPTION
1	VDD	Positive power for laser driver (4.5V - 5.5V)
2	GND	Chip ground pin (0V)
3	IOUT	Current output to laser diode
4	RAMP	Set pin for output current amplitude
5	RFREQ	Set pin for oscillator frequency

**Recommended Operating Conditions**

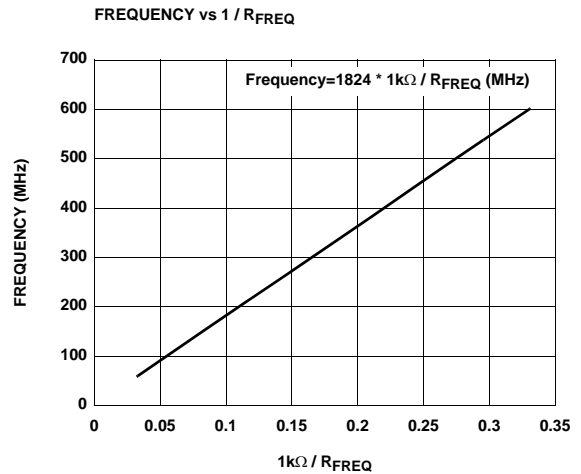
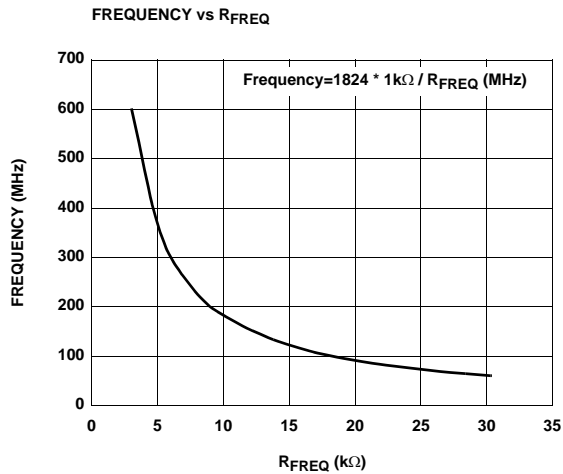
V <sub>DD</sub> .....	5V ±10%	R <sub>AMP</sub> .....	1.25kΩ (min)
V <sub>OUT</sub> .....	.2V - 3V	F <sub>OSC</sub> .....	.100-600MHz
R <sub>RFREQ</sub> .....	3kΩ (min)	I <sub>OUT</sub> .....	10-100mA <sub>PK-PK</sub>

**I<sub>OUT</sub> Control**

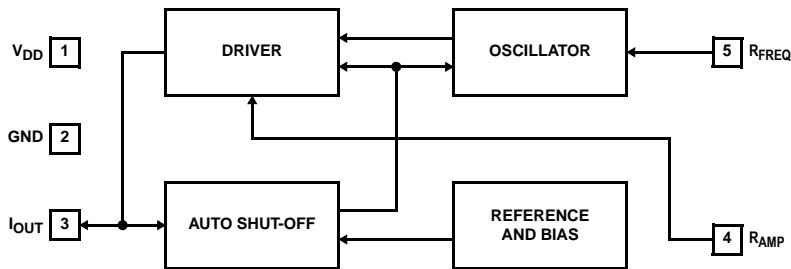
V <sub>OUT</sub>	I <sub>OUT</sub>
Less than V <sub>CUTOFF</sub>	OFF
More than V <sub>CUTOFF</sub>	Normal Operation

**Typical Performance Curves**

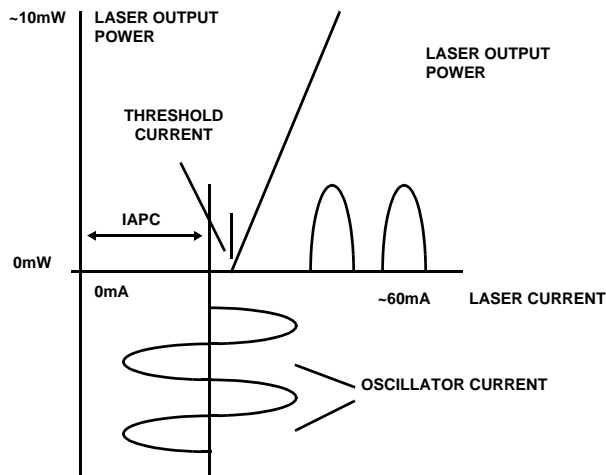
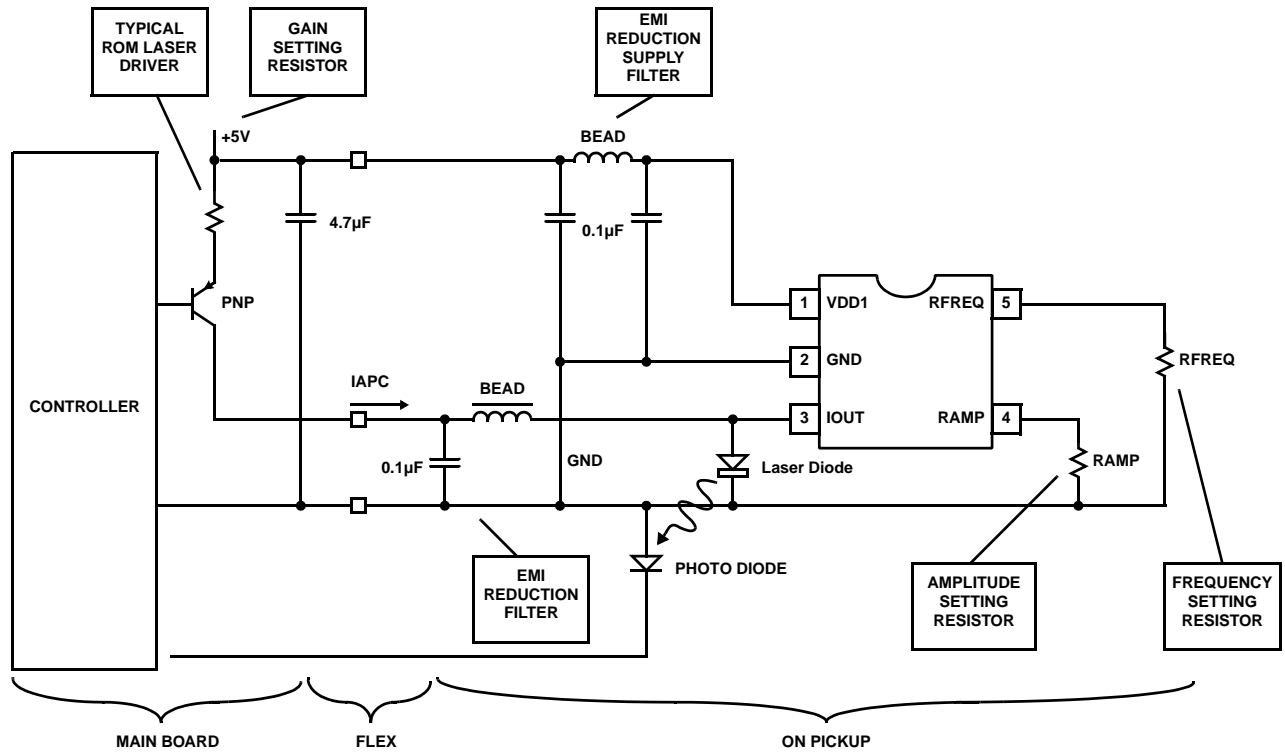
V<sub>DD</sub> = 5V, T<sub>A</sub> = 25°C, R<sub>L</sub> = 10Ω, R<sub>RFREQ</sub> = 3.5kΩ, R<sub>AMP</sub> = 2.54kΩ, V<sub>OUT</sub> = 2.2V unless otherwise specified.



**Block Diagram**



Typical Application Circuit



## Applications Information

### Product Description

The EL6206 is a solid state, low-power, high-speed laser modulation oscillator with external resistor-adjustable operating frequency and output amplitude. It is designed to interface easily to laser diodes to break up optical feedback resonant modes and thereby reduce laser noise. The output of the EL6206 is composed of a push-pull current source, switched alternately at the oscillator frequency. The output and oscillator are automatically disabled for power saving when the average laser voltage drops to less than 1.1V. The EL6206 has the operating frequency from 100MHz to 600MHz and the output current from 10mA<sub>P-P</sub> to 100mA<sub>P-P</sub>. The supply current is only 22mA for the output current of 50mA<sub>P-P</sub> at the operating frequency of 550MHz.

### Theory of Operation

A typical semiconductor laser will emit a small amount of incoherent light at low values of forward laser current. But after the threshold current is reached, the laser will emit coherent light. Further increases in the forward current will cause rapid increases in laser output power. A typical threshold current is 35mA and a typical slope efficiency is 0.7mW/mA.

When the laser is lasing, it will often change its mode of operation slightly, due to changes in current, temperature, or optical feedback into the laser. In a DVD-ROM, the optical feedback from the moving disk forms a significant noise factor due to feedback-induced mode hopping. In addition to the mode hopping noise, a diode laser will roughly have a constant noise level regardless of the power level when a threshold current is exceeded.

The oscillator is designed to produce a low noise oscillating current that is added to the external DC current. The effective AC current is to cause the laser power to change at the oscillator frequency. This change causes the laser to go through rapid mode hopping. The low frequency component of laser power noise due to mode hopping is translated up to sidebands around the oscillator frequency by this action. Since the oscillator frequency can be filtered out of the low frequency read and serve channels, the net result is that the laser noise seems to be reduced. The second source of laser noise reduction is caused by the increase in the laser power above the average laser power during the pushing-current time. The signal-to-noise ratio (SNR) of the output power is better at higher laser powers because of the almost constant noise power when a threshold current is exceeded. In addition, when the laser is off during the pulling-current time, the noise is also very low.

### R<sub>AMP</sub> and R<sub>FREQ</sub> Value Setting

The laser should always have a forward current during operation. This will prevent the laser voltage from collapsing,

and ensure that the high frequency components reach the junction without having to charge the junction capacitance.

Generally it is desirable to make the oscillator currents as large as possible to obtain the greatest reduction in laser noise. But it is not a trivial matter to determine this critical value. The amplitude depends on the wave shape of the oscillator current reaching the laser junction.

If the output current is sinusoidal, and the components in the output circuit are fixed and linear, then the shape of the current will be sinusoidal. But the amount of current reaching the laser junction is a function of the circuit parasitics. These parasitics can result in a resonant increase in output depending on the frequency due to the junction capacitance and layout. Also, the amount of junction current causing laser emission is variable with frequency due to the junction capacitance. In conclusion, the sizes of the R<sub>AMP</sub> and R<sub>FREQ</sub> resistors must be determined experimentally. A good starting point is to take a value of R<sub>AMP</sub> for a peak-to-peak current amplitude less than the minimum laser threshold current and a value of R<sub>FREQ</sub> for an output current close to a sinusoidal wave form (refer to the proceeding performance curves).

### R<sub>AMP</sub> and R<sub>FREQ</sub> Pin Interfacing

Figure 1 shows an equivalent circuit of pins associated with the R<sub>AMP</sub> and R<sub>FREQ</sub> resistors. V<sub>REF</sub> is roughly 1.27V for both R<sub>AMP</sub> and R<sub>FREQ</sub>. The R<sub>AMP</sub> and R<sub>FREQ</sub> resistors should be connected to the non-load side of the power ground to avoid noise pick-up. These resistors should also return to the EL6206's ground very directly to prevent noise pickup. They also should have minimal capacitance to ground. Trimmer resistors can be used to adjust initial operating points.

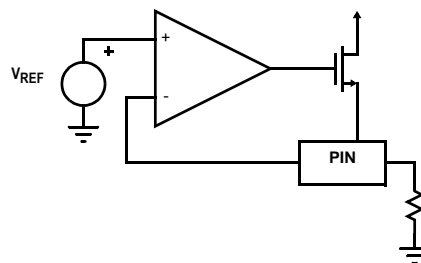


FIGURE 1. R<sub>AMP</sub> AND R<sub>FREQ</sub> PIN INTERFACE

External voltage sources can be coupled to the R<sub>AMP</sub> and R<sub>FREQ</sub> pins to effect frequency or amplitude modulation or adjustment. It is recommended that a coupling resistor of 1k be installed in series with the control voltage and mounted directly next to the pin. This will keep the inevitable high-frequency noise of the EL6206's local environment from propagating to the modulation source, and it will keep parasitic capacitance at the pin minimized.

### Supply Bypassing and Grounding

The resistance of bypass-capacitors and the inductance of bonding wires prevent perfect bypass action, and 150mV<sub>p-p</sub> noise on the power lines is common. There needs to be a lossy bead inductance and secondary bypass on the supply side to control signals from propagating down the wires. Figure 2 shows the typical connection.

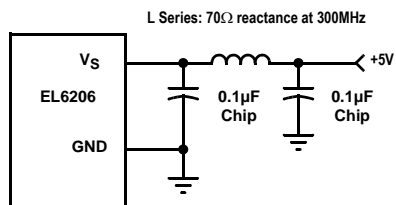


FIGURE 2. RECOMMENDED SUPPLY BYPASSING

Also important is circuit-board layout. At the EL6206's operating frequencies, even the ground plane is not low-impedance. High frequency current will create voltage drops in the ground plane. Figure 3 shows the output current loops.

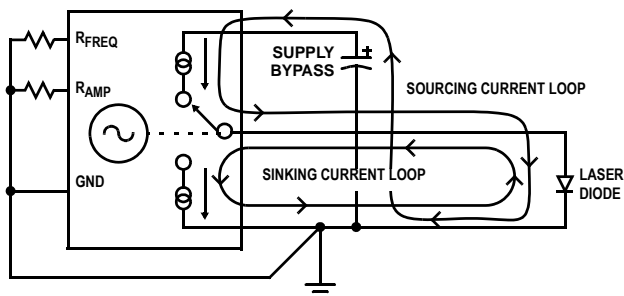


FIGURE 3. OUTPUT CURRENT LOOPS

For the pushing current loop, the current flows through the bypass capacitor, into the EL6206 supply pin, out the I<sub>OUT</sub> pin to the laser, and from the laser back to the decoupling capacitor. This loop should be small.

For the pulling current loop, the current flows into the I<sub>OUT</sub> pin, out of the ground pin, to the laser cathode, and from the laser diode back to the I<sub>OUT</sub> pin. This loop should also be small.

### Power Dissipation

With the high output drive capability, the EL6206 is possible to exceed the 125°C “absolute-maximum junction temperature” under certain conditions. Therefore, it is important to calculate the maximum junction temperature for the application to determine if the conditions need to be modified for the oscillator to remain in the safe operating area.

The maximum power dissipation allowed in a package is determined according to:

$$P_{D\text{MAX}} = \frac{T_{J\text{MAX}} - T_{A\text{MAX}}}{\theta_{JA}}$$

where

P<sub>DMAX</sub> = Maximum Power Dissipation in the Package

T<sub>JMAX</sub> = Maximum Junction Temperature

T<sub>AMAX</sub> = Maximum Ambient Temperature

θ<sub>JA</sub> = Thermal Resistance of the Package

The supply current of the EL6206 depends on the peak-to-peak output current and the operating frequency which are determined by resistors R<sub>AMP</sub> and R<sub>FREQ</sub>. The supply current can be predicted approximately by the following equation:

$$I_{\text{SUP}} = \frac{31.25\text{mA} \times 1\text{k}\Omega}{R_{\text{AMP}}} + \frac{30\text{mA} \times 1\text{k}\Omega}{R_{\text{FREQ}}} + 0.6\text{mA}$$

The power dissipation can be calculated from the following equation:

$$P_D = V_{\text{SUP}} \times I_{\text{SUP}}$$

Here, V<sub>SUP</sub> is the supply voltage. Figures 4 and 5 provide a convenient way to see if the device will overheat. The maximum safe power dissipation can be found graphically, based on the package type and the ambient temperature. By using the previous equation, it is a simple matter to see if P<sub>D</sub> exceeds the device's power derating curve. To ensure proper operation, it is important to observe the recommended derating curve shown in Figures 4 and 5. A flex circuit may have a higher θ<sub>JA</sub>, and lower power dissipation would then be required.

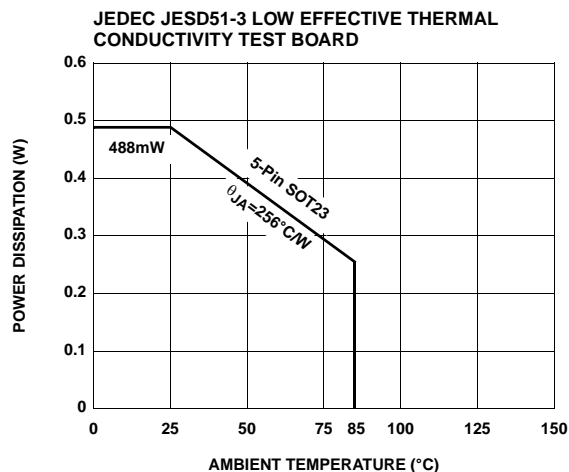


FIGURE 4. PACKAGE POWER DISSIPATION VS AMBIENT TEMPERATURE

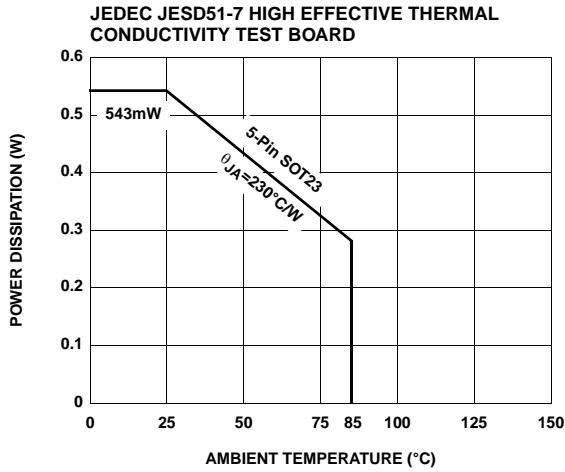


FIGURE 5. PACKAGE POWER DISSIPATION VS AMBIENT TEMPERATURE

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