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### Triple Low-Power 60MHz Unity-Gain Stable Op Amp



The EL2344 is a triple version of the popular EL2044. It is a high speed, low power, low cost monolithic operational

amplifier built on Elantec's proprietary complementary bipolar process. The EL2344 is unity-gain stable and feature a 325V/μs slew rate and 60MHz gain-bandwidth product while requiring only 5.2mA of supply current per amplifier.

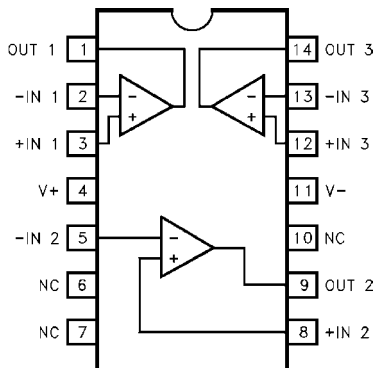
The power supply operating range of the EL2344 is from ±18V down to as little as ±2V. For single-supply operation, the EL2344 operates from 36V down to as little as 2.5V. The excellent power supply operating range of the EL2344 makes it an obvious choice for applications on a single +5V or +3V supply.

The EL2344 also features an extremely wide output voltage swing of ±13.6V with  $V_S = \pm 15V$  and  $R_L = 1000\Omega$ . At ±5V, output voltage swing is a wide ±3.8V with  $R_L = 500\Omega$  and ±3.2V with  $R_L = 150\Omega$ . Furthermore, for single-supply operation at +5V, output voltage swing is an excellent 0.3V to 3.8V with  $R_L = 500\Omega$ .

At a gain of +1, the EL2344 has a -3dB bandwidth of 120MHz with a phase margin of 50°. It can drive unlimited load capacitance, and because of its conventional voltage-feedback topology, the EL2344 allows the use of reactive or non-linear elements in their feedback network. This versatility combined with low cost and 75mA of output-current drive makes the EL2344 an ideal choice for price-sensitive applications requiring low power and high speed.

### Pinout

EL2344  
14-PIN PDIP, SO  
TOP VIEW



### Features

- 60MHz gain-bandwidth product
- Unity-gain stable
- Low supply current (per Amplifier)
  - 5.2mA at  $V_S = \pm 15V$
- Wide supply range
  - ±2V to ±18V dual-supply
  - 2.5V to 36V single-supply
- High slew rate = 325V/μs
- Fast settling = 80ns to 0.1% for a 10V step
- Low differential gain = 0.04% at  $A_V = +2$ ,  $R_L = 150\Omega$
- Low differential phase = 0.15° at  $A_V = +2$ ,  $R_L = 150\Omega$
- Stable with unlimited capacitive load
- Wide output voltage swing
  - 13.6V with  $V_S = \pm 15V$ ,  $R_L = 1000\Omega$
  - 3.8V/0.3V with  $V_S = +5V$ ,  $R_L = 500\Omega$
- Low cost, enhanced replacement for the AD827 and LT1229/LT1230

### Applications

- Video amplifier
- Single-supply amplifier
- Active filters/integrators
- High-speed sample-and-hold
- High-speed signal processing
- ADC/DAC buffer
- Pulse/RF amplifier
- Pin diode receiver
- Log amplifier
- Photo multiplier amplifier
- Difference amplifier

### Ordering Information

PART NUMBER	TEMP. RANGE	PACKAGE	PKG. NO.
EL2344CN	-40°C to +85°C	14-Pin PDIP	MDP0031
EL2344CS	-40°C to +85°C	14-Pin SO	MDP0027

**Absolute Maximum Ratings** ( $T_A = 25\text{ }^\circ\text{C}$ )

Supply Voltage ( $V_S$ ) .....  $\pm 18\text{V}$  or  $36\text{V}$   
 Peak Output Current ( $I_{OP}$ ) ..... Short-Circuit Protected  
 Output Short-Circuit Duration (Note 1) ..... Infinite  
 Input Voltage ( $V_{IN}$ ) .....  $\pm V_S$   
 Differential Input Voltage ( $V_{IN}$ ) .....  $\pm 10\text{V}$

Power Dissipation ( $P_D$ ) ..... See Curves  
 Operating Temperature Range ( $T_A$ ) .....  $-40^\circ\text{C}$  to  $+85^\circ\text{C}$   
 Operating Junction Temperature ( $T_J$ ) .....  $150^\circ\text{C}$   
 Storage Temperature ( $T_{ST}$ ) .....  $-65^\circ\text{C}$  to  $+150^\circ\text{C}$

*CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.*

*IMPORTANT NOTE: All parameters having Min/Max specifications are guaranteed. Typical values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore:  $T_J = T_C = T_A$*

**DC Electrical Specifications**  $V_S = \pm 15\text{V}$ ,  $R_L = 1000\Omega$ , unless otherwise specified.

PARAMETER	DESCRIPTION	CONDITION	TEMP	MIN	TYP	MAX	UNITS
V <sub>OS</sub>	Input Offset Voltage	V <sub>S</sub> = $\pm 15\text{V}$	25°C		0.5	12.0	mV
			T <sub>MIN</sub> , T <sub>MAX</sub>			17.0	mV
TCV <sub>OS</sub>	Average Offset Voltage Drift	(Note 1)	All		10.0		$\mu\text{V}/^\circ\text{C}$
I <sub>B</sub>	Input Bias Current	V <sub>S</sub> = $\pm 15\text{V}$	25°C		2.8	8.2	$\mu\text{A}$
			T <sub>MIN</sub> , T <sub>MAX</sub>			11.2	$\mu\text{A}$
I <sub>OS</sub>	Input Offset Current	V <sub>S</sub> = $\pm 15\text{V}$	25°C		50	300	nA
			T <sub>MIN</sub> , T <sub>MAX</sub>			500	nA
I <sub>OS</sub>	Input Offset Current	V <sub>S</sub> = $\pm 5\text{V}$	25°C		2.8		$\mu\text{A}$
			T <sub>MIN</sub> , T <sub>MAX</sub>				
TCI <sub>OS</sub>	Average Offset Current Drift		All		0.3		nA/°C
A <sub>VOL</sub>	Open-Loop Gain	V <sub>S</sub> = $\pm 15\text{V}$ , V <sub>OUT</sub> = $\pm 10\text{V}$ , R <sub>L</sub> = $1000\Omega$	25°C	800	1500		V/V
			T <sub>MIN</sub> , T <sub>MAX</sub>	600			V/V
			25°C		1200		V/V
PSRR	Power Supply Rejection Ratio	V <sub>S</sub> = $\pm 5\text{V}$ to $\pm 15\text{V}$	25°C	65	80		dB
			T <sub>MIN</sub> , T <sub>MAX</sub>	60			dB
CMRR	Common-Mode Rejection Ratio	V <sub>CM</sub> = $\pm 12\text{V}$ , V <sub>OUT</sub> = $0\text{V}$	25°C	70	90		dB
			T <sub>MIN</sub> , T <sub>MAX</sub>	70			dB
CMIR	Common-Mode Input Range	V <sub>S</sub> = $\pm 15\text{V}$	25°C		$\pm 14.0$		V
		V <sub>S</sub> = $\pm 5\text{V}$	25°C		$\pm 4.2$		V
		V <sub>S</sub> = $+5\text{V}$	25°C		4.2/0.1		V
V <sub>OUT</sub>	Output Voltage Swing	V <sub>S</sub> = $\pm 15\text{V}$ , R <sub>L</sub> = $1000\Omega$	25°C	$\pm 13.4$	$\pm 13.6$		V
			T <sub>MIN</sub> , T <sub>MAX</sub>	$\pm 13.1$			V
		V <sub>S</sub> = $\pm 15\text{V}$ , R <sub>L</sub> = $500\Omega$	25°C	$\pm 12.0$	$\pm 13.4$		V
		V <sub>S</sub> = $\pm 5\text{V}$ , R <sub>L</sub> = $500\Omega$	25°C	$\pm 3.4$	$\pm 3.8$		V
		V <sub>S</sub> = $\pm 5\text{V}$ , R <sub>L</sub> = $150\Omega$	25°C		$\pm 3.2$		V
		V <sub>S</sub> = $+5\text{V}$ , R <sub>L</sub> = $500\Omega$	25°C	3.6/0.4	3.8/0.3		V
I <sub>SC</sub>	Output Short Circuit Current		25°C	40	75		mA
			T <sub>MIN</sub> , T <sub>MAX</sub>	35			mA

**DC Electrical Specifications**  $V_S = \pm 15V$ ,  $R_L = 1000\Omega$ , unless otherwise specified. **(Continued)**

PARAMETER	DESCRIPTION	CONDITION	TEMP	MIN	TYP	MAX	UNITS
I <sub>S</sub>	Supply Current (Per Amplifier)	V <sub>S</sub> = ±15V, No Load	25°C		5.2	7	mA
			T <sub>MIN</sub> , T <sub>MAX</sub>			7.6	mA
		V <sub>S</sub> = ±5V, No Load	25°C		5.0		mA
R <sub>IN</sub>	Input Resistance	Differential	25°C		150		kΩ
		Common-Mode	25°C		15		MΩ
C <sub>IN</sub>	Input Capacitance	A <sub>V</sub> = +1 @ 10MHz	25°C		1.0		pF
R <sub>OUT</sub>	Output Resistance	A <sub>V</sub> = +1	25°C		50		mΩ
PSOR	Power-Supply Operating Range	Dual-Supply	25°C	±2.0		±18.0	V
		Single-Supply	25°C	2.5		36.0	V

**NOTE:**

1. Measured from T<sub>MIN</sub> to T<sub>MAX</sub>.

**Closed-Loop AC Electrical Specifications**

$V_S = \pm 15V$ ,  $A_V = +1$ ,  $R_L = 1000\Omega$  unless otherwise specified.

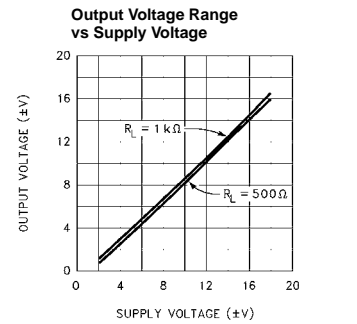
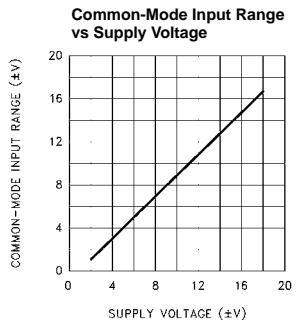
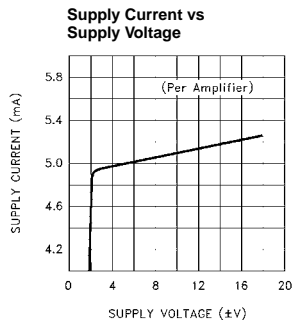
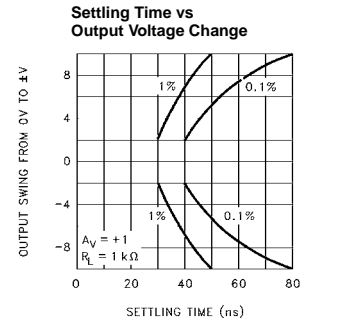
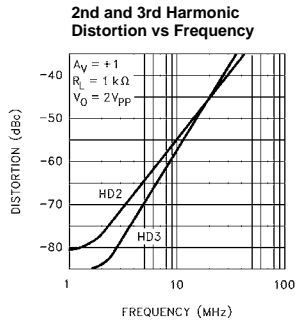
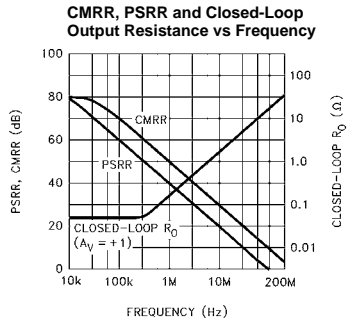
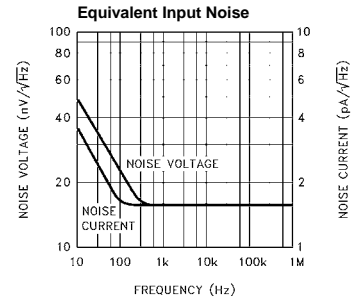
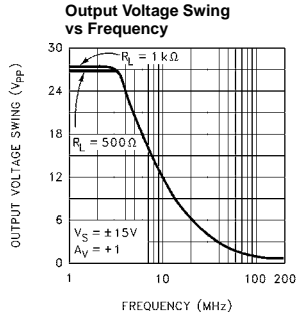
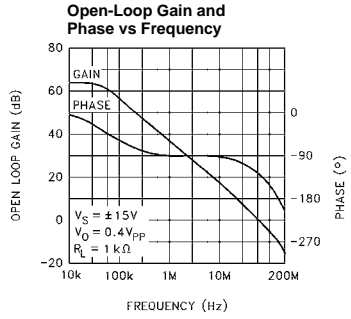
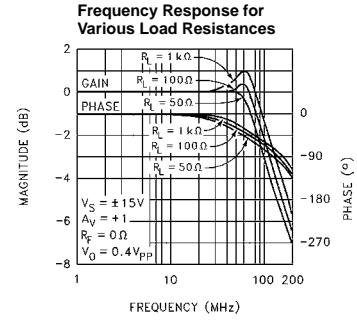
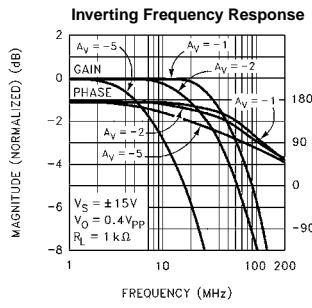
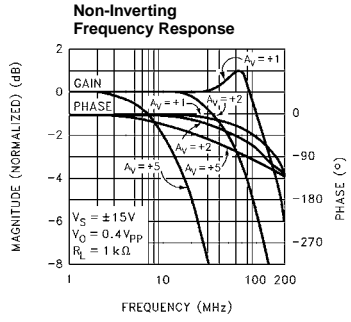
PARAMETER	DESCRIPTION	CONDITION	TEMP	MIN	TYP	MAX	UNITS
BW	-3dB Bandwidth ( $V_{OUT} = 0.4V_{PP}$ )	$V_S = \pm 15V$ , $A_V = +1$	25°C		120		MHz
		$V_S = \pm 15V$ , $A_V = -1$	25°C		60		MHz
		$V_S = \pm 15V$ , $A_V = +2$	25°C		60		MHz
		$V_S = \pm 15V$ , $A_V = +5$	25°C		12		MHz
		$V_S = \pm 15V$ , $A_V = +10$	25°C		6		MHz
		$V_S = \pm 5V$ , $A_V = +1$	25°C		80		MHz
GBWP	Gain-Bandwidth Product	$V_S = \pm 15V$	25°C		60		MHz
		$V_S = \pm 5V$	25°C		45		MHz
PM	Phase Margin	$R_L = 1k\Omega$ , $C_L = 10pF$	25°C		50		°
CS	Channel Separation	$f = 5MHz$	25°C		85		dB
SR	Slew Rate (Note 1)	$V_S = \pm 15V$ , $R_L = 1000\Omega$	25°C	250	325		V/ $\mu s$
		$V_S = \pm 5V$ , $R_L = 500\Omega$	25°C		200		V/ $\mu s$
FPBW	Full-Power Bandwidth (Note 2)	$V_S = \pm 15V$	25°C	4.0	5.2		MHz
		$V_S = \pm 5V$	25°C		12.7		MHz
$t_R$ , $t_F$	Rise Time, Fall Time	0.1V Step	25°C		3.0		ns
OS	Overshoot	0.1V Step	25°C		20		%
$t_{PD}$	Propagation Delay		25°C		2.5		ns
$t_S$	Settling to +0.1% ( $A_V = +1$ )	$V_S = \pm 15V$ , 10V Step	25°C		80		ns
		$V_S = \pm 5V$ , 5V Step	25°C		60		ns
$d_G$	Differential Gain (Note 3)	NTSC/PAL	25°C		0.04		%
$d_P$	Differential Phase (Note 3)	NTSC/PAL	25°C		0.15		°
$e_N$	Input Noise Voltage	10kHz	25°C		15.0		nH/ $\sqrt{Hz}$
$i_N$	Input Noise Current	10kHz	25°C		1.50		pA/ $\sqrt{Hz}$
CI STAB	Load Capacitance Stability	$A_V = +1$	25°C		Infinite		pF

NOTES:

- Slew rate is measured on rising edge.
- For  $V_S = \pm 15V$ ,  $V_{OUT} = 20V_{PP}$ . For  $V_S = \pm 5V$ ,  $V_{OUT} = 5V_{PP}$ . Full-power bandwidth is based on slew rate measurement using:  $FPBW = SR/(2\pi * V_{peak})$ .
- Video Performance measured at  $V_S = \pm 15V$ ,  $A_V = +2$  with 2 times normal video level across  $R_L = 150\Omega$ . This corresponds to standard video levels across a back-terminated  $75\Omega$  load. For other values of  $R_L$ , see curves.

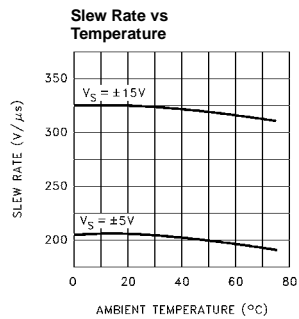
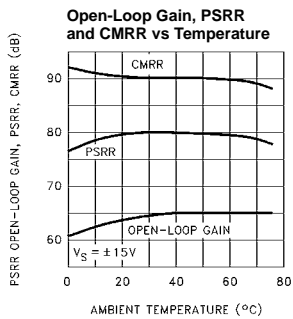
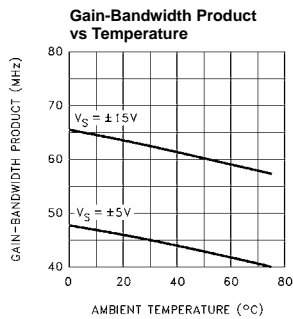
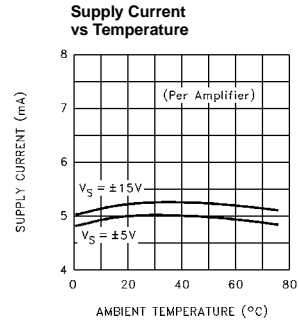
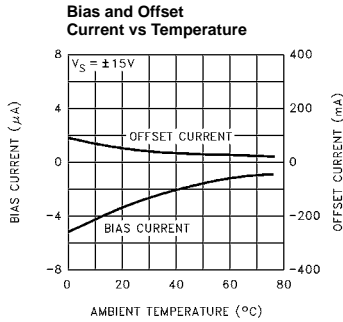
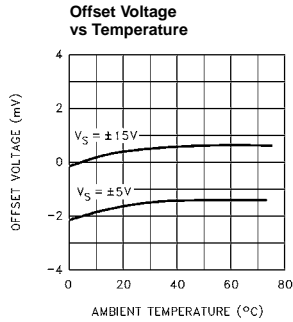
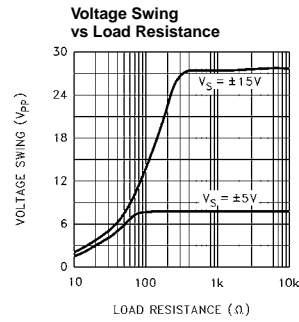
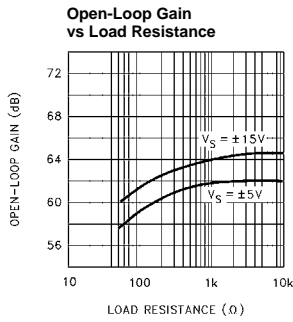
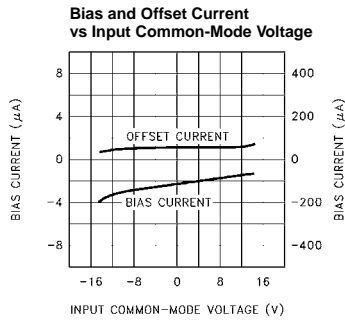
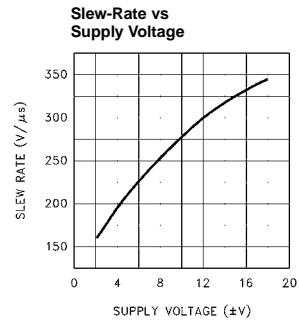
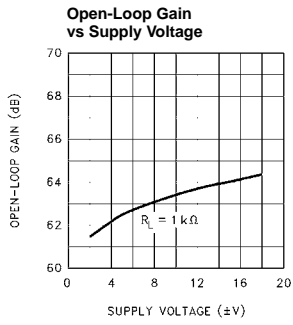
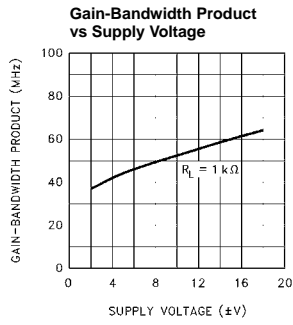
Typical Performance Curves

$T_A = 25^\circ\text{C}$ ,  $R_L = 1000\Omega$ ,  $A_V = +1$  unless otherwise specified.



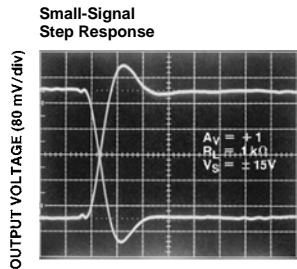
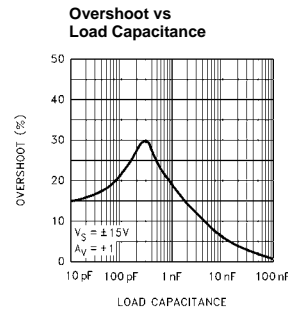
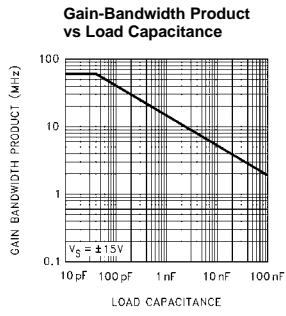
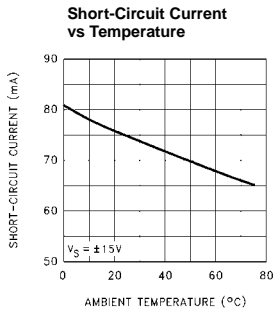
Typical Performance Curves

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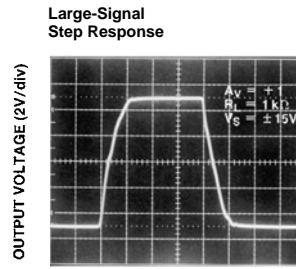


Typical Performance Curves

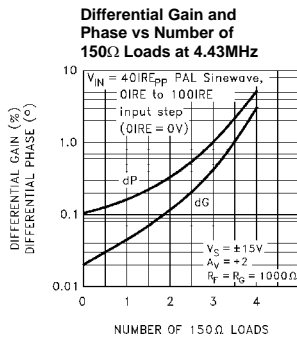
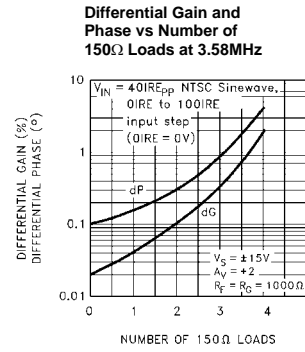
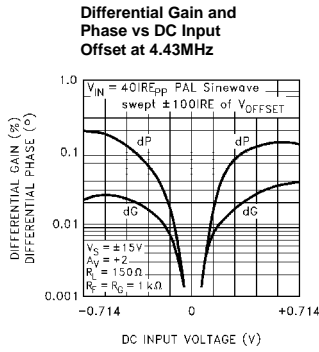
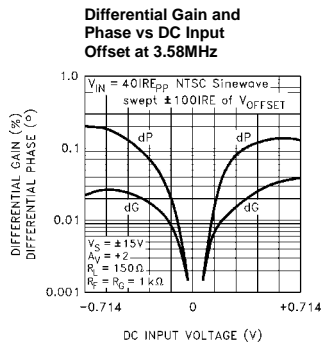
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TIME (5 ns/div)

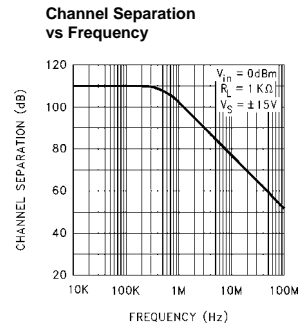
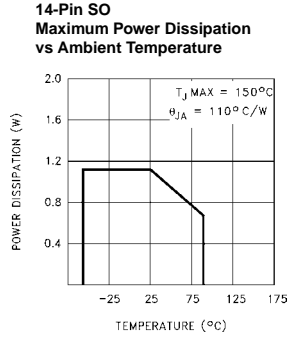
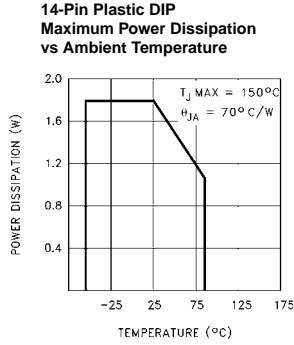


TIME (50 ns/div)

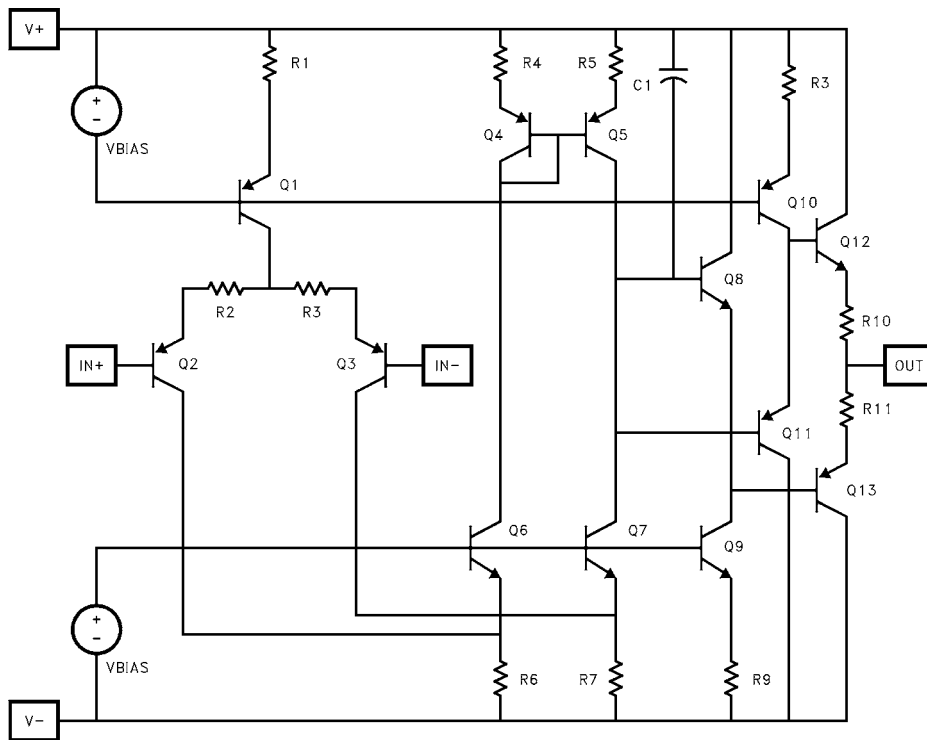


**Typical Performance Curves**

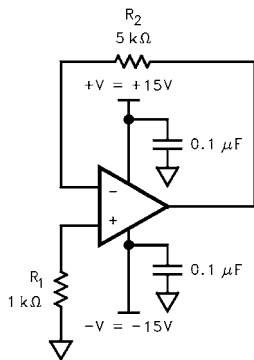
$T_A = 25^\circ\text{C}$ ,  $R_L = 1000\Omega$ ,  $A_V = +1$  unless otherwise specified. (Continued)



**Simplified Schematic** (Per Amplifier)



**Burn-In Circuit** (Per Amplifier)



All Packages Use the Same Schematic

**Applications Information**

**Product Description**

The EL2344 is a low-power wideband monolithic operational amplifier built on Elantec's proprietary high-speed complementary bipolar process. The EL2344 uses a classical voltage-feedback topology which allows them to be used in a variety of applications where current-feedback amplifiers are not appropriate because of restrictions placed upon the feedback element used with the amplifier. The conventional topology of the EL2344 allows, for example, a capacitor to be placed in the feedback path, making it an excellent choice for applications such as active filters, sample-and-holds, or integrators. Similarly, because of the ability to use diodes in the feedback network, the EL2344 is



an excellent choice for applications such as fast log amplifiers.

**Power Dissipation**

With the wide power supply range and large output drive capability of the EL2344, it is possible to exceed the 150°C maximum junction temperatures under certain load and power-supply conditions. It is therefore important to calculate the maximum junction temperature ( $T_{Jmax}$ ) for all applications to determine if power supply voltages, load conditions, or package type need to be modified for the EL2344 to remain in the safe operating area. These parameters are related as follows:

$$T_{JMAX} = T_{MAX} + (\theta_{JA} * (PD_{maxtotal}))$$

where  $PD_{maxtotal}$  is the sum of the maximum power dissipation of each amplifier in the package ( $PD_{max}$ ).  $PD_{max}$  for each amplifier can be calculated as follows:

$$PD_{max} = (2 * V_S * I_{SMAX} + (V_S - V_{OUTMAX}) * (V_{OUTMAX} / R_L))$$

where:

- $T_{MAX}$  = Maximum Ambient Temperature
- $\theta_{JA}$  = Thermal Resistance of the Package
- $PD_{MAX}$  = Maximum Power Dissipation of 1 Amplifier
- $V_S$  = Supply Voltage
- $I_{SMAX}$  = Maximum Supply Current of 1 Amplifier
- $V_{OUTMAX}$  = Maximum Output Voltage Swing of the Application
- $R_L$  = Load Resistance

To serve as a guide for the user, we can calculate maximum allowable supply voltages for the example of the video cable-driver below since we know that  $T_{JMAX} = 150^\circ C$ ,  $T_{MAX} = 75^\circ C$ ,  $I_{SMAX} = 7.6mA$ , and the package  $\theta_{JA}$ s are shown in Table 1. If we assume (for this example) that we are driving a back-terminated video cable, then the maximum average value (over duty-cycle) of  $V_{OUTMAX}$  is 1.4V, and  $R_L = 150\Omega$ , giving the results seen in Table 1.

TABLE 1

	PACKAGE	$\theta_{JA}$	MAX PDISS @ $T_{MAX}$	MAX $V_S$
EL2344CN	PDIP14	70°C/W	1.071W @ 75°C	±11.5V
EL2344CS	SO14	110°C/W	0.682W @ 75°C	±7.5V

**Single-Supply Operation**

The EL2344 has been designed to have a wide input and output voltage range. This design also makes the EL2344 an excellent choice for single-supply operation. Using a single positive supply, the lower input voltage range is within 100mV of ground ( $R_L = 500\Omega$ ), and the lower output voltage range is within 300mV of ground. Upper input voltage range reaches 4.2V, and output voltage range reaches 3.8V with a

5V supply and  $R_L = 500\Omega$ . This results in a 3.5V output swing on a single 5V supply. This wide output voltage range also allows single-supply operation with a supply voltage as high as 36V or as low as 2.5V. On a single 2.5V supply, the EL2344 still has 1V of output swing.

**Gain-Bandwidth Product and the -3dB Bandwidth**

The EL2344 has a gain-bandwidth product of 60MHz while using only 5.2mA of supply current per amplifier. For gains greater than 4, their closed-loop -3dB bandwidth is approximately equal to the gain-bandwidth product divided by the noise gain of the circuit. For gains less than 4, higher-order poles in the amplifiers' transfer function contribute to even higher closed loop bandwidths. For example, the EL2344 has a -3dB bandwidth of 120MHz at a gain of +1, dropping to 60MHz at a gain of +2. It is important to note that the EL2344 has been designed so that this "extra" bandwidth in low-gain applications does not come at the expense of stability. As seen in the typical performance curves, the EL2344 in a gain of +1 only exhibits 1.0dB of peaking with a 1000 $\Omega$  load.

**Video Performance**

An industry-standard method of measuring the video distortion of components such as the EL2344 is to measure the amount of differential gain ( $d_G$ ) and differential phase ( $d_P$ ) that they introduce. To make these measurements, a 0.286V<sub>PP</sub> (40IRE) signal is applied to the device with 0V DC offset (0IRE) at either 3.58MHz for NTSC or 4.43MHz for PAL. A second measurement is then made at 0.714V DC offset (100IRE). Differential gain is a measure of the change in amplitude of the sine wave, and is measured in percent. Differential phase is a measure of the change in phase, and is measured in degrees.

For signal transmission and distribution, a back-terminated cable (75 $\Omega$  in series at the drive end, and 75 $\Omega$  to ground at the receiving end) is preferred since the impedance match at both ends will absorb any reflections. However, when double termination is used, the received signal is halved; therefore a gain of 2 configuration is typically used to compensate for the attenuation.

The EL2344 has been designed as an economical solution for applications requiring low video distortion. It has been thoroughly characterized for video performance in the topology described above, and the results have been included as typical  $d_G$  and  $d_P$  specifications and as typical performance curves. In a gain of +2, driving 150 $\Omega$ , with standard video test levels at the input, the EL2344 exhibits  $d_G$  and  $d_P$  of only 0.04% and 0.15° at NTSC and PAL. Because  $d_G$  and  $d_P$  can vary with different DC offsets, the video performance of the EL2344 has been characterized over the entire DC offset range from -0.714V to +0.714V. For more information, refer to the curves of  $d_G$  and  $d_P$  vs DC Input Offset.

**Output Drive Capability**

The EL2344 has been designed to drive low impedance loads. It can easily drive 6V<sub>PP</sub> into a 150Ω load. This high output drive capability makes the EL2344 an ideal choice for RF, IF and video applications. Furthermore, the current drive of the EL2344 remains a minimum of 35mA at low temperatures. The EL2344 is current-limited at the output, allowing it to withstand shorts to ground. However, power dissipation with the output shorted can be in excess of the power-dissipation capabilities of the package.

**Capacitive Loads**

For ease of use, the EL2344 has been designed to drive any capacitive load. However, the EL2344 remains stable by automatically reducing its gain-bandwidth product as capacitive load increases. Therefore, for maximum bandwidth, capacitive loads should be reduced as much as possible or isolated via a series output resistor (Rs). Similarly, coax lines can be driven, but best AC performance is obtained when they are terminated with their characteristic impedance so that the capacitance of the coaxial cable will not add to the capacitive load seen by the amplifier. Although stable with all capacitive loads, some peaking still occurs as load capacitance increases. Series resistors at the output of the EL2344 can be used to reduce this peaking and further improve stability.

**Printed-Circuit Layout**

The EL2344 is well behaved, and easy to apply in most applications. However, a few simple techniques will help assure rapid, high quality results. As with any high-frequency device, good PCB layout is necessary for optimum performance.

Ground-plane construction is highly recommended, as is good power supply bypassing. A 0.1μF ceramic capacitor is recommended for bypassing both supplies. Pin lengths should be as short as possible, and bypass capacitors should be as close to the device pins as possible. For good AC performance, parasitic capacitances should be kept to a minimum at both inputs and at the output. Resistor values should be kept under 5kΩ because of the RC time constants associated with the parasitic capacitance. Metal-film and carbon resistors are both acceptable, use of wire-wound resistors is not recommended because of their parasitic inductance. Similarly, capacitors should be low-inductance for best performance.

**The EL2344 Macromodel**

This macromodel has been developed to assist the user in simulating the EL2344 with surrounding circuitry. It has been developed for the PSPICE simulator (copywritten by the Microsim Corporation), and may need to be rearranged for other simulators. It approximates DC, AC, and transient response for resistive loads, but does not accurately model capacitive loading. This model is slightly more complicated than the models used for low-frequency op-amps, but it is much more accurate for AC analysis.

The model does not simulate these characteristics accurately:

**TABLE 2.**

noise	non-linearities
settling-time	temperature effects
CMRR	manufacturing variations
PSRR	

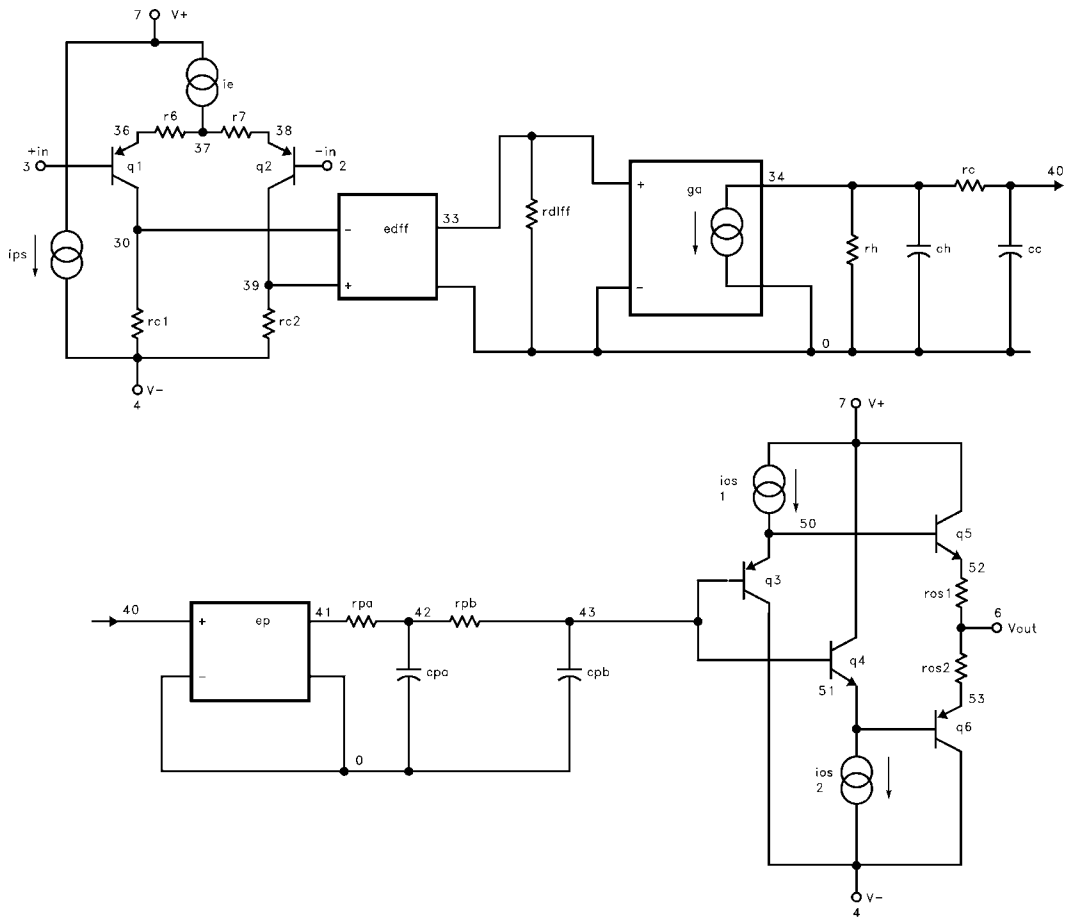
**EL2344 Macromodel** (Continued)

```

* Connections: +input
*               | -input
*               | | +Vsupply
*               | | | -Vsupply
*               | | | | output
*               | | | | |
.subckt M2344 3 2 7 4 6
*
* Input stage
*
ie 7 37 1mA
r6 36 37 800
r7 38 37 800
rc1 4 30 850
rc2 4 39 850
q1 30 3 36 qp
q2 39 2 38 qpa
ediff 33 0 39 30 1.0
rdiff 33 0 1Meg
*
* Compensation Section
*
ga 0 34 33 0 1m
rh 34 0 2Meg
ch 34 0 1.3pF
rc 34 40 1K
cc 40 0 1pF
*
IN+IN+IN+IN+IN+IN+NININININ
* Poles
*
ep 41 0 40 0 1
rpa 41 42 200
cpa 42 0 1pF
rpb 42 43 200
cpb 43 0 1pF
*
* Output Stage
*
ios1 7 50 1.0mA
ios2 51 4 1.0mA
q3 4 43 50 qp
q4 7 43 51 qn
q5 7 50 52 qn
q6 4 51 53 qp
ros1 52 6 25
ros2 6 53 25
*
* Power Supply Current
*
ips 7 4 2.7mA
*
* Models
*
.model qn npn(is=800E-18 bf=200 tf=0.2nS)
.model qpa pnp(is=864E-18 bf=100 tf=0.2nS)
.model qp pnp(is=800E-18 bf=125 tf=0.2nS)
.ends

```

EL2344 Macromodel (Continued)



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