## Design Idea DI-67

 TOPSwitch-GX Isolated, PowerFactor Corrected (PFC), 17 W LED Driver

| Application | Device | Power Output | Input Voltage | Output Current | Topology |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LED Arrays | TOP246F | $17.6 \mathrm{~W} \max$ | $108-132 \mathrm{VAC} 60 \mathrm{~Hz}$ | $700 \mathrm{~mA}(16-24 \mathrm{~V})$ | Flyback |

## Design Highlights

- 700 mA of output current regulated to within $\pm 5 \%$
- Power factor: > 0.98, THD: $\leq 9.6 \%$
- No output current overshoot at power-on
- Temperature range: $-40^{\circ} \mathrm{C}$ to $+80^{\circ} \mathrm{C}$
- Harmonics comply with IEC61000-3-2, Edition 2.1
- Conducted EMI complies with CISPR-22 B


## Operation

This low-cost, TOP246F based PFC LED Driver takes advantage of built-in TOPSwitch-GX features. This supply is current (not voltage) regulated, except in the case of no-load. Without a load, the output voltage is limited to about 30 V (max), by R6 and VR2. Configured as a flyback converter, this circuit operates in the discontinuous conduction mode. It can deliver an average of 700 mA ( 1 A at the peak of output ripple) over a 16 V to 24 V range, which makes it ideal for driving high current LED arrays, such as the Luxeon 12 UP LED Ring.

The DC input capacitor ( $\mathrm{C} 3,100 \mathrm{nF}$ ) was sized so that its voltage approaches zero at the AC input zero crossings (see the middle waveform of Figure 2).

A $220 \mu \mathrm{~F}$ capacitor (C6) was chosen for the bias supply to minimize the 120 Hz ripple current into the current source (Q1), which provides control current to U1. The output rectifier (D9) must be rated for an average of 3.5 A . Capacitor C7's value (680 $\mu \mathrm{F}$ ) sets the magnitude of the output ripple current to 600 mA peak to peak, at 120 Hz .

Resistors R7, R8, R9 and U2's LED set the 700 mA average current limit. The U2 phototransistor drives the current source (Q1) and the PFC-loop filter capacitor (C8, $100 \mu \mathrm{~F}$ ). Capacitor C8 was sized to provide the low loop bandwidth necessary for high power-factor. R4 is the power-off discharge path for C6 and C8.

The CONTROL pin bypass capacitor ( $\mathrm{C} 5,1 \mu \mathrm{~F}$ ) is just large enough to allow smooth start-up of the output load current, and yet small enough to prevent output current overshoot. A larger value of C5 would increase start-up delay time.
700 mA


## Key Design Points

- To have high power factor, a constant duty factor must be maintained over the 8.33 ms half cycle period. Therefore, the bias supply voltage and the U1 CONTROL pin current must remain extremely constant. The values of C6 and C8 must be chosen accordingly.
- Decreasing the value of C 8 will reduce the turn-on delay time, but will also degrade the power factor.
- Because low-cost is the goal of this low-loop-gain design, the tolerance of the output current depends on the CTR of the opto-coupler and the (unregulated) value of the bias voltage. The restricted AC input voltage range allows using the forward (not flyback) configuration for the bias winding. If the AC input voltage range is extended, voltage regulation of the bias supply circuit will be required.


Figure 2. PFC LED Driver Waveforms.
Top: Input Current at 120 VAC 60 Hz .
Middle: C3 Capacitor Voltage.
Bottom: Output Current (with 20 V LED Load).

| TRANSFORMER PARAMETERS |  |
| :---: | :--- |
| Core | EF-20 or Equivalent <br> $A_{\text {LG }}$ of 1570 nH/TT |
| Bobbin | Miles-Platts EF0700 EF20 <br> 8 Pin Horizontal |
| Winding Details | Primary: 70T, 2 layers, 29 AWG <br> Secondary: 13T, 2 x 32 AWG <br> Triple Insulated Wire <br> Bias: 9T, 2 x 23 AWG |
| Winding Order <br> (pin numbers) | Primary: 2-5, tape <br> Secondary: 8-7, tape <br> Primary: 5-1, tape <br> Bias: 3-4, tape 3 layers |
| Primary Inductance | $350 \mu \mathrm{H} \pm 10 \%$ |
| Primary Resonant |  |
| Frequency |  |$\quad 2.0 \mathrm{MHz} \mathrm{(Min)}$| Leakage Inductance |
| :---: |

Table 1. Transformer Construction Information.


Figure 3. PFC Driver Current vs. Temperature.

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| Power Integrations |  | 5245 Hellyer Avenue |  |
| :---: | :---: | :---: | :--- |
| MAIN PHONE NUMBER | APPLICATIONS HOTLINE | APPLICATIONS FAX | San Jose, California 95138 |
| $+1408-414-9200$ | $+1408-414-9660$ | $+1408-414-9760$ | For a complete listing of worldwide sales offices, <br> please visit www.powerint.com |

