RHR1K160D

## 1A, 600V Hyperfast Dual Diode

The RHR1K160D is a hyperfast dual diode with soft recovery characteristics ( $\mathrm{t}_{\mathrm{rr}}<25 \mathrm{~ns}$ ). It has about half the recovery time of ultrafast diodes and is silicon nitride passivated ionimplanted epitaxial planar construction.

This device is intended for use as freewheeling/clamping diodes and rectifiers in a variety of switching power supplies and other power switching applications. Its low stored charge and hyperfast soft recovery minimize ringing and electrical noise in many power switching circuits reducing power loss in the switching transistors.

Formerly developmental type TA49185.

## Ordering Information

| PART NUMBER | PACKAGE | BRAND |
| :--- | :--- | :--- |
| RHR1K160D | MS-012AA | RHR1K160D |

NOTE: When ordering, use the entire part number. For ordering in tape and reel, add the suffix 96 to the part number, i.e., RHR1K160D96.

## Packaging

## BRANDING DASH



## Features

- Hyperfast with Soft Recovery . . . . . . . . . . . . . . . . . . $<25 n s$
- Operating Temperature. . . . . . . . . . . . . . . . . . . . . . . $150^{\circ} \mathrm{C}$
- Reverse Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . . . 600 V
- Thermal Impedance SPICE® Model
- Thermal Impedance SABER© Model
- Avalanche Energy Rated
- Planar Construction
- Related Literature
- TB334, "Guidelines for Soldering Surface Mount Components to PC Boards"


## Applications

- Switching Power Supplies
- Power Switching Circuits
- General Purpose


## Symbol



| Absolute Maximum Ratings (Per Leg) $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Unless Otherwise Specified |  |  |
| :---: | :---: | :---: |
|  | RHR1K160D | UNITS |
| Peak Repetitive Reverse Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\mathrm{V}_{\text {RRM }}$ | 600 | V |
| Working Peak Reverse Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\mathrm{V}_{\text {RWM }}$ | 600 | V |
| DC Blocking Voltage . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\mathrm{V}_{\mathrm{R}}$ | 600 | V |
|  | 1 | A |
|  | 2 | A |
| Nonrepetitive Peak Surge Current . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . I FSM Halfwave, 1 phase, 60 Hz | 10 | A |
| Maximum Power Dissipation (Note 1) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\mathrm{P}_{\mathrm{D}}$ | 2.5 | W |
| Avalanche Energy (See Figures 11 and 12) . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\mathrm{E}_{\text {AVL }}$ | 5 | mJ |
| Operating and Storage Temperature . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . T $_{\text {STG }}, \mathrm{T}_{J}$ | -55 to 150 | ${ }^{\circ} \mathrm{C}$ |
| Maximum Temperature for Soldering |  |  |
| Leads at 0.063in (1.6mm) from Case for 10s . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . . $\mathrm{T}_{\text {L }}$ | 300 | ${ }^{\circ} \mathrm{C}$ |
|  | 260 | ${ }^{\circ} \mathrm{C}$ |

Electrical Specifications (Per Leg) $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, Unless Otherwise Specified

| SYMBOL | TEST CONDITION | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{F}$ | $\mathrm{I}_{\mathrm{F}}=1 \mathrm{~A}$ | - | - | 2.1 | V |
|  | $\mathrm{I}_{\mathrm{F}}=1 \mathrm{~A}, \mathrm{~T}_{\mathrm{A}}=150^{\circ} \mathrm{C}$ | - | - | 1.7 | V |
| $\mathrm{I}_{\mathrm{R}}$ | $\mathrm{V}_{\mathrm{R}}=600 \mathrm{~V}$ | - | - | 100 | $\mu \mathrm{A}$ |
|  | $\mathrm{V}_{\mathrm{R}}=600 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=150^{\circ} \mathrm{C}$ | - | - | 500 | $\mu \mathrm{A}$ |
| $\mathrm{trrr}^{\text {r }}$ | $\mathrm{I}_{\mathrm{F}}=1 \mathrm{~A}, \mathrm{dl}_{\mathrm{F}} / \mathrm{dt}=200 \mathrm{~A} / \mu \mathrm{s}$ | - | - | 25 | ns |
| $\mathrm{t}_{\mathrm{a}}$ | $\mathrm{I}_{\mathrm{F}}=1 \mathrm{~A}, \mathrm{dl}_{\mathrm{F}} / \mathrm{dt}=200 \mathrm{~A} / \mu \mathrm{s}$ | - | 10.5 | - | ns |
| $t_{b}$ | $\mathrm{I}_{\mathrm{F}}=1 \mathrm{~A}, \mathrm{dI}_{\mathrm{F}} / \mathrm{dt}=200 \mathrm{~A} / \mu \mathrm{s}$ | - | 5 | - | ns |
| $\mathrm{Q}_{\mathrm{RR}}$ | $\mathrm{I}_{\mathrm{F}}=1 \mathrm{~A}, \mathrm{dl}_{\mathrm{F}} / \mathrm{dt}=200 \mathrm{~A} / \mu \mathrm{s}$ | - | 20 | - | nC |
| $\mathrm{C}_{J}$ | $\mathrm{V}_{\mathrm{R}}=10 \mathrm{~V}, \mathrm{I}_{\mathrm{F}}=0 \mathrm{~A}$ | - | 10 | - | pf |
| $\mathrm{R}_{\theta \mathrm{JA}}$ | Pad Area $=0.483$ in $^{2}($ Note 1) | - | - | 50 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | Pad Area $=0.027$ in $^{2}$ (Note 2) (Figure 13) | - | - | 201 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | Pad Area $=0.006$ in $^{2}$ (Note 2) (Figure 13) | - | - | 239 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

## DEFINITIONS

$V_{F}=$ Instantaneous forward voltage ( $\mathrm{pw}=300 \mu \mathrm{~s}, \mathrm{D}=2 \%$ ).
$\mathrm{I}_{\mathrm{R}}=$ Instantaneous reverse current.
$t_{r r}=$ Reverse recovery time (See Figure 10), summation of $t_{a}+t_{b}$.
$t_{a}=$ Time to reach peak reverse current (See Figure 10).
$t_{b}=$ Time from peak $I_{R M}$ to projected zero crossing of $I_{R M}$ based on a straight line from peak $I_{R M}$ through $25 \%$ of $I_{R M}$ (See Figure 10).
$\mathrm{Q}_{\mathrm{rr}}=$ Reverse recovery charge.
$\mathrm{C}_{\mathrm{J}}=$ Junction Capacitance.
$R_{\theta J A}=$ Thermal resistance junction to ambient.
$\mathrm{pw}=$ Pulse width.
D = Duty cycle.
NOTES:

1. Measured using FR-4 copper board at 0.8 seconds.
2. 2. Measured using FR-4 copper board at 1000 seconds.

## Typical Performance Curve



FIGURE 1. FORWARD CURRENT vs FORWARD VOLTAGE


FIGURE 2. REVERSE CURRENT vs REVERSE VOLTAGE

## Typical Performance Curve (Continued)



FIGURE 3. $t_{r r}, t_{a}$ AND $t_{b}$ CURVES vs FORWARD CURRENT


FIGURE 5. $t_{r r}, t_{a}$ AND $t_{b}$ CURVES vs FORWARD CURRENT


FIGURE 4. $t_{r r}, t_{a}$ AND $t_{b}$ CURVES vs FORWARD CURRENT


FIGURE 6. CURRENT DERATING CURVE


FIGURE 7. JUNCTION CAPACITANCE vs REVERSE VOLTAGE

## Typical Performance Curve (Continued)



FIGURE 8. NORMALIZED MAXIMUM TRANSIENT THERMAL IMPEDANCE

## Test Circuits and Waveforms



FIGURE 9. $\mathrm{t}_{\mathrm{rr}}$ TEST CIRCUIT

$$
\begin{aligned}
& \mathrm{L}=20 \mathrm{mH} \\
& \mathrm{R}<0.1 \Omega \\
& \mathrm{E}_{\mathrm{AVL}}=1 / 2 \mathrm{LI}^{2}\left[\mathrm{~V}_{\mathrm{R}(\mathrm{AVL})} /\left(\mathrm{V}_{\mathrm{R}(\mathrm{AVL})}-\mathrm{V}_{\mathrm{DD}}\right)\right] \\
& \mathrm{Q}_{1}=\operatorname{IGBT}\left(B V_{C E S}>\operatorname{DUT} \mathrm{V}_{\mathrm{R}(\mathrm{AVL})}\right)
\end{aligned}
$$



FIGURE 11. AVALANCHE ENERGY TEST CIRCUIT


FIGURE 10. $t_{r r}$ WAVEFORMS AND DEFINITIONS


FIGURE 12. AVALANCHE CURRENT AND VOLTAGE WAVEFORMS

## Thermal Resistance vs Mounting Pad Area

The maximum rated junction temperature, $\mathrm{T}_{\mathrm{JM}}$, and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation, $\mathrm{P}_{\mathrm{DM}}$, in an application. Therefore the application's ambient temperature, $\mathrm{T}_{\mathrm{A}}\left({ }^{\circ} \mathrm{C}\right)$, and thermal resistance $\mathrm{R}_{\theta \mathrm{JA}}\left({ }^{\circ} \mathrm{C} / \mathrm{W}\right)$ must be reviewed to ensure that $T_{J M}$ is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$
\begin{equation*}
P_{D M}=\frac{\left(T_{J M}-T_{A}\right)}{Z_{\theta J A}} \tag{EQ.1}
\end{equation*}
$$

In using surface mount devices such as the SOP-8 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of $\mathrm{P}_{\mathrm{DM}}$ is complex and influenced by many factors:

1. Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
2. The number of copper layers and the thickness of the board.
3. The use of external heat sinks.
4. The use of thermal vias.
5. Air flow and board orientation.
6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.
Intersil provides thermal information to assist the designer's preliminary application evaluation. Figure 13 defines the $R_{\theta J A}$ for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 2 oz. copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Intersil device SPICE thermal model or manually utilizing the normalized maximum transient thermal impedance curve.


FIGURE 13. THERMAL RESISTANCE vs MOUNTING PAD AREA

Displayed on the curve are $R_{\theta J A}$ values listed in the Electrical Specifications table. These points were chosen to depict the compromise between the copper board area, the thermal resistance and ultimately the power dissipation, $\mathrm{P}_{\mathrm{DM}}$. Thermal resistances corresponding to other component side copper areas can be obtained from Figure 13 or by calculation using Equation 2. The area, in square inches is the top copper board area, the thermal resistance and ultimately the power dissipation, $\mathrm{P}_{\mathrm{DM}}$.
$R_{\theta J A}=110.18-25.24 \times \ln ($ Area $)$
While Equation 2 describes the thermal resistance of a single die, the dual die SOP-8 package introduces an additional thermal component, thermal coupling resistance, $\mathrm{R}_{\theta \beta}$. Equation 3 describes $\mathrm{R}_{\theta \beta}$ as a function of the top copper mounting pad area.
$R_{\theta \beta}=43.81-22.66 \times \ln ($ Area $)$
The thermal coupling resistance vs. copper area is also graphically depicted in Figure 13. It is important to note the thermal resistance ( $R_{\theta J A}$ ) and thermal coupling resistance $\left(\mathrm{R}_{\theta \beta}\right)$ are equivalent for both die. For example at 0.1 square inches of copper:
$R_{\theta J A 1}=R_{\theta J A 2}=168^{\circ} \mathrm{C} / \mathrm{W}$
$R_{\theta \beta 1}=R_{\theta \beta 2}=96^{\circ} \mathrm{C} / \mathrm{W}$
$T_{J 1}$ and $T_{J 2}$ define the junction temperature of the respective die. Similarly, $P_{1}$ and $P_{2}$ define the power dissipated in each die. The steady state junction temperature can be calculated using Equation 4 for die 1 and Equation 5 for die 2.

Example: Use Equation 4 to calculate $T_{J 1}$ and Equation 5 to calculate $T_{J 2}$ with the following conditions. Die 2 is dissipating 0.5 W ; die 1 is dissipating 0 W ; the ambient temperature is $60^{\circ} \mathrm{C}$; the package is mounted to a top copper area of 0.1 square inches per die.
$T_{J 1}=P_{1} R_{\theta J A}+P_{2} R_{\theta \beta}+T_{A}$
$\mathrm{T}_{\mathrm{J} 1}=(0 \mathrm{~W})\left(168^{\circ} \mathrm{C} / \mathrm{W}\right)+(0.5 \mathrm{~W})\left(96^{\circ} \mathrm{C} / \mathrm{W}\right)+60^{\circ} \mathrm{C}$
$\mathrm{T}_{\mathrm{J} 1}=108^{\circ} \mathrm{C}$
$T_{J 2}=P_{2} R_{\theta J A}+P_{1} R_{\theta \beta}+T_{A}$
$\mathrm{T}_{\mathrm{J} 2}=(0.5 \mathrm{~W})\left(168^{\circ} \mathrm{C} / \mathrm{W}\right)+(0 \mathrm{~W})\left(96^{\circ} \mathrm{C} / \mathrm{W}\right)+60^{\circ} \mathrm{C}$
$\mathrm{T}_{\mathrm{J} 2}=144^{\circ} \mathrm{C}$
The transient thermal impedance $\left(Z_{\theta J A}\right)$ is also effected by varied top copper board area. Figure 14 shows the effect of
copper pad area on single pulse transient thermal impedance. Each trace represents a copper pad area in square inches corresponding to the descending list in the graph. SPICE and SABER thermal models are provided for each of the listed pad areas.

Copper pad area has no perceivable effect on transient thermal impedance for pulse widths less than 100 ms . For pulse widths less than 100 ms the transient thermal impedance is determined by the die and package. Therefore, CTHERM1 through CTHERM6 and RTHERM1 through RTHERM5 remain constant for each of the thermal models. A listing of the model component values is available in Table 1.


FIGURE 14. TRANSIENT THERMAL IMPEDANCE vs MOUNTING PAD AREA

## SPICE Thermal Model

REV October 1998
RHR1K160D
Copper Area $=0.483 \mathrm{in}^{2}$
CTHERM1 th 8 6e-6
CTHERM2 $874 \mathrm{e}-5$
CTHERM3 76 1.5e-4
CTHERM4 $657.5 \mathrm{e}-4$
CTHERM5 54 7e-3
CTHERM6 43 2e-2
CTHERM7 32 8e-2
CTHERM8 2 tl 2.5
RTHERM1 th $85 \mathrm{e}-2$
RTHERM2 87 2.5e-1
RTHERM3 761.5
RTHERM4 652.5
RTHERM5 547.5
RTHERM6 4322
RTHERM7 3238
RTHERM8 2 tl 38

## SABER Thermal Model

Copper Area $=0.483 \mathrm{in}^{2}$
template thermal_model th tl
thermal_c th, tl
\{
ctherm.ctherm1 th $8=6 \mathrm{e}-6$
ctherm.ctherm2 $87=4 \mathrm{e}-5$
ctherm.ctherm3 $76=1.5 \mathrm{e}-4$
ctherm.ctherm4 $65=7.5 \mathrm{e}-4$
ctherm.ctherm5 $54=7 \mathrm{e}-3$
ctherm.ctherm6 $43=2 \mathrm{e}-2$
ctherm.ctherm7 $32=8 \mathrm{e}-2$
ctherm.ctherm8 $2 \mathrm{tl}=2.5$
rtherm.rtherm1 th $8=5 \mathrm{e}-2$
rtherm.rtherm2 $87=2.5 \mathrm{e}-1$
rtherm. $\mathrm{rtherm3} 76=1.5$
rtherm.rtherm4 $65=2.5$
rtherm.rtherm5 $54=7.5$
rtherm.rtherm6 $43=22$
rtherm.rtherm7 $32=38$
rtherm. $\mathrm{rtherm8} 2 \mathrm{tl}=38$
\}
TABLE 1. THERMAL MODELS

| COMPONENT | $\mathbf{0 . 0 2} \mathbf{~ i n}^{\mathbf{2}}$ | $\mathbf{0 . 1 4} \mathbf{i n}^{\mathbf{2}}$ | $\mathbf{0 . 2 5 7} \mathbf{~ i n}^{\mathbf{2}}$ | $\mathbf{0 . 3 8} \mathbf{~ i n}^{\mathbf{2}}$ | $\mathbf{0 . 4 8 3 ~ i n ~}^{\mathbf{2}}$ |
| :--- | :---: | :---: | :---: | :---: | :---: |
| CTHERM7 | $7.5 \mathrm{e}-2$ | $8 \mathrm{e}-2$ | $8 \mathrm{e}-2$ | $8 \mathrm{e}-2$ | $8 \mathrm{e}-2$ |
| CTHERM8 | 1 | 1.5 | 2 | 2 | 2.5 |
| RTHERM6 | 25 | 22 | 22 | 22 | 22 |
| RTHERM7 | 65 | 45 | 40 | 38 | 38 |
| RTHERM8 | 70 | 55 | 48 | 43 | 38 |



|  | INCHES |  | MILLIMETERS |  |  |
| :---: | :---: | :--- | :---: | :---: | :---: |
| SYMBOL | MIN | MAX | MIN | MAX |  |
| A | 0.0532 | 0.0688 | 1.35 | 1.75 | - |
| $\mathrm{A}_{1}$ | 0.004 | 0.0098 | 0.10 | 0.25 | - |
| b | 0.013 | 0.020 | 0.33 | 0.51 | - |
| c | 0.0075 | 0.0098 | 0.19 | 0.25 | - |
| D | 0.189 | 0.1968 | 4.80 | 5.00 | 2 |
| E | 0.2284 | 0.244 | 5.80 | 6.20 | - |
| $\mathrm{E}_{1}$ | 0.1497 | 0.1574 | 3.80 | 4.00 | 3 |
| e | 0.050 BSC |  | 1.27 |  | BSC |
| H | 0.0099 | 0.0196 | 0.25 | 0.50 | - |
| L | 0.016 | 0.050 | 0.40 | 1.27 | 4 |

NOTES:

1. All dimensions are within allowable dimensions of Rev. C of JEDEC MS-012AA outline dated 5-90.
2. Dimension "D" does not include mold flash, protrusions or gate burrs. Mold flash, protrusions or gate burrs shall not exceed 0.006 inches $(0.15 \mathrm{~mm})$ per side.
3. Dimension " $E_{1}$ " does not include inter-lead flash or protrusions. Inter-lead flash and protrusions shall not exceed 0.010 inches ( 0.25 mm ) per side.
4. "L" is the length of terminal for soldering.
5. The chamfer on the body is optional. If it is not present, a visual index feature must be located within the crosshatched area.
6. Controlling dimension: Millimeter.
7. Revision 8 dated 5-99.

MS-012AA


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