

### General Description

The AAT3239 MicroPower™ Low Dropout Linear Regulator is ideally suited for portable applications where very fast transient response, extended battery life and small size are critical. The AAT3239 has been specifically designed for high speed turn on and turn off performance, fast transient response, good power supply rejection ratio (PSRR) and is reasonably low noise, making it ideal for powering sensitive circuits with fast switching requirements.

Other features include low quiescent current, typically 70µA, and low dropout voltage which is typically less than 400mV at 300mA. The device is output short circuit protected and has a thermal shutdown circuit for additional protection under extreme operating conditions.

The AAT3239 also features a low-power shutdown mode for extended battery life. A reference bypass pin has been provided to improve PSRR performance and output noise, by connecting a small external capacitor from the AAT3239's reference output to ground.

The AAT3239 is available in an 8-pin TSOPJW-8 package in factory programmed voltages.

### Features

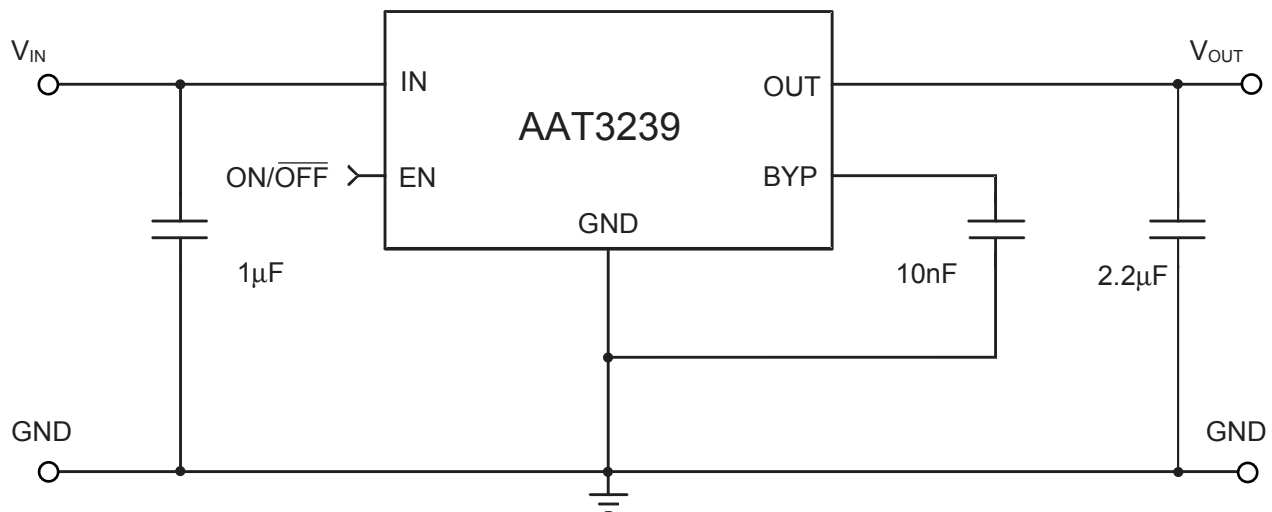
- 500mA Output Current
- Low Dropout - 400mV at 300mA
- High accuracy ±2.0%
- 70µA Quiescent Current
- Fast line and load transient response
- High speed device turn-on and shutdown
- High Power Supply Rejection Ratio
- Low self noise
- Short circuit protection
- Over-Temperature protection
- Uses Low ESR ceramic capacitors
- Noise reduction bypass capacitor
- Shutdown mode for longer battery life
- Low temperature coefficient
- TSOPJW 8-pin package

### Applications

- Cellular Phones
- Notebook Computers
- Portable Communication Devices
- Personal Portable Electronics
- Digital Cameras

Preliminary Information

### Typical Application

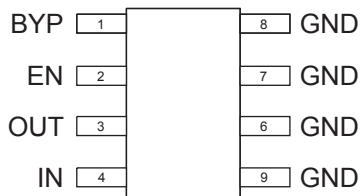


## Pin Descriptions

Pin #	Symbol	Function
1	BYP	Bypass capacitor connection - to improve AC ripple rejection, connect a 10nF capacitor to GND. This will also provide a soft start function.
2	EN	Enable pin - this pin should not be left floating. When pulled low the PMOS pass transistor turns off and all internal circuitry enters low-power mode, consuming less than 1µA.
3	OUT	Output pin - should be decoupled with 2.2µF ceramic capacitor.
4	IN	Input voltage pin - should be decoupled with 1µF or greater capacitor.
5, 6, 7, 8	GND	Ground connection pin

## Pin Configuration

**TSOPJW-8**  
**(Top View)**



## Absolute Maximum Ratings<sup>1</sup>

Symbol	Description	Value	Units
$V_{IN}$	Input Voltage	6	V
$V_{ENIN(MAX)}$	Maximum EN to Input Voltage	0.3	V
$I_{OUT}$	DC Output Current	$P_D/(V_{IN}-V_O)$	mA
$T_J$	Operating Junction Temperature Range	-40 to 150	°C

Note 1: Stresses above those listed in Absolute Maximum Ratings may cause permanent damage to the device. Functional operation at conditions other than the operating conditions specified is not implied. Only one Absolute Maximum rating should be applied at any one time.

## Thermal Information

Symbol	Description	Rating	Units
$\Theta_{JA}$	Maximum Thermal Resistance <sup>2</sup>	90	°C/W
$P_D$	Maximum Power Dissipation <sup>2,3</sup> ( $T_A = 25^\circ\text{C}$ )	1.11	W

Note 2: Mounted on a demo board.

Note 3: Derate 11.1 mW/°C above 25°C.

## Recommended Operating Conditions

Symbol	Description	Rating	Units
$V_{IN}$	Input Voltage <sup>4</sup>	( $V_{OUT}+V_{DO}$ ) to 5.5	V
T	Ambient Temperature Range	-40 to +85	°C

Note 4: To calculate minimum input voltage, use the following equation:  $V_{IN(MIN)} = V_{OUT(MAX)} + V_{DO(MAX)}$  as long as  $V_{IN} \geq 2.5\text{V}$ .

### Electrical Characteristics<sup>3</sup>

( $V_{IN} = V_{OUT(NOM)} + 1.2V$  for  $V_{OUT}$  options greater than 1.5V.  $V_{IN} = 2.5$  for  $V_{OUT} \leq 1.5V$ .  $I_{OUT} = 1mA$ ,  $C_{OUT} = 2.2\mu F$ ,  $C_{IN} = 1\mu f$ ,  $T_A = -40$  to  $85^\circ C$  unless otherwise noted. Typical values are  $T_A = 25^\circ C$ )

Symbol	Description	Conditions	Min	Typ	Max	Units	
$V_{OUT}$	Output Voltage Tolerance	$I_{OUT} = 1mA$ to $300mA$	$T_A = 25^\circ C$	-1.5		1.5	%
			$T_A = -40$ to $85^\circ C$	-2.5		2.5	
		$I_{OUT} = 1mA$ to $500mA$	$T_A = 25^\circ C$	-2.0		2.0	
			$T_A = -40$ to $85^\circ C$	-3.5		3.5	
$I_{OUT}$	Output Current	$V_{OUT} > 1.2V$	500			mA	
$V_{DO}$	Dropout Voltage <sup>1,2</sup>	$I_{OUT} = 300mA$		400	600	mV	
		$I_{OUT} = 500mA$		0.8	1.2	V	
$I_{SC}$	Short Circuit Current	$V_{OUT} < 0.4V$		600		mA	
$I_Q$	Ground Current	$V_{IN} = 5V$ , No load, $EN = V_{IN}$		70	125	$\mu A$	
$I_{SD}$	Shutdown Current	$V_{IN} = 5V$ , $EN = 0V$			1	$\mu A$	
$\frac{\Delta V_{OUT}}{V_{OUT}} \cdot \Delta V_{IN}$	Line Regulation	$V_{IN} = V_{OUT} + 1$ to $5.0V$			0.09	%/V	
$\Delta V_{OUT}(\text{line})$	Dynamic Line Regulation	$V_{IN} = V_{OUT} + 1V$ to $V_{OUT} + 2V$ , $I_{OUT} = 500mA$ , $T_R/T_F = 2\mu s$		2.5		mV	
$\Delta V_{OUT}(\text{load})$	Dynamic Load Regulation	$I_{OUT} = 1mA$ to $300mA$ , $T_R < 5\mu s$		100		mV	
		$I_{OUT} = 1mA$ to $500mA$ , $T_R < 5\mu s$		120			
$t_{ENDLY}$	Enable Delay Time	BYP = open		15		$\mu s$	
$V_{EN(L)}$	Enable Threshold Low				0.6	V	
$V_{EN(H)}$	Enable Threshold High		1.5			V	
$I_{EN}$	Leakage Current on Enable Pin	$V_{EN} = 5V$			1	$\mu A$	
PSRR	Power Supply Rejection Ratio	$I_{OUT} = 10mA$ , $C_{BYP} = 10nF$	1 kHz		67	dB	
			10kHz		47		
			1MHz		45		
$T_{SD}$	Over Temp Shutdown Threshold			145		$^\circ C$	
$T_{HYS}$	Over Temp Shutdown Hysteresis			12		$^\circ C$	
$e_N$	Output Noise	Noise Power BW = 300Hz-50kHz		50		$\mu V_{rms}/rtHz$	
TC	Output Voltage Temp. Coeff.			22		ppm/ $^\circ C$	

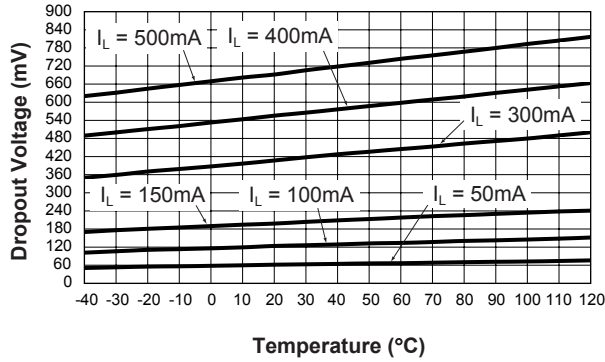
Notes:

- $V_{DO}$  is defined as  $V_{IN} - V_{OUT}$  when  $V_{OUT}$  is 98% of nominal.
- For  $V_{OUT} < 2.1V$ ,  $V_{DO} = 2.5V - V_{OUT}$ .
- The AAT 3239 is guaranteed to meet performance over the  $-40$  to  $85^\circ C$  operating temperature range and are assured by design, characterization and correlation with statistical process controls.

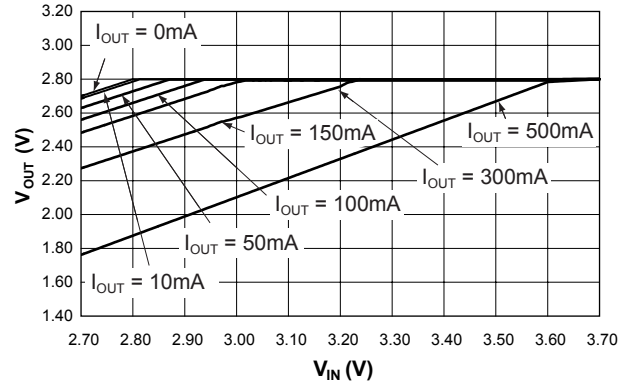
## Typical Characteristics

(Unless otherwise noted,  $V_{IN} = 5V$ ,  $T_A = 25^\circ C$ )

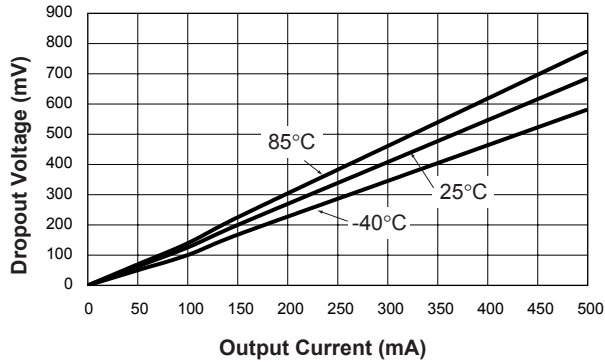
### Dropout Voltage vs. Temperature



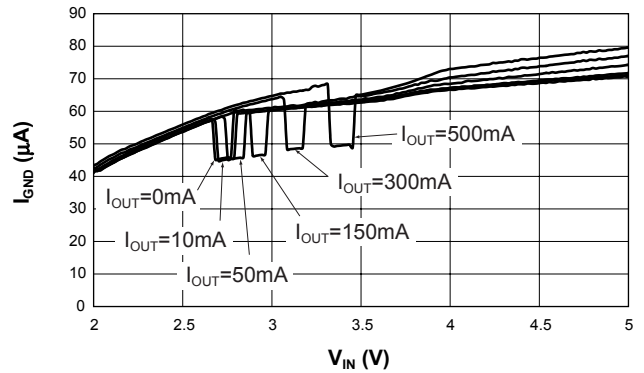
### Dropout Characteristics



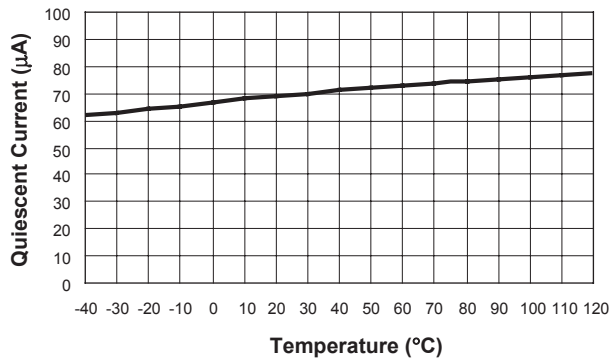
### Dropout Voltage vs. Output Current



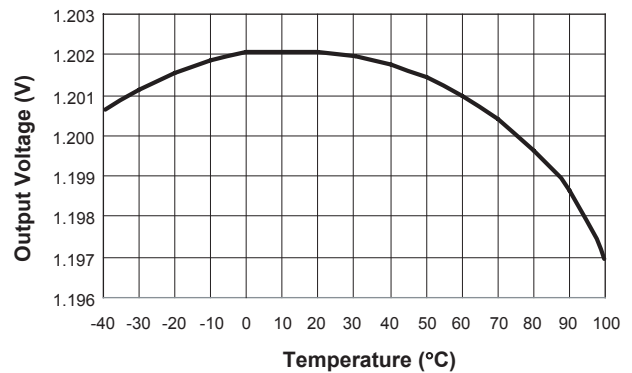
### Ground Current vs. Input Voltage



### Quiescent Current vs. Temperature



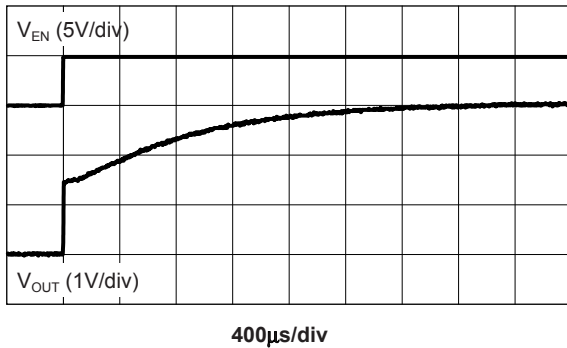
### Output Voltage vs. Temperature



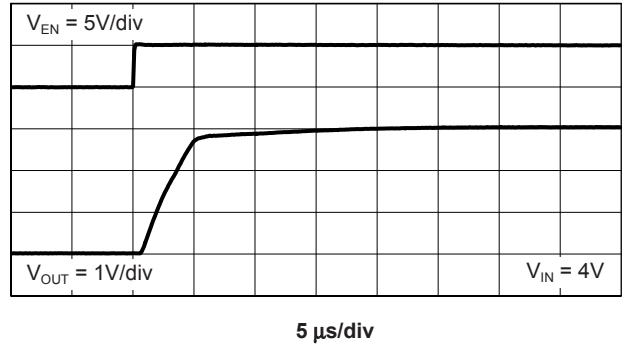
### Typical Characteristics

(Unless otherwise noted,  $V_{IN} = 5V$ ,  $T_A = 25^\circ C$ )

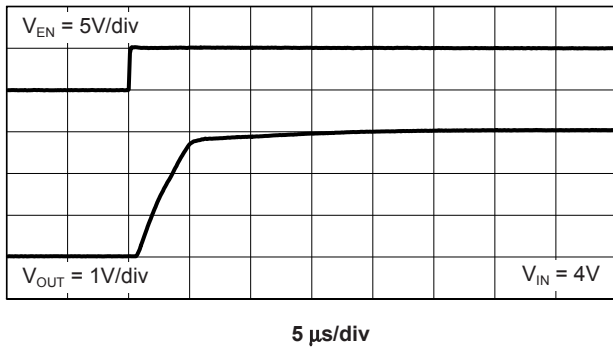
**Initial Power Up Response Time**  
 $C_{BYP} = 10nF$



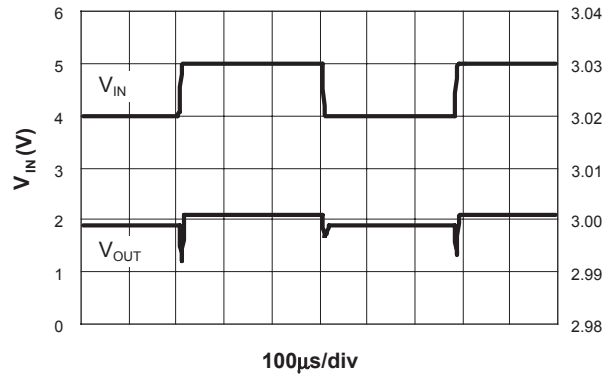
**Turn-ON Time From Enable ( $V_{IN}$  present)**  
 $C_{BYP} = 10nF$



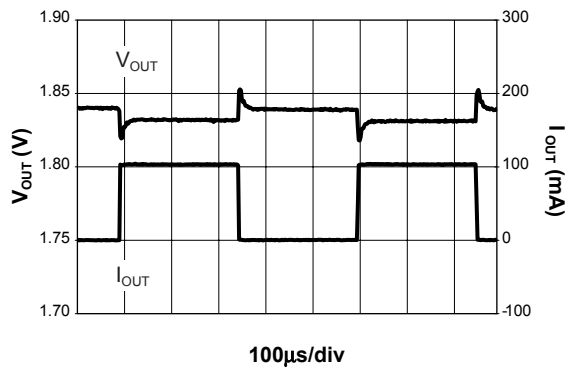
**Turn-ON Time From Enable ( $V_{IN}$  present)**  
 $C_{BYP} = 10nF$



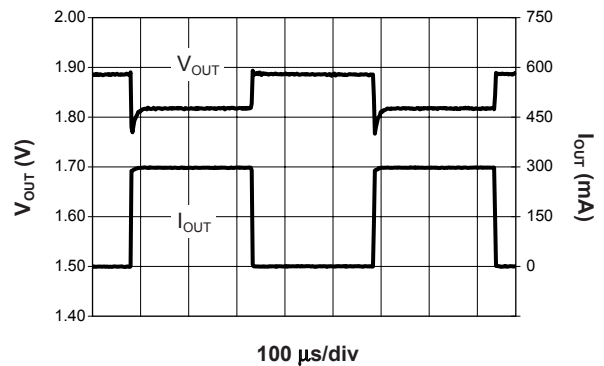
**Line Transient Response**



**Load Transient Response 100mA**

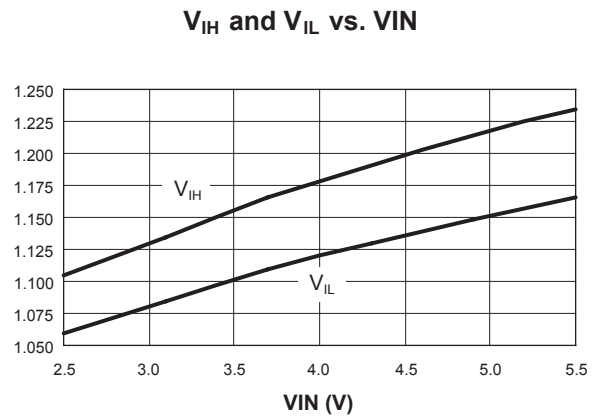
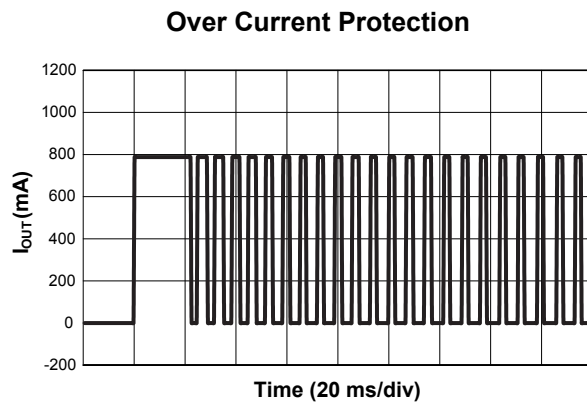
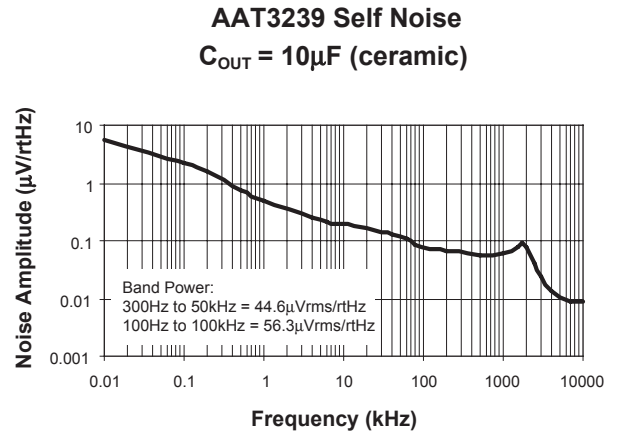
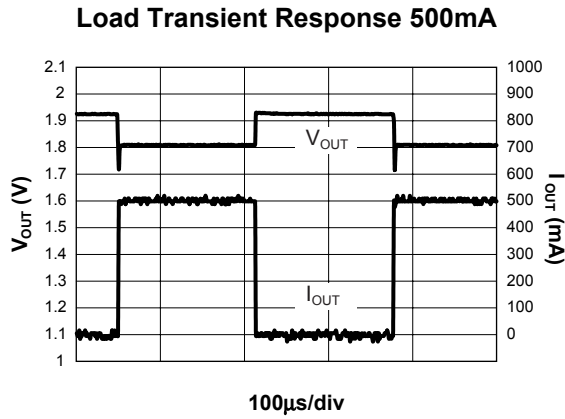


**Load Transient Response 300mA**

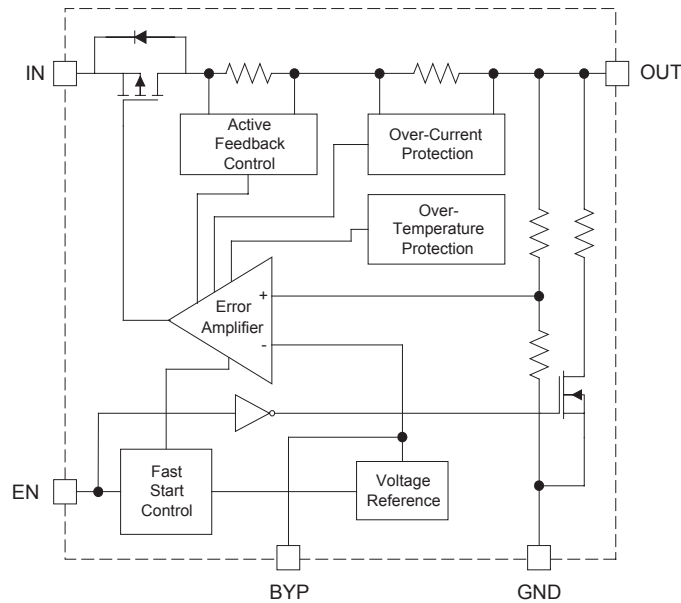


## Typical Characteristics

(Unless otherwise noted,  $V_{IN} = 5V$ ,  $T_A = 25^\circ C$ )



## Functional Block Diagram



## Functional Description

The AAT3239 is intended for LDO regulator applications where output current load requirements range from no load to 500mA. Refer to the Thermal Considerations discussion in this section for details on maximum power dissipation.

The advanced circuit design of the AAT3239 has been specifically optimized for very fast start-up and shutdown timing. This CMOS LDO has been tailored for superior transient response characteristics, a trait which is particularly important for applications that require fast power supply timing, such as GSM cellular telephone handsets.

The high-speed turn-on capability of the AAT3239 is enabled through the implementation of a fast start control circuit, which accelerates the power up behavior of fundamental control and feedback circuits within the LDO regulator.

Fast turn-off time response is achieved by an active output pull down circuit, which is enabled when the LDO regulator is placed in the shutdown mode. This active fast shutdown circuit has no adverse effect on normal device operation.

The AAT3239 has very fast transient response characteristics, which is an important feature for

applications where fast line and load transient response is required. This rapid transient response behavior is accomplished through the implementation of an active error amplifier feedback control. This proprietary circuit design is unique to this MicroPower™ LDO regulator.

The LDO regulator output has been specifically optimized to function with low cost, low ESR ceramic capacitors. However, the design will allow for operation over a wide range of capacitor types.

A bypass pin has been provided to allow the addition of an optional voltage reference bypass capacitor to reduce output self noise and increase power supply ripple rejection. Device self noise and PSRR will be improved by the addition of a small ceramic capacitor in this pin. However, increased values of  $C_{\text{BYPASS}}$  may slow down the LDO regulator turn-on time.

This LDO regulator has complete short circuit and thermal protection. The integral combination of these two internal protection circuits give the AAT3239 a comprehensive safety system to guard against extreme adverse operating conditions. Device power dissipation is limited to the package type and thermal dissipation properties. Refer to the thermal considerations discussion in the section for details on device operation at maximum output current loads.



## Applications Information

To assure the maximum possible performance is obtained from the AAT3239, please refer to the following application recommendations.

### Input Capacitor

Typically a 1 $\mu$ F or larger capacitor is recommended for  $C_{IN}$  in most applications. A  $C_{IN}$  capacitor is not required for basic LDO regulator operation. However, if the AAT3239 is physically located more than 3 centimeters from an input power source, a  $C_{IN}$  capacitor will be needed for stable operation.  $C_{IN}$  should be located as close to the device  $V_{IN}$  pin as practically possible.  $C_{IN}$  values greater than 1 $\mu$ F will offer superior input line transient response and will assist in maximizing the highest possible power supply ripple rejection.

Ceramic, tantalum or aluminum electrolytic capacitors may be selected for  $C_{IN}$ . There is no specific capacitor ESR requirement for  $C_{IN}$ . However, for 500mA LDO regulator output operation, ceramic capacitors are recommended for  $C_{IN}$  due to their inherent capability over tantalum capacitors to withstand input current surges from low impedance sources such as batteries in portable devices.

### Output Capacitor

For proper load voltage regulation and operational stability, a capacitor is required between pins  $V_{OUT}$  and GND. The  $C_{OUT}$  capacitor connection to the LDO regulator ground pin should be made as direct as practically possible for maximum device performance.

The AAT3239 has been specifically designed to function with very low ESR ceramic capacitors. For best performance, ceramic capacitors are recommended.

Typical output capacitor values for maximum output current conditions range from 1 $\mu$ F to 10 $\mu$ F. Applications utilizing the exceptionally low output noise and optimum power supply ripple rejection characteristics of the AAT3239 should use 2.2 $\mu$ F or greater for  $C_{OUT}$ . If desired,  $C_{OUT}$  may be increased without limit.

In low output current applications where output load is less than 10mA, the minimum value for  $C_{OUT}$  can be as low as 0.47 $\mu$ F.

## Bypass Capacitor and Low Noise Applications

A bypass capacitor pin is provided to enhance the low noise characteristics of the AAT3239 LDO regulator. The bypass capacitor is not necessary for operation of the AAT3239. However, for best device performance, a small ceramic capacitor should be placed between the Bypass pin (BYP) and the device ground pin (GND). The value of  $C_{BYP}$  may range from 470pF to 10nF. For lowest noise and best possible power supply ripple rejection performance a 10nF capacitor should be used. To practically realize the highest power supply ripple rejection and lowest output noise performance, it is critical that the capacitor connection between the BYP pin and GND pin be direct and PCB traces should be as short as possible. Refer to the PCB Layout Recommendations section of this document for examples.

There is a relationship between the bypass capacitor value and the LDO regulator turn on time and turn off time. In applications where fast device turn on time and turn off time is desired, the value of  $C_{BYP}$  should be reduced.

In applications where low noise performance and/or ripple rejection are less of a concern, the bypass capacitor may be omitted. The fastest device turn on time will be realized when no bypass capacitor is used.

DC leakage on this pin can affect the LDO regulator output noise and voltage regulation performance. For this reason, the use of a low leakage, high quality ceramic (NPO or COG type) or film capacitor is highly recommended.

### Capacitor Characteristics

Ceramic composition capacitors are highly recommended over all other types of capacitors for use with the AAT3239. Ceramic capacitors offer many advantages over their tantalum and aluminum electrolytic counterparts. A ceramic capacitor typically has very low ESR, is lower cost, has a smaller PCB footprint and is non-polarized. Line and load transient response of the LDO regulator is improved by using low ESR ceramic capacitors. Since ceramic capacitors are non-polarized, they are not prone to incorrect connection damage.

## Applications Information

**Equivalent Series Resistance (ESR):** ESR is a very important characteristic to consider when selecting a capacitor. ESR is the internal series resistance associated with a capacitor, which includes lead resistance, internal connections, size and area, material composition and ambient temperature. Typically capacitor ESR is measured in milliohms for ceramic capacitors and can range to more than several ohms for tantalum or aluminum electrolytic capacitors.

**Ceramic Capacitor Materials:** Ceramic capacitors less than 0.1 $\mu$ F are typically made from NPO or COG materials. NPO and COG materials are typically tight tolerance very stable over temperature. Larger capacitor values are typically composed of X7R, X5R, Z5U and Y5V dielectric materials. Large ceramic capacitors, typically greater than 2.2 $\mu$ F are often available in the low cost Y5V and Z5U dielectrics. These two material types are not recommended for use with LDO regulators since the capacitor tolerance can vary more than  $\pm 50\%$  over the operating temperature range of the device. A 2.2 $\mu$ F Y5V capacitor could be reduced to 1 $\mu$ F over temperature, this could cause problems for circuit operation. X7R and X5R dielectrics are much more desirable. The temperature tolerance of X7R dielectric is better than  $\pm 15\%$ .

Capacitor area is another contributor to ESR. Capacitors which are physically large in size will have a lower ESR when compared to a smaller sized capacitor of an equivalent material and capacitance value. These larger devices can improve circuit transient response when compared to an equal value capacitor in a smaller package size.

Consult capacitor vendor data sheets carefully when selecting capacitors for LDO regulators.

### Enable Function

The AAT3239 features an LDO regulator enable/disable function. This pin (EN) is active high and is compatible with CMOS logic. To assure the LDO regulator will switch on, the EN turn on control level must be greater than 1.5 volts. The LDO regulator will go into the disable shutdown mode when the voltage on the EN pin falls below 0.6 volts. If the enable function is not needed in a specific application, it may be tied to  $V_{IN}$  to keep the LDO regulator in a continuously on state.

When the LDO regulator is in the shutdown mode, an internal 1.5k $\Omega$  resistor is connected between  $V_{OUT}$  and GND. This is intended to discharge  $C_{OUT}$  when the LDO regulator is disabled. The internal 1.5k $\Omega$  has no adverse effect on device turn on time.

### Short Circuit Protection

The AAT3239 contains an internal short circuit protection circuit that will trigger when the output load current exceeds the internal threshold limit. Under short circuit conditions the output of the LDO regulator will be current limited until the short circuit condition is removed from the output or LDO regulator package power dissipation exceeds the device thermal limit.

### Thermal Protection

The AAT3239 has an internal thermal protection circuit which will turn on when the device die temperature exceeds 145°C. The internal thermal protection circuit will actively turn off the LDO regulator output pass device to prevent the possibility of over temperature damage. The LDO regulator output will remain in a shutdown state until the internal die temperature falls back below the 145°C trip point.

The combination and interaction between the short circuit and thermal protection systems allow the LDO regulator to withstand indefinite short circuit conditions without sustaining permanent damage.

### No-Load Stability

The AAT3239 is designed to maintain output voltage regulation and stability under operational no-load conditions. This is an important characteristic for applications where the output current may drop to zero.

### Reverse Output to Input Voltage Conditions and Protection

Under normal operating conditions a parasitic diode exists between the output and input of the LDO regulator. The input voltage should always remain greater than the output load voltage maintaining a reverse bias on the internal parasitic diode. Conditions where  $V_{OUT}$  might exceed  $V_{IN}$  should be avoided since this would forward bias the internal parasitic diode and allow excessive current flow into the  $V_{OUT}$  pin possibly damaging the LDO regulator.

### Applications Information

In applications where there is a possibility of  $V_{OUT}$  exceeding  $V_{IN}$  for brief amounts of time during normal operation, the use of a larger value  $C_{IN}$  capacitor is highly recommended. A larger value of  $C_{IN}$  with respect to  $C_{OUT}$  will effect a slower  $C_{IN}$  decay rate during shutdown, thus preventing  $V_{OUT}$  from exceeding  $V_{IN}$ . In applications where there is a greater danger of  $V_{OUT}$  exceeding  $V_{IN}$  for extended periods of time, it is recommended to place a Schottky diode across  $V_{IN}$  to  $V_{OUT}$  (connecting the cathode to  $V_{IN}$  and anode to  $V_{OUT}$ ). The Schottky diode forward voltage should be less than 0.45 volts.

### Thermal Considerations and High Output Current Applications

The AAT3239 is designed to deliver a continuous output load current of 500mA under normal operations. The short circuit current limit is greater than 500mA, typically active at 600mA..

The limiting characteristics for the maximum output load current safe operating area is essentially package power dissipation, the internal preset thermal limit of the device, and the input-to-output voltage drop across the AAT3239. In order to obtain high operating currents, careful device layout and circuit operating conditions need to be taken into account.

The following discussions will assume the LDO regulator is mounted on a printed circuit board utilizing the minimum recommended footprint as stated in the layout considerations section of the document. At any given ambient temperature ( $T_A$ ) the maximum package power dissipation can be determined by the following equation:

$$P_{D(MAX)} = \frac{T_{J(MAX)} - T_A}{\theta_{JA}}$$

Constants for the AAT3239 are  $T_{J(MAX)}$ , the maximum junction temperature for the device which is 125°C and  $T_{JA} = 90^\circ\text{C/W}$ , the package thermal resistance. Typically, maximum conditions are calculated at the maximum operating temperature of  $T_A = 85^\circ\text{C}$  and under normal ambient conditions where  $T_A = 25^\circ\text{C}$ . Given  $T_A = 85^\circ\text{C}$ , the maximum package power dissipation is 444mW. At  $T_A = 25^\circ\text{C}$ , the maximum package power dissipation is 1.11W.

The maximum continuous output current for the AAT3239 is a function of the package power dissipation and the input to output voltage drop across the LDO regulator. Refer to the following simple equation:

$$I_{OUT(MAX)} < \frac{P_{D(MAX)}}{V_{IN} - V_{OUT}}$$

For example, if  $V_{IN} = 4.2\text{V}$ ,  $V_{OUT} = 1.8\text{V}$  and  $T_A = 25^\circ\text{C}$ ,  $I_{OUT(MAX)} < 463\text{mA}$ . If the output load current were to exceed 463mA or if the ambient temperature were to increase, the internal die temperature will increase. If the condition remained constant, the LDO regulator thermal protection circuit will activate.

To figure what the maximum output current would be for a given output voltage, refer to the following equation. This calculation accounts for the total power dissipation of the LDO Regulator, including that caused by ground current.

$$P_{D(MAX)} = (V_{IN} - V_{OUT})I_{OUT} + (V_{IN} \times I_{GND})$$

This formula can be solved for  $I_{OUT}$  to determine the maximum output current.

$$I_{OUT} = \frac{P_{D(MAX)} - (V_{IN} \times I_{GND})}{V_{IN} - V_{OUT}}$$

The following is an example for an AAT3239 set for a 1.5 volt output:

From the discussion above,  $P_{D(MAX)}$  was determined to equal 1.11W at  $T_A = 25^\circ\text{C}$ .

$$V_{OUT} = 1.5\text{V}$$

$$V_{IN} = 4.2\text{V}$$

$$I_{GND} = 125\mu\text{A}$$

$$I_{OUT} = \frac{1.11\text{W} - (4.2\text{V} \times 125\mu\text{A})}{4.2 - 1.5}$$

$$I_{OUT(MAX)} = 411\text{mA}$$

Thus, the AAT3239 can sustain a constant 1.5V output at a 411mA load current at an ambient temperature of  $25^\circ\text{C}$ . Higher input to output voltage differentials can be obtained with the AAT3239, while maintaining device functions within the thermal safe operating area. To accomplish this, the device thermal resistance must be reduced by increasing the heat sink area or by operating the LDO regulator in a duty cycled mode.

For example, an application requires  $V_{IN} = 4.2\text{V}$  while  $V_{OUT} = 1.5\text{V}$  at a 500mA load and  $T_A = 25^\circ\text{C}$ .  $V_{IN}$  is greater than 3.7V, which is the maximum safe

continuous input level for  $V_{OUT} = 1.5\text{V}$  at 500mA for  $T_A = 25^\circ\text{C}$ . To maintain this high input voltage and output current level, the LDO regulator must be operated in a duty cycled mode. Refer to the following calculation for duty cycle operation:

$$P_{D(MAX)} \text{ is assumed to be } 1.1\text{W}$$

$$I_{GND} = 125\mu\text{A}$$

$$I_{OUT} = 500\text{mA}$$

$$V_{IN} = 4.2\text{V}$$

$$V_{OUT} = 1.5\text{V}$$

$$\%DC = \frac{100(P_{D(MAX)})}{(V_{IN} - V_{OUT})I_{OUT} + V_{IN} \times I_{GND}}$$

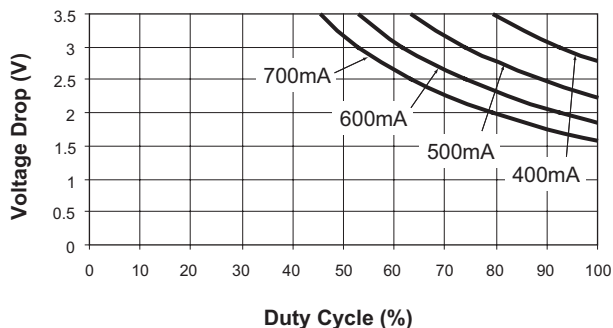
$$\%DC = \frac{100(1.11\text{W})}{(4.2\text{V} - 1.5\text{V})500\text{mA} + 4.2\text{V} \times 125\mu\text{A}}$$

$$\%DC = 82\%$$

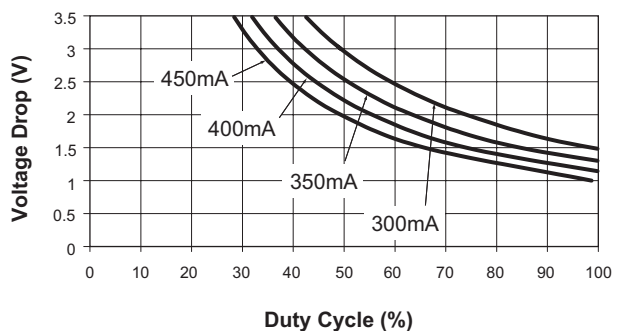
For a 500mA output current and a 2.7 volt drop across the AAT3239 at an ambient temperature of  $25^\circ\text{C}$ , the maximum on time duty cycle for the device would be 82%.

The following family of curves show the safe operating area for duty cycled operation from ambient room temperature to the maximum operating level.

**Device Duty Cycle vs.  $V_{DROP}$**   
 **$V_{OUT} = 1.5\text{V} @ 25^\circ\text{C}$**



**Device Duty Cycle vs.  $V_{DROP}$**   
 **$V_{OUT} = 1.5\text{V} @ 85^\circ\text{C}$**

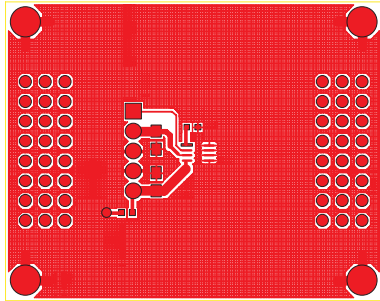


### Evaluation Board Layout

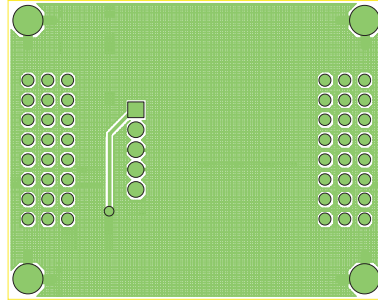
The AAT3239 evaluation layout follows the recommend printed circuit board layout procedures and

can be used as an example for good application layouts.

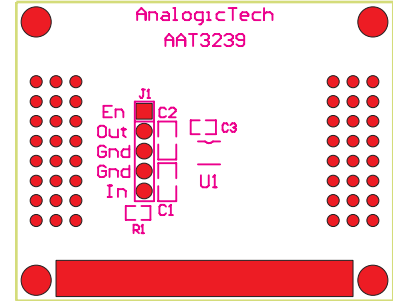
Note: Board layout shown is not to scale.



**Figure 3: Evaluation board component side layout**



**Figure 4: Evaluation board solder side layout**



**Figure 5: Evaluation board top side silk screen layout / assembly drawing**

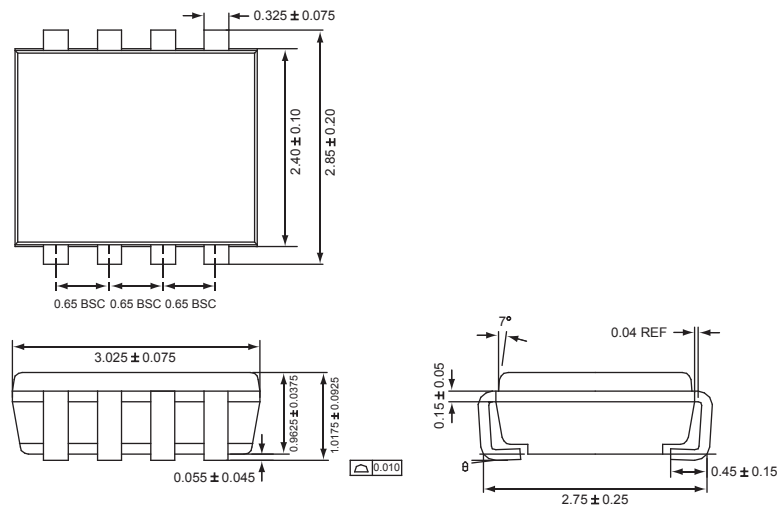
## Ordering Information

Output Voltage	Package	Marking <sup>1</sup>	Part Number (Tape and Reel)
1.5V	TSOPJW-8	JVXY	AAT3239ITS-1.5-T1
1.85V	TSOPJW-8	JWXY	AAT3239ITS-1.85-T1
3.3V	TSOPJW-8	MAXY	AAT3239ITS-3.3-T1

Note 1: XYY = assembly and date code.

## Package Information

### TSOPJW-8



All dimensions in millimeters.

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