# ASSP For Power Management Applications BIPOLAR

# Switching Regulator Controller (Switchable between push-pull and single-end functions)

# **MB3759**

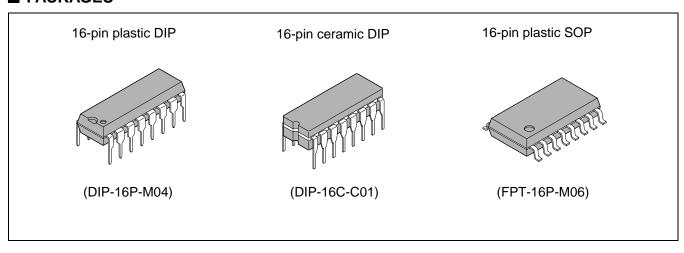
#### **■ DESCRIPTION**

The MB3759 is a control IC for constant-frequency pulse width modulated switching regulators. The IC contains most of the functions required for switching regulator control circuits. This reduces both the component count and assembly work.

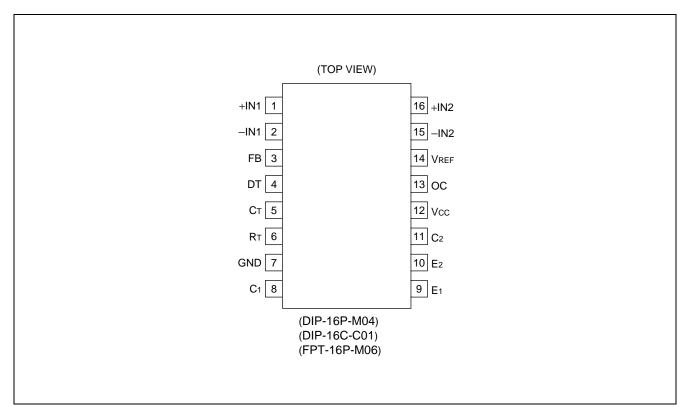
#### **■ FEATURES**

- Drives a 200 mA load
- Can be set to push-pull or single-end operation
- Prevents double pulses
- · Adjustable dead-time
- Error amplifier has wide common phase input range
- Built in a circuit to prevent misoperation due to low power supply voltage.
- Built in an internal 5 V reference voltage with superior voltage reduction characteristics

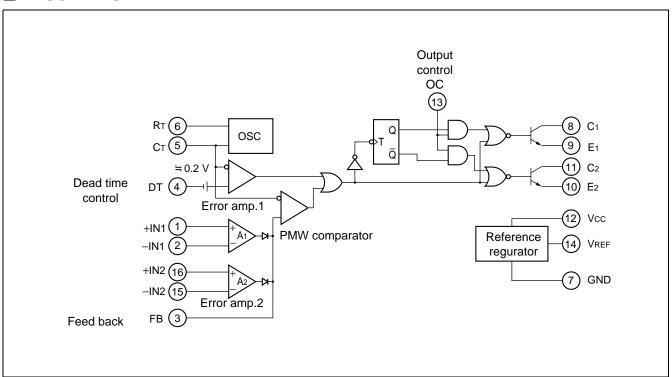
#### ■ PACKAGES



## **■ PIN ASSIGNMENT**



# **■ BLOCK DIAGRAM**



### ■ ABSOLUTE MAXIMUM RATINGS

Parameter		Symbol	Condition	Ra	Unit	
		Syllibol	Condition	Min	Max	
Power supply voltage		Vcc	_	_	41	V
Collector output voltage		Vce	_	_	41	V
Collector output current		Ice	_	_	250	mA
Amplifier input voltage		Vı	_	_	Vcc + 0.3	V
	Plastic DIP		Ta ≤ +25 °C	_	1000	
Power dissipation	Ceramic DIP	P□	Ta ≤ +60 °C	_	800	mW
	SOP *		Ta ≤ +25 °C	_	620	
Operating temperature		Тор	_	-30	+85	°C
Storage temperature		Tstg	_	-55	+125	°C

<sup>\*:</sup> When mounted on a 4 cm square double-sided epoxy circuit board (1.5 mm thickness)
The ceramic circuit board is 3 cm x 4 cm (0.5 mm thickness)

WARNING: Semiconductor devices can be permanently damaged by application of stress (voltage, current, temperature, etc.) in excess of absolute maximum ratings. Do not exceed these ratings.

#### ■ RECOMMENDED OPERATING CONDITIONS

Parameter	Symbol	Value				
Farameter	Syllibol	Min	Min Typ		Unit	
Power supply voltage	Vcc	7	15	32	V	
Collector output voltage	Vce	_	_	40	V	
Collector output current	ICE	5	_	200	mA	
Amplifier input voltage	Vin	-0.3	0 to V <sub>R</sub>	Vcc – 2	V	
FB sink current	Isink	_	_	0.3	mA	
FB source current	Isource	_	_	2	mA	
Reference section output current	IREF	_	5	10	mA	
Timing resistor	R⊤	1.8	30	500	kΩ	
Timing capacitor	Ст	470	1000	10 <sup>6</sup>	pF	
Oscillator frequency	fosc	1	40	300	kHz	
Operating temperature	Тор	-30	+25	+85	°C	

Note: Values are for standard derating conditions. Give consideration to the ambient temperature and power consumption if using a high supply voltage.

WARNING: The recommended operating conditions are required in order to ensure the normal operation of the semiconductor device. All of the device's electrical characteristics are warranted when the device is operated within these ranges.

Always use semiconductor devices within their recommended operating condition ranges. Operation outside these ranges may adversely affect reliability and could result in device failure.

No warranty is made with respect to uses, operating conditions, or combinations not represented on the data sheet. Users considering application outside the listed conditions are advised to contact their FUJITSU representatives beforehand.

# **■ ELECTRICAL CHARACTERISTICS**

(Vcc = 15 V, Ta = +25 °C)

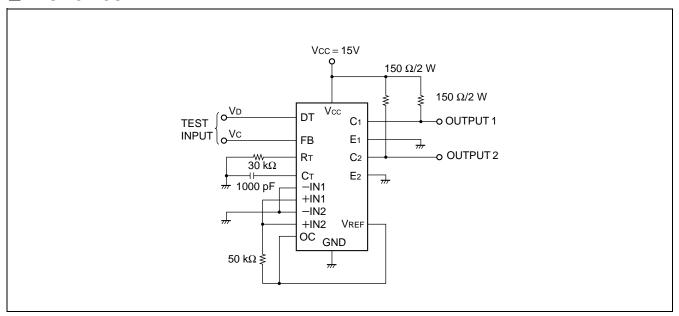
Parameter		Symbol Condition	Value			Unit		
			Condition	Min	Тур	Max	Offic	
Output voltage		V <sub>REF</sub>	lo = 1 mA	4.75	5.0	5.25	V	
	Input regulation		$\Delta V_{R(IN)}$	7 V ≤ Vcc ≤ 40 V, Ta = +25 °C	_	2	25	mV
	Load regulation		$\Delta V_{\text{R(LD)}}$	1 mA $\leq$ lo $\leq$ 10 mA, Ta = +25 °C	_	-1	-15	mV
Reference section	Temperature	e stability	$\Delta V_R/\Delta T$	–20 °C ≤ Ta ≤ + 85 °C	_	±200	±750	μV/°C
		Short circuit output current		_	15	40	_	mA
	Reference lockout voltage		_	_	_	4.3	_	V
	Reference hysteresis voltage		_	_	_	0.3	_	V
	Oscillator frequency Standard deviation of frequency Frequency change with voltage		fosc	$R_T = 30 \text{ k}\Omega,$ $C_T = 1000 \text{ pF}$	36	40	44	kHz
Oscillator			_	$R_T = 30 \text{ k}\Omega,$ $C_T = 1000 \text{ pF}$	_	±3	_	%
section			_	7 V ≤ Vcc ≤ 40 V, Ta = +25 °C	_	±0.1	_	%
	Frequency change with temperature		Δfosc/ΔT	–20 °C ≤ Ta ≤ +85 °C	_	±0.01	±0.03	%/°C
Input bias current		lο	0 ≤ Vı ≤ 5.25 V		-2	-10	μА	
Dead-time control section	Maximum duty cycle (Each output)		_	$V_1 = 0$	40	45	_	%
	Input threshold voltage	0% duty cycle	V <sub>DO</sub>	_	_	3.0	3.3	V
		Max. duty cycle	V <sub>DM</sub>	_	0	_	_	V

# (Continued)

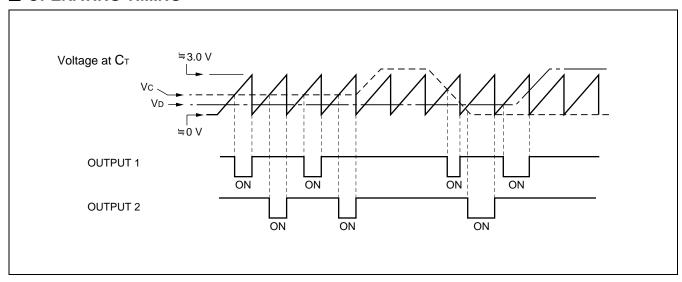
(Vcc = 15 V, Ta = +25 °C)

Parameter		Symbol	Symbol Condition	Value			Unit	
		Symbol	Condition	Min	Тур	Max	Unit	
	Input offset	voltage	Vio	Vo (pin3) = 2.5 V	_	±2	±10	mV
	Input offset current		lio	Vo (pin3) = 2.5 V	_	±25	±250	nA
	Input bias cu	urrent	lı	Vo (pin3) = 2.5 V	_	-0.2	-1.0	μΑ
	Common-mon-mon-mon-mon-mon-mon-mon-mon-mo	ode input	Vсм	7 V ≤ Vcc ≤ 40 V	-0.3	_	Vcc – 2	V
Error amplifier	Open-loop v amplificatio	-	Av	0.5 V ≤ V <sub>0</sub> ≤ 3.5 V	70	95	_	dB
section	Unity-gain b	andwidth	BW	A <sub>V</sub> = 1	_	800	_	kHz
	Common-merejection ration		CMR	Vcc = 40 V	65	80	_	dB
	Output sink	ISINK	Isink	$-5 \text{ V} \le \text{V}_{\text{ID}} \le -15 \text{ mV},$ Vo = 0.7 V	0.3	0.7	_	mA
	current (pin 3)	ISOURCE	Isource	15 mV $\leq$ V <sub>ID</sub> $\leq$ 5V, Vo = 3.5 V	-2	-10	_	mA
	Collector lea	akage current	Ico	Vce = 40 V, Vcc = 40 V	_	_	100	μА
	Emitter leakage current		leo	Vcc = Vc = 40 V, VE = 0	_	_	-100	μА
Output Collector emitter saturation voltage	Emitter grounded	Vsat(c)	V <sub>E</sub> = 0, I <sub>C</sub> = 200 mA	_	1.1	1.3	V	
		Emitter follower	VSAT(E)	Vc = 15 V, IE = -200 mA	_	1.5	2.5	V
	Output control input current		Горс	Vi = Vref	_	1.3	3.5	mA
PWM	Input thresh	old voltage	Vтн	0% Duty	_	4	4.5	V
comparator section Input sink		urrent (pin 3)	Isink	Vo (pin3) = 0.7 V	0.3	0.7	_	mA
Power supply current		Icc	V(pin4) = 2 V, See Fig-2	_	8	_	mA	
Standby current		Iccq	V(pin6) = VREF, I/O open	_	7	12	mA	
	Rise time	Emitter	<b>t</b> R	$R_L = 68 \Omega$	_	100	200	ns
Switching	Fall time	grounded	t⊧	$R_L = 68 \Omega$	_	25	100	ns
characteristics	Rise time	Emitter	<b>t</b> R	$R_L = 68 \Omega$	_	100	200	ns
	Fall time	follower	t⊧	$R_L = 68 \Omega$		40	100	ns

# **■ TEST CIRCUIT**



# **■** OPERATING TIMING



# **■ OSCILLATION FREQUENCY**

$$f \, osc = \frac{1.2}{R\tau \cdot C\tau}$$

$$R\tau : k\Omega$$

$$C\tau : \mu F$$

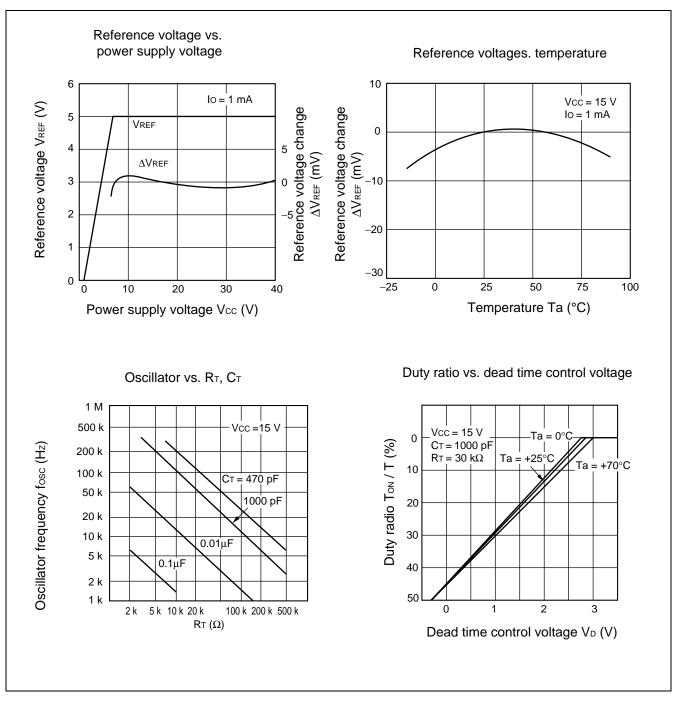
$$f osc : kHz$$

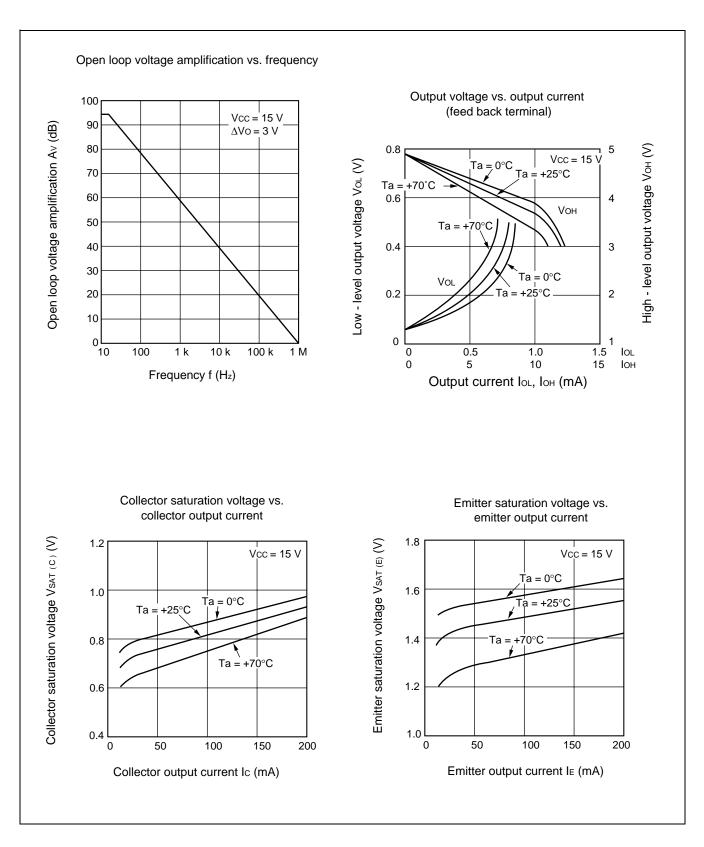
# **■ OUTPUT LOGIC TABLE**

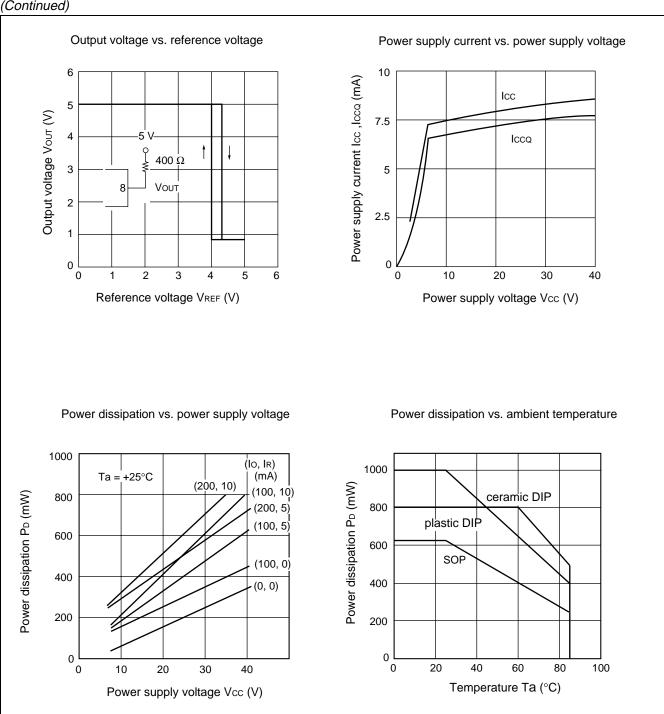
Input (Output Control)	Output State		
GND	Single-ended or parallel output		
Vref	Push-pull		

7

## **■ TYPICAL CHARACTERISTICS**







#### **■ BASIC OPERATION**

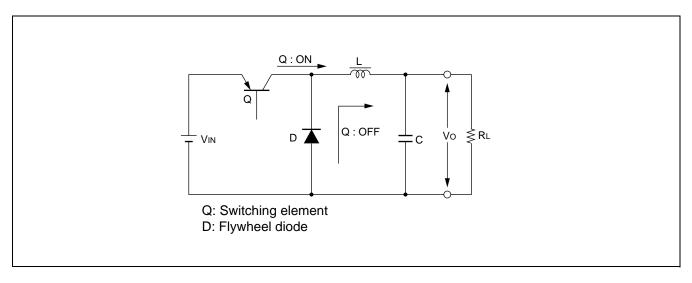
Switching regulators can achieve a high level of efficiency. This section describes the basic principles of operation using a chopper regulator as an example.

As shown in the diagram, diode D provides a current path for the current through inductance L when Q is off. Transistor Q performs switching and is operated at a frequency that provides a stable output. As the switching element is saturated when Q is on and cutoff when Q is off, the losses in the switching element are much less than for a series regulator in which the pass transistor is always in the active state.

While Q is conducting, the input voltage  $V_{IN}$  is supplied to the LC circuit and when Q is off, the energy stored in L is supplied to the load via diode D. The LC circuit smooths the input to supply the output voltage.

The output voltage Vo is given by the following equation.

$$Vo = \frac{Ton}{Ton + Toff} Vin = \frac{Ton}{T} Vin$$



As indicated by the equation, variation in the input voltage is compensated for by controlling the duty cycle (Ton/T). If V<sub>IN</sub> drops, the control circuit operates to increase the duty cycle so as to keep the output voltage constant. The current through L flows from the input to the output when Q is on and through D when Q is off. Accordingly, the average input current I<sub>IN</sub> is the product of the output current and the duty cycle for Q.

$$IIN = \frac{Ton}{T}Io$$

The theoretical conversion efficiency if the switching loss in Q and loss in D are ignored is as follows.

$$\eta = \frac{PO}{PIN} \times 100 \text{ (\%)}$$

$$= \frac{VO \cdot IO}{VIN \cdot IIN} \times 100$$

$$= \frac{VIN \cdot IO \cdot TON / T}{VIN \cdot IO \cdot TON / T} \times 100$$

$$= 100 \text{ (\%)}$$

The theoretical conversion efficiency is 100%. In practice, losses occur in the switching element and elsewhere, and design decisions to minimize these losses include making the switching frequency as low as practical and setting an optimum ratio of input to output voltage.

#### **■ SWITCHING ELEMENT**

### 1. Selection of the Switching Transistor

It can be said that the success or otherwise of a switching regulator is determined by the choice of switching transistor. Typically, the following parameters are considered in selecting a transistor.

- Withstand voltage
- Current
- Power
- Speed

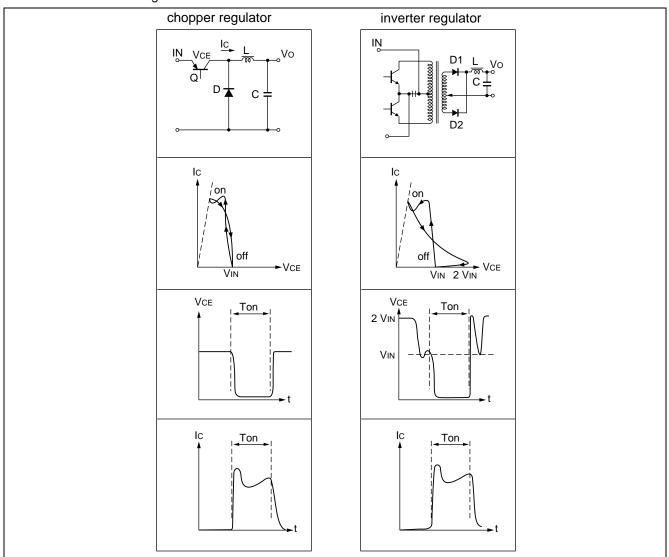
For the withstand voltage, current, and power, it is necessary to determine that the area of safe operation (ASO) of the intended transistor covers the intended range for these parameters.

The speed (switching speed: rise time tr, storage time tstg, and fall time tf) is related to the efficiency and also influences the power.

The figures show the transistor load curve and VcE - Ic waveforms for chopper and inverter-type regulators.

The chopper regulator is a relatively easy circuit to deal with as the diode clamps the collector. A peak can be seen immediately after turn-on. However, this is due to the diode and is explained later.

In an inverter regulator, the diodes on the secondary side act as a clamp. Viewed from the primary side, however, a leakage inductance is present. This results in an inductive spike which must be taken account of as it is added to double the  $V_{\text{IN}}$  voltage.

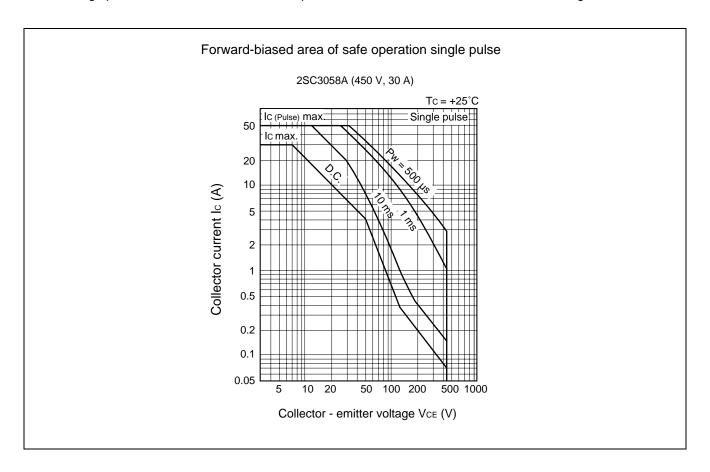


The figure below shows an example of the ASO characteristics for a forward-biased power transistor (2SC3058A) suitable for switching.

Check that the ASO characteristics for the transistor you intend to use fully covers the load curve. Next, check whether the following conditions are satisfied. If so, the transistor can be expected to perform the switching operation safely.

- The intended ON time does not exceed the ON-time specified for the ASO characteristic.
- The OFF-time ASO characteristic satisfies the intended operation conditions.
- Derating for the junction temperature has been taken into account.

For a switching transistor, the junction temperature is closely related to the switching speed. This is because the switching speed becomes slower as the temperature increases and this affects the switching losses.



#### 2. Selecting the Diode

Consideration must be given to the switching speed when selecting the diode. For chopper regulators in particular, the diode affects the efficiency and noise characteristics and has a big influence on the performance of the switching regulator.

If the reverse recovery time of the diode is slower than the turn-on time of the transistor, an in-rush current of more than twice the load current occurs resulting in noise (spikes) and reduced efficiency.

As a rule for diode selection, use a diode with a reverse recovery time  $t_{rr}$  that is sufficiently faster than the transistor  $t_{r}$ .

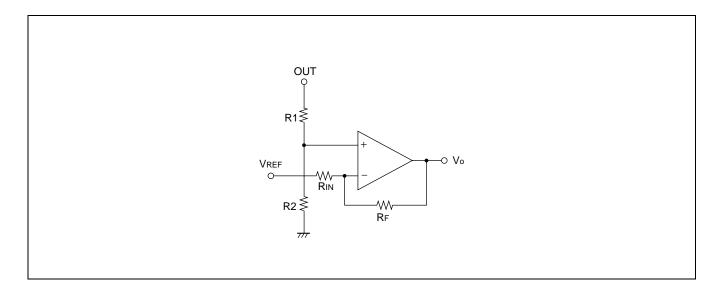
#### ■ APPLICATION IN PRACTICAL CIRCUITS

#### 1. Error Amplifier Gain Adjustment

Take care that the bias current does not become large when connecting an external circuit to the FB pin (pin 3) for adjusting the amplifier gain. As the FB pin is biased to the low level by a sink current, the duty cycle of the output signal will be affected if the current from the external circuit is greater than the amplifier can sink.

The figure below shows a suitable circuit for adjusting the gain.

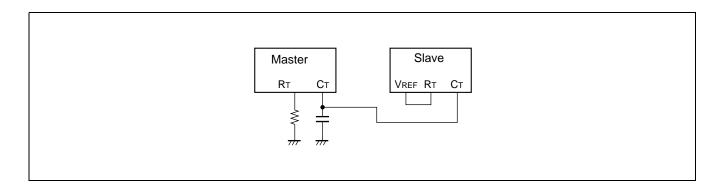
It is very important that you avoid having a capacitive load connected to the output stage as this will affect the response time.



### 2. Synchronized Oscillator Operation

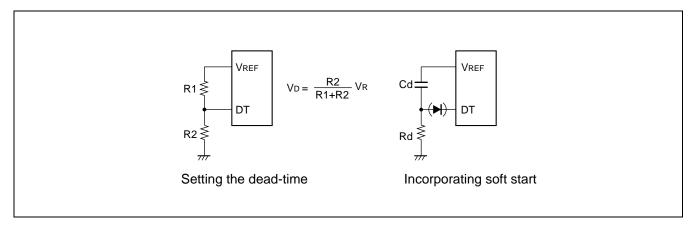
The oscillator can be halted by connecting the  $C_T$  pin to the GND pin. If supplying the signal externally, halt the internal oscillator and input to the  $C_T$  pin.

Using this method, multiple ICs can be used together in synchronized operation. For synchronized operation, set one IC as the master and connect the other ICs as shown in the diagram.



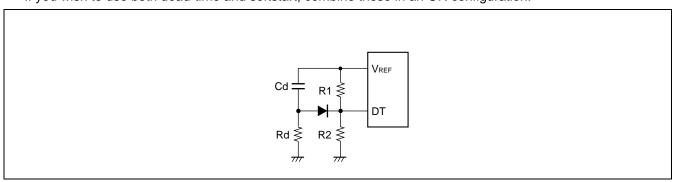
#### 3. Soft Start

A soft start function can be incorporated by using the dead-time control element.



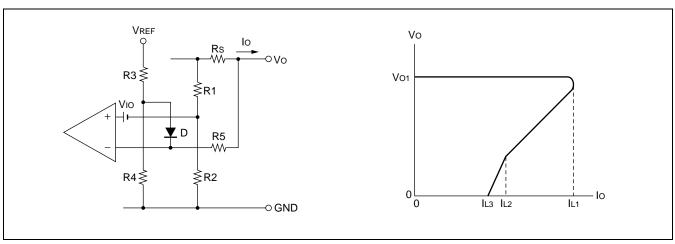
When the power is turned on, Cd is not yet charged and the DT input is pulled to the V<sub>REF</sub> pin causing the output transistor to turn off. Next, the input voltage to the DT pin drops in accordance with the Cd, Rd constant causing the output pulse width to increase steadily, providing stable control circuit operation.

If you wish to use both dead-time and softstart, combine these in an OR configuration.



#### 4. Output Current Limiting (Fallback system using a detection resistor inserted on the output side)

### (1) Typical example



• Initial limit current IL1

$$Vo > \frac{R4}{R3 + R4} VREF$$
 The condition for Vo is:

As the diode is reverse biased

Rs 
$$IL1 = \frac{R1}{R1 + R2} VO - VIO$$
  

$$\therefore IL1 = \frac{R1}{R1 + R2} \frac{VO}{Rs} - \frac{VIO}{Rs} \qquad Eq. (1) \text{ (where R2 >> R1)}$$

 $V_{10}$  is the input offset voltage to the op-amp (-10 mV  $\leq$   $V_{10} \leq$  +10 mV) and this causes the variation in  $I_{L}$ . Accordingly, if for example the variation in  $I_{L}$  is to be limited to  $\pm$ 10 %, using equation (1) and only considering the variation in the offset voltage gives the following:

$$Io = \frac{1}{Rs} \frac{R1}{R1 + R2} (Vo + Vee) - \frac{Vio}{Rs} (R2 >> R1)$$

This indicates a setting of 100 mV or more is required.

Polarity change point IL2

As this is the point where the diode becomes forward biased, it can be calculated by substituting [R4/(R3+R4)  $V_{REF}$  -  $V_D$ ] for  $V_D$  in equation (where  $V_D$  is the forward voltage of the diode).

$$IL2 = \frac{R1}{R1 + R2} \frac{R4/(R3 + R4) \cdot VREF - VD}{Rs} - \frac{VIO}{Rs}$$

• Final limit current I∟3

The limit current for  $V_0 = 0$  when  $R2 \gg R1$  is the point where the voltages on either side of Rs and on either side of Rs are biased.

Rs IL3 = 
$$\frac{R4R5 \text{ VREF} - R3R5 \text{ VD} - R4R5 \text{ VD}}{R3R4 + R3R5 + R4R5} - \text{VIO}$$

$$\therefore \text{IL3} = \frac{1}{Rs} \frac{1}{1 + (R3 // R4) / R5} (\frac{R4}{R3 + R4} \text{ VREF} - \text{VD}) - \frac{\text{VIO}}{Rs} (2) \text{ Eq.}$$

R3//R4 is the resistance formed by R3 and R4 in parallel (R3R4/(R3 + R4)). When R3//R4 << R5, equation (2) becomes:

IL3 C = 
$$\frac{1}{Rs}$$
  $\left(\frac{R4}{R3 + R4} VREF - VD\right) - \frac{VIO}{Rs}$ 

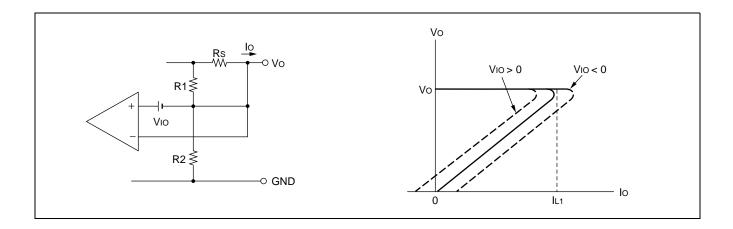
In addition to determining the limit current  $I_{L3}$  for  $V_0 = 0$ , R3, R4, R5, and diode D also operate as a starter when the power is turned on.

Starter circuit

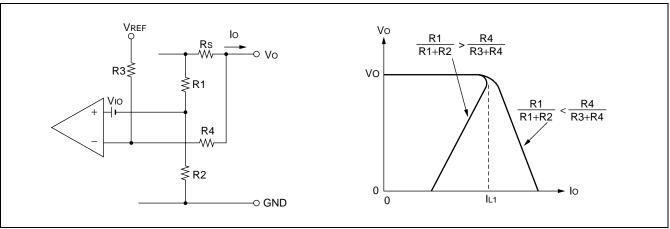
The figure below shows the case when the starter circuit formed by R3, R4, R5, and D is not present. The output current lo after the operation of the current limiting circuit is:

$$Io = \frac{R1}{R1 + R2} \frac{Vo}{Rs} - \frac{Vio}{Rs}$$

When  $V_0 = 0$  such as when the power is turned on, the output current  $I_0 = -V_{10} / R_S$  and, if the offset voltage  $V_{10}$  is positive, the output current is limited to being negative and therefore the output voltage does not rise. Accordingly, if using a fallback system with a detection resistor inserted in the output, always include a starter circuit, expect in the cases described later.



### (2) Example that does not use a diode

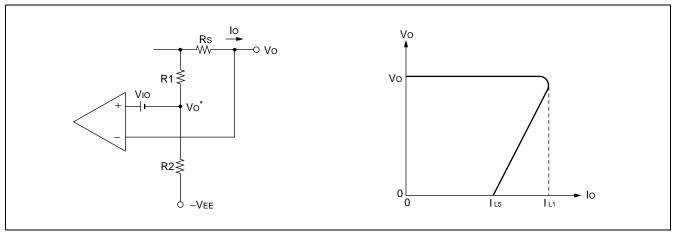


The output current lo after current limiting is:

Io = 
$$\frac{1}{Rs}$$
 [( $\frac{R1}{R1 + R2}$  -  $\frac{R4}{R3 + R4}$ ) Vo +  $\frac{R4}{R3 + R4}$ VREF - Vio ] (R2 >> R1)

In this case, a current flows into the reference voltage source via R3 and R4 if  $V_0 > V_{REF}$ . To maintain the stability of the reference voltage, design the circuit such that this does not exceed 200  $\mu$ A.

# (3) When an external stabilized negative power supply is present



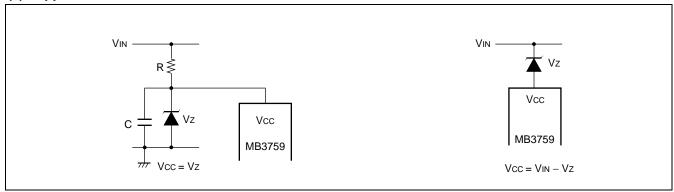
The output current lo after current limiting is:

$$Io = \frac{1}{Rs} \frac{R1}{R1 + R2} (Vo + VEE) - \frac{Vio}{Rs} (R2 >> R1)$$

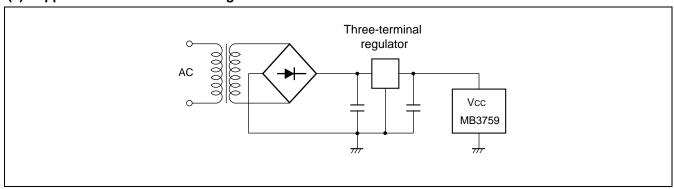
If the output is momentarily shorted,  $V_0^*$  goes briefly negative. In this case, set the voltage across R1 to 300 mV or less to ensure that a voltage of less than -0.3 V is not applied to the op-amp input.

### 5. Example Power Supply Voltage Supply Circuit

### (1) Supplied via a Zener diode



#### (2) Supplied via a three-terminal regulator

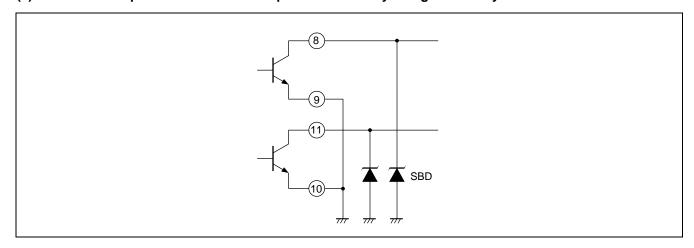


### 6. Example Protection Circuit for Output Transistor

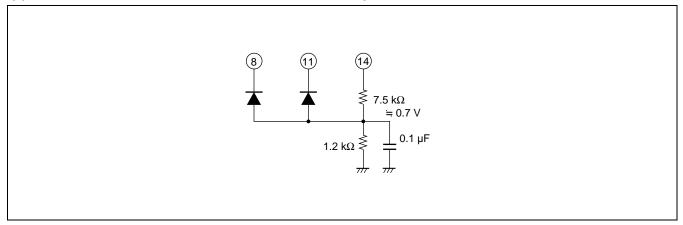
Due to its monolithic IC characteristics, applying a negative voltage greater than the diode voltage ( $\pm$  0.5 V) to the substrate (pin 7) of the MB3759 causes a parasitic effect in the IC which can result in misoperation.

Accordingly, the following measures are required if driving a transformer or similar directly from the output transistor of the IC.

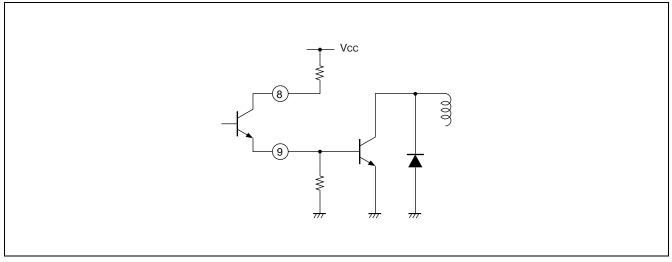
### (1) Protect the output transistor from the parasitic effect by using a Schottky barrier diode.



# (2) Provide a bias at the anode-side of the diode to clamp the low level side of the transistor.

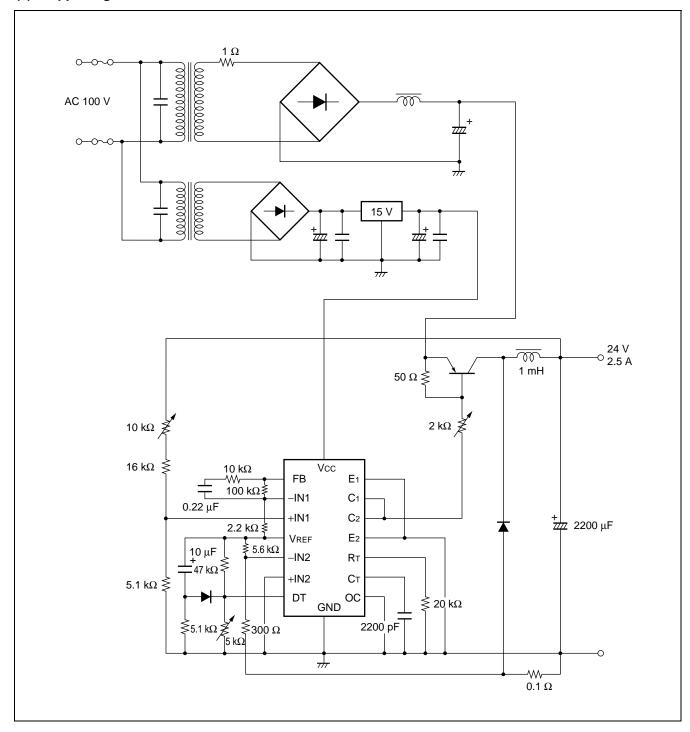


# (3) Drive the transformer via a buffer transistor.

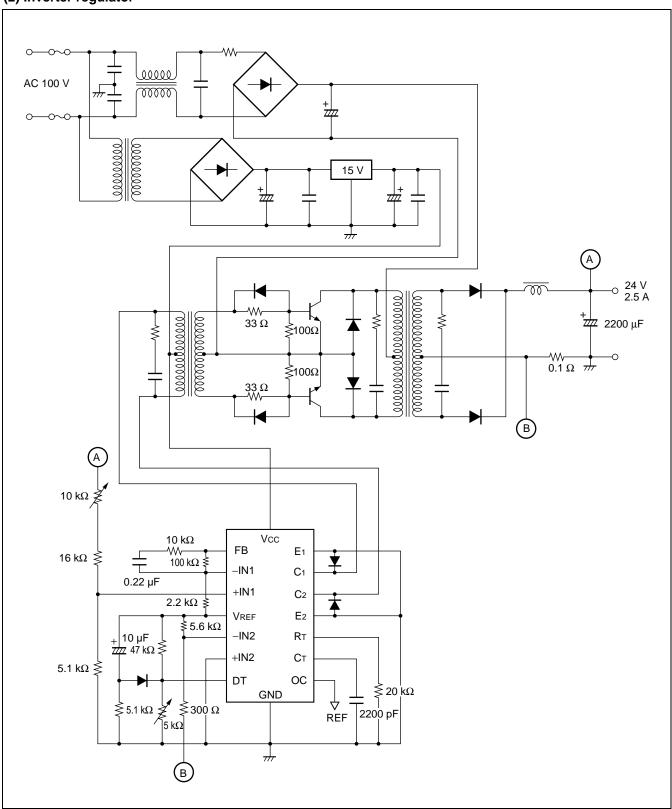


# 7. Typical Application

# (1)Chopper regulator



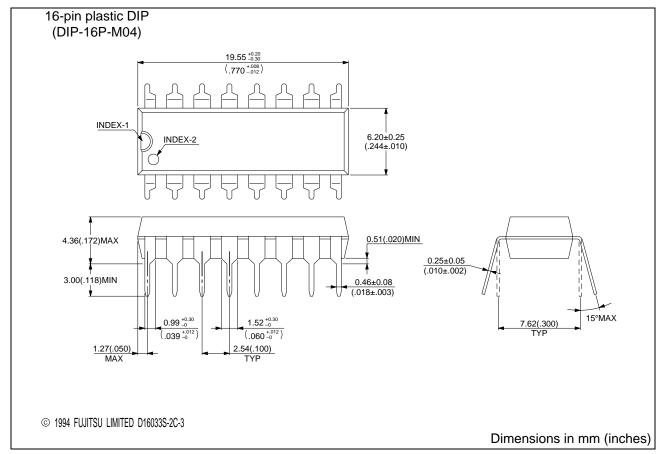
# (2) Inverter regulator

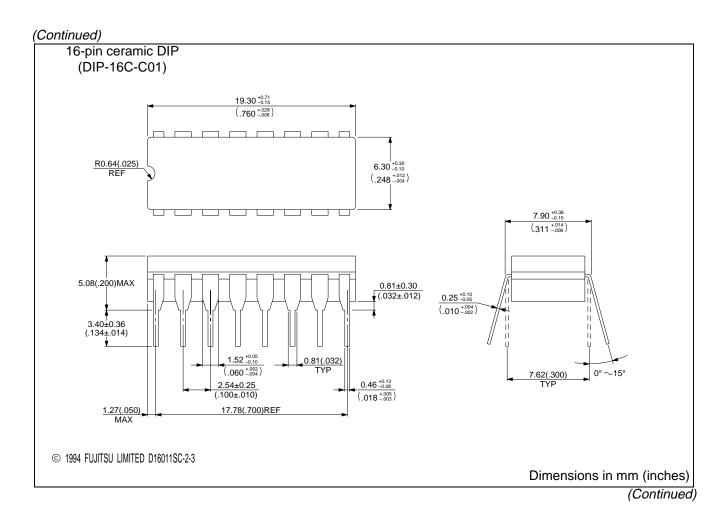


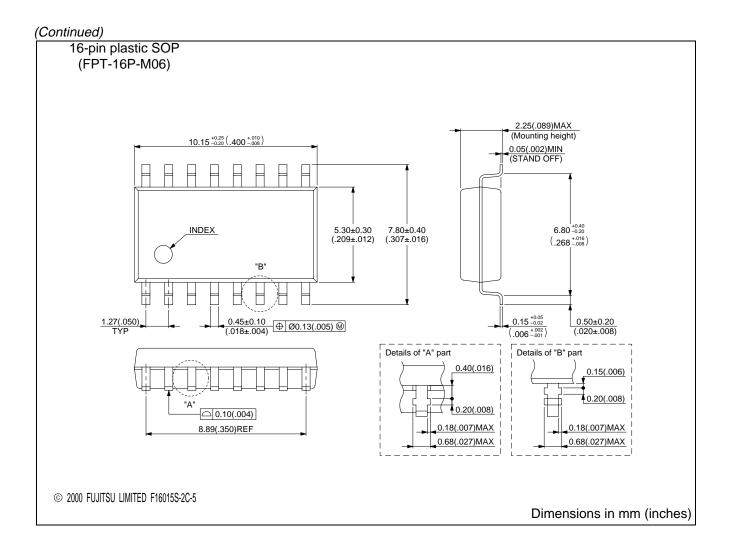
# **■** ORDERING INFORMATION

Part number	Package	Remarks
MB3759P	16-pin plastic DIP (DIP-16P-M04)	
MB3759C	16-pin ceramic DIP (DIP-16C-C01)	
MB3759PF	16-pin plastic SOP (FPT-16P-M06)	

# **■ PACKAGE DIMENSIONS**







# **FUJITSU LIMITED**

For further information please contact:

#### **Japan**

FUJITSU LIMITED Corporate Global Business Support Division Electronic Devices KAWASAKI PLANT, 4-1-1, Kamikodanaka, Nakahara-ku, Kawasaki-shi, Kanagawa 211-8588, Japan Tel: +81-44-754-3763

Fax: +81-44-754-3329

http://www.fujitsu.co.jp/

#### North and South America

FUJITSU MICROELECTRONICS, INC. 3545 North First Street, San Jose, CA 95134-1804, U.S.A.

Tel: +1-408-922-9000 Fax: +1-408-922-9179

Customer Response Center Mon. - Fri.: 7 am - 5 pm (PST)

Tel: +1-800-866-8608 Fax: +1-408-922-9179

http://www.fujitsumicro.com/

#### **Europe**

FUJITSU MICROELECTRONICS EUROPE GmbH Am Siebenstein 6-10,

D-63303 Dreieich-Buchschlag,

Germany

Tel: +49-6103-690-0 Fax: +49-6103-690-122 http://www.fujitsu-fme.com/

#### **Asia Pacific**

FUJITSU MICROELECTRONICS ASIA PTE. LTD. #05-08, 151 Lorong Chuan, New Tech Park, Singapore 556741

Singapore 556741 Tel: +65-281-0770 Fax: +65-281-0220

http://www.fmap.com.sg/

#### Korea

FUJITSU MICROELECTRONICS KOREA LTD. 1702 KOSMO TOWER, 1002 Daechi-Dong, Kangnam-Gu, Seoul 135-280

Korea

Tel: +82-2-3484-7100 Fax: +82-2-3484-7111

F0006

© FUJITSU LIMITED Printed in Japan

All Rights Reserved.

The contents of this document are subject to change without notice. Customers are advised to consult with FUJITSU sales representatives before ordering.

The information and circuit diagrams in this document are presented as examples of semiconductor device applications, and are not intended to be incorporated in devices for actual use. Also, FUJITSU is unable to assume responsibility for infringement of any patent rights or other rights of third parties arising from the use of this information or circuit diagrams.

The contents of this document may not be reproduced or copied without the permission of FUJITSU LIMITED.

FUJITSU semiconductor devices are intended for use in standard applications (computers, office automation and other office equipments, industrial, communications, and measurement equipments, personal or household devices, etc.).

#### CAUTION:

Customers considering the use of our products in special applications where failure or abnormal operation may directly affect human lives or cause physical injury or property damage, or where extremely high levels of reliability are demanded (such as aerospace systems, atomic energy controls, sea floor repeaters, vehicle operating controls, medical devices for life support, etc.) are requested to consult with FUJITSU sales representatives before such use. The company will not be responsible for damages arising from such use without prior approval.

Any semiconductor devices have inherently a certain rate of failure. You must protect against injury, damage or loss from such failures by incorporating safety design measures into your facility and equipment such as redundancy, fire protection, and prevention of over-current levels and other abnormal operating conditions.

If any products described in this document represent goods or technologies subject to certain restrictions on export under the Foreign Exchange and Foreign Trade Control Law of Japan, the prior authorization by Japanese government should be required for export of those products from Japan.