# SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference 

## General Description

The single MAX9015/MAX9016 and dual MAX9017MAX9020 nanopower comparators in space-saving SOT23 packages feature Beyond-the-Rails ${ }^{\text {TM }}$ inputs and are guaranteed to operate down to 1.8 V . The $\mathrm{A}-$ grade packages feature an on-board $1.236 \mathrm{~V} \pm 1 \%$ reference, while the B-grade packages feature a 1.24 V $\pm 1.75 \%$ reference. An ultra-low supply current of $0.85 \mu \mathrm{~A}$ (MAX9019/MAX9020), 1 1 A (MAX9015/MAX9016), or $1.2 \mu \mathrm{~A}(\mathrm{MAX} 9017 / \mathrm{MAX} 9018)$ makes the MAX9015MAX9020 family of comparators ideal for all 2-cell battery monitoring/management applications.
The unique design of the MAX9015-MAX9020 output stage limits supply-current surges while switching, which virtually eliminates the supply glitches typical of many other comparators. This design also minimizes overall power consumption under dynamic conditions. The MAX9015/MAX9017/MAX9019 have a push-pull output stage that sinks and sources current. Large internal output drivers allow Rail-to-Rail ${ }^{\circledR}$ output swing with loads up to 6mA. The MAX9016/MAX9018/MAX9020 have an open-drain output stage that makes them suitable for mixed-voltage system design. All devices are available in the ultra-small 8-pin SOT23 package.
Refer to the MAX9117-MAX9120 data sheet for similar single comparators with or without reference in a tiny SC70 package.

|  |  |
| :--- | :--- |
| 2-Cell Battery | Window Detectors |
| Monitoring/Management | Sensing at Ground or |
| Ultra-Low Power Systems | Supply Line |
| Mobile Communications | Telemetry and Remote |
| Notebooks and PDAs | Systems |
| Threshold Detectors/ | Medical Instruments |
| Discriminators |  |

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- Ultra-Low Total Supply Current $0.85 \mu \mathrm{~A}$ (MAX9019/MAX9020) $1.0 \mu \mathrm{~A}$ (MAX9015A/MAX9016A) $1.2 \mu \mathrm{~A}$ (MAX9017/MAX9018)
}
- Guaranteed Operation Down to 1.8 V
- Precision Vos < 5mV (max)
- Internal $1.236 \mathrm{~V} \pm 1 \%$ Reference (A Grade)
- Input Voltage Range Extends 200mV Beyond-the-Rails
- CMOS Push-Pull Output with $\pm 6 m A$ Drive Capability (MAX9015/MAX9017/MAX9019)
- Open-Drain Output Versions Available (MAX9016/MAX9018/MAX9020)
- Crowbar-Current-Free Switching
- Internal 4mV Hysteresis for Clean Switching
- No Phase Reversal for Overdriven Inputs
- Dual Versions in Space-Saving 8-Pin SOT23 Package

Ordering Information

| PART | TEMP RANGE | PIN- <br> PACKAGE | TOP <br> MARK |
| :---: | :---: | :---: | :---: |
| MAX9015AEKA-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIW |
| MAX9016AEKAA-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIX |
| MAX9017AEKA-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIQ |
| MAX9017BEKA-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIS |

Ordering Information continued at end of data sheet.
Pin Configurations appear at end of data sheet.
Beyond-the-Rails is a trademark of Maxim Integrated Products, Inc. Rail-to-Rail is a registered trademark of Nippon Motorola, Ltd.

Selector Guide

| PART | COMPARATOR(S) | INTERNAL REFERENCE (V) | OUTPUT TYPE | SUPPLY CURRENT $(\boldsymbol{\mu} \mathbf{A})$ |
| :---: | :---: | :---: | :---: | :---: |
| MAX9015A | 1 | $1.236 \pm 1 \%$ | Push-pull | 1 |
| MAX9016A | 1 | $1.236 \pm 1 \%$ | Open drain | 1 |
| MAX9017A | 2 | $1.236 \pm 1 \%$ | Push-pull | 1.2 |
| MAX9017B | 2 | $1.240 \pm 1.75 \%$ | Push-pull | 1.2 |
| MAX9018A | 2 | $1.236 \pm 1 \%$ | Open drain | 1.2 |
| MAX9018B | 2 | $1.240 \pm 1.75 \%$ | Open drain | 1.2 |
| MAX9019 | 2 | - | Push-pull | 0.85 |
| MAX9020 | 2 | - | Open drain | 0.85 |

## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference

ABSOLUTE MAXIMUM RATINGS<br>Supply Voltage (VCC to $\mathrm{VEE}_{\mathrm{E}}$ ).<br>$\qquad$<br>$\qquad$ IN+, IN-, INA+, INB+, INA-, INB-, REF/INA-, REF<br>$\qquad$<br>.......................(VEE $-0.3 \mathrm{~V})$ to ( $\mathrm{VCC}+0.3 \mathrm{~V}$ )<br>Output Voltage (OUT_)<br>MAX9015A, MAX9017_, MAX9019....(VEE - 0.3V) to (VCC + 0.3V) MAX9016A, MAX9018_, MAX9020.<br>$\qquad$<br>..(VEE - 0.3 V ) to +6 V<br>Output Current (REF, OUT_, REF/INA-).<br>$\qquad$<br>$\qquad$ .$\pm 50 \mathrm{~mA}$

Output Short-Circuit Duration (REF, OUT_, REF/INA-) ...........10s Continuous Power Dissipation ( $\mathrm{T}_{\mathrm{A}}=+70^{\circ} \mathrm{C}$ )

8-Pin SOT23 (derate $9.1 \mathrm{~mW} /{ }^{\circ} \mathrm{C}$ above $+70^{\circ} \mathrm{C}$ )............ 727 mW Operating Temperature Range ........................... $40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ Storage Temperature Range ............................ $65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ Junction Temperature . .$+150^{\circ} \mathrm{C}$
Lead Temperature (soldering, 10s) ........................................... $+300^{\circ} \mathrm{C}$

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ELECTRICAL CHARACTERISTICS-MAX9015-MAX9018 (Single and Duals with REF)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=0 \mathrm{~V}, \mathrm{~V}_{\mathrm{IN}}-=\mathrm{V}_{\mathrm{REF}}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 1)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supply Voltage Range | VCC | Inferred from the PSRR test |  | 1.8 |  | 5.5 | V |
| Supply Current | Icc | MAX9015A/ MAX9016A | $V_{C C}=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | $\begin{array}{ll}1.0 & 1.5 \\ 1.1 & 1.7 \\ & 2.0\end{array}$ |  |  | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  |  |  |
|  |  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \\ & \mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\text {MIN }} \text { to } \mathrm{T}_{\text {MAX }} \end{aligned}$ |  |  |  |  |
|  |  | MAX9017」 MAX9018_ | $\mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 1.2 | 1.9 |  |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 1.4 | 2.3 |  |
|  |  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \\ & \mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\text {MIN }} \text { to } \mathrm{T}_{\text {MAX }} \end{aligned}$ |  |  | 2.8 |  |
| Input Common-Mode <br> Voltage Range <br> (MAX9015A/MAX9016A) | $V_{C M}$ | Inferred from the out $V_{E E}-0.2 V<V_{C M}<1$ | put swing test, $/ C c+0.2 \mathrm{~V}$ | Vee - 0.2 |  | $V_{C C}+0.2$ | V |
| IN+ Voltage Range (MAX9017_/MAX9018_) | VIN+ | Inferred from the out | ut swing test | VEe - 0.2 |  | $V_{C C}+0.2$ | V |
|  |  | $V_{\text {EE }}-0.2 \mathrm{~V}<\mathrm{V}_{\text {cm }}<$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 0.15 | 5 |  |
| Input Ofset Voltage | Vos | $\mathrm{V}_{\mathrm{CC}}+0.2 \mathrm{~V}(\text { Note 2) }$ | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 10 |  |
| Input-Referred Hysteresis | $\mathrm{V}_{\mathrm{HB}}$ | $\mathrm{V}_{\text {EE }}-0.2 \mathrm{~V}<\mathrm{V}_{\text {CM }}<\mathrm{V}^{\prime}$ | CC + 0.2V (Note 3) |  | 4 |  | mV |
| Input Bias Current (IN+, |  | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  |  | $\pm 0.15$ | $\pm 1$ |  |
| IN-, INA+, INB+, INB-) |  | $\mathrm{T}_{\mathrm{A}}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  |  | $\pm 2$ |  |
| Power-Supply Rejection Ratio | PSRR | $\mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ to 5.5 V |  |  | 0.1 | 1 | mV/V |
|  |  | $\mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$, | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 100 | 200 |  |
| Output Voltage Swing High |  | ISOURCE $=1 \mathrm{~mA}$ | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 300 |  |
| (MAX9015A/MAX9017_) |  | $\mathrm{V}_{C C}=5.0 \mathrm{~V}$, | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 250 | 350 |  |
|  |  | ISOURCE $=6 \mathrm{~mA}$ | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 450 |  |
|  |  | $\mathrm{V}_{\text {CC }}=1.8 \mathrm{~V}$, | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 105 | 200 |  |
| Output Voltage Swing Low |  | $\mathrm{ISINK}=1 \mathrm{~mA}$ | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 300 | mV |
| (MAX9015A/MAX9017_) |  | $\mathrm{V}_{\text {CC }}=5.0 \mathrm{~V}$, | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 285 | 350 |  |
|  |  | $\mathrm{ISINK}=6 \mathrm{~mA}$ | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 450 |  |

# SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference 

## ELECTRICAL CHARACTERISTICS—MAX9015-MAX9018 (Single and Duals with REF) (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=0 \mathrm{~V}, \mathrm{VIN}-=\mathrm{V}_{\text {REF }}, \mathrm{T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 1)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN | TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Output Leakage Current (MAX9016A/MAX9018_) | ILEAK | $\mathrm{V}_{\text {CC }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=5.5 \mathrm{~V}$ |  |  | 0.001 | 1 | $\mu \mathrm{A}$ |
| Output Short-Circuit Current | ISC | Sourcing, VOUT = VEE (MAX9015A/ MAX9017_ only) | $V_{C C}=1.8 \mathrm{~V}$ |  | 3 |  | mA |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ |  | 35 |  |  |
|  |  | Sinking, <br> Vout $=\mathrm{V}_{\text {CC }}$ | $\mathrm{V}_{C C}=1.8 \mathrm{~V}$ |  | 3 |  |  |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ |  | 33 |  |  |
| High-to-Low Propagation Delay (Note 4) | tpD- | $\mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ |  |  | 7 |  | $\mu \mathrm{s}$ |
|  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ |  |  | 6 |  |  |
| Low-to-High Propagation Delay (Note 4) | tpD+ | $V_{C C}=1.8 \mathrm{~V}$ | MAX9015A/MAX9017_ |  | 11 |  | $\mu \mathrm{s}$ |
|  |  |  | MAX9016A/MAX9018_, <br> RPULLUP $=100 \mathrm{k} \Omega$ to $\mathrm{V}_{\mathrm{CC}}$ |  | 12 |  |  |
|  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ | MAX9015A/MAX9017_ |  | 28 |  |  |
|  |  |  | MAX9016A/MAX9018_, <br> RPULLUP $=100 \mathrm{k} \Omega$ to $\mathrm{V}_{\mathrm{CC}}$ |  | 31 |  |  |
| Rise Time | trise | $C_{L}=15 p F$ (MAX9015A/MAX9017_) |  |  | 1.6 |  | $\mu \mathrm{s}$ |
| Fall Time | tFALL | $C_{L}=15 \mathrm{pF}$ |  |  | 0.2 |  | $\mu \mathrm{s}$ |
| Power-Up Time | ton |  |  |  | 1.2 |  | ms |
| Reference Voltage | VREF | MAX901_A | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, 1.0 \%$ | 1.224 | 1.236 | 1.248 | V |
|  |  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$, $2.5 \%$ | 1.205 |  | 1.267 |  |
|  |  | MAX901_B | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}, 1.75 \%$ | 1.218 | 1.240 | 1.262 |  |
|  |  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}, 4.5 \%$ | 1.184 |  | 1.296 |  |
| Reference Voltage Temperature Coefficient | TCref |  |  |  | 40 |  | ppm $/{ }^{\circ} \mathrm{C}$ |
| Reference Output Voltage Noise | EN | $B W=10 \mathrm{~Hz}$ to $1 \mathrm{kHz}, \mathrm{CREF}=1 \mathrm{nF}$ |  |  | 29 |  | $\mu \mathrm{V}_{\text {RMS }}$ |
|  |  | $\mathrm{BW}=10 \mathrm{~Hz}$ to 6 kHz , CREF $=1 \mathrm{nF}$ |  |  | 60 |  |  |
| Reference Line Regulation | $\Delta V_{\text {REF }} /$ <br> $\Delta V_{C C}$ | $1.8 \mathrm{~V} \leq \mathrm{V}_{\mathrm{CC}} \leq 5.5 \mathrm{~V}$ |  |  | 0.5 |  | mV/V |
| Reference Load Regulation | $\Delta V_{\text {REF }} /$ <br> $\Delta$ IOUT | Iout $=0$ to 100nA |  |  | 0.03 |  | $\mathrm{mV} / \mathrm{nA}$ |

# SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference 

ELECTRICAL CHARACTERISTICS—MAX9019/MAX9020 (Duals without REF)
$\left(V_{C C}=5 \mathrm{~V}, \mathrm{~V}_{E E}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) ( Note 1)

| PARAMETER | SYMBOL | CONDITIONS |  | MIN TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supply Voltage Range | VCC | Inferred from the PSRR test |  | 1.8 | 5.5 | V |
| Supply Current | IcC | $\begin{aligned} & \text { MAX9019/ } \\ & \text { MAX9020 } \end{aligned}$ | $\mathrm{V}_{C C}=1.8 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 0.85 | 1.50 | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 1.1 | 1.70 |  |
|  |  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \\ & \mathrm{~T}_{\mathrm{A}}=\mathrm{T}_{\text {MIN }} \text { to } \mathrm{T}_{\text {MAX }} \end{aligned}$ |  | 2.0 |  |
| Input Common-Mode Voltage Range | $V_{\text {CM }}$ | Inferred from the output swing test,$V_{E E}-0.2 \mathrm{~V}<\mathrm{V}_{\mathrm{CM}}<\mathrm{V}_{\mathrm{CC}}+0.2 \mathrm{~V}$ |  | Vee - 0.2 | $V_{C C}+0.2$ | V |
| Input Offset Voltage | Vos | $\begin{aligned} & \mathrm{V}_{\mathrm{EE}}-0.2 \mathrm{~V}<\mathrm{V}_{\mathrm{CM}}< \\ & \mathrm{V}_{\mathrm{CC}}+0.2 \mathrm{~V} \text { (Note 2) } \end{aligned}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 1 | 5 | mV |
|  |  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 10 |  |
| Input-Referred Hysteresis | VHB | $\mathrm{V}_{\text {EE }}-0.2 \mathrm{~V}<\mathrm{V}_{\text {CM }}<\mathrm{V}_{\text {CC }}+0.2 \mathrm{~V}$ (Note 3) |  | 4 |  | mV |
| Input Bias Current (INA-, INA+, INB+, INB-) | IB | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ |  | 0.15 | 1 | nA |
|  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  |  | 2 |  |
| Power-Supply Rejection Ratio | PSRR | $\mathrm{V}_{\mathrm{CC}}=1.8 \mathrm{~V}$ to 5.5 V |  | 0.1 | 1 | $\mathrm{mV} / \mathrm{V}$ |
| Output Voltage Swing High (MAX9019 Only) | VCC $-\mathrm{V}_{\text {OH }}$ | $\begin{aligned} & \mathrm{V} \mathrm{VC}=1.8 \mathrm{~V}, \\ & \mathrm{ISOURCE}=1 \mathrm{~mA} \end{aligned}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 55 | 200 | mV |
|  |  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 300 |  |
|  |  | $\begin{aligned} & \text { VCC }=5.0 \mathrm{~V}, \\ & \text { ISOURCE }=6 \mathrm{~mA} \end{aligned}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 190 | 350 |  |
|  |  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 450 |  |
| Output Voltage Swing Low | Vol | $\begin{array}{\|l\|} \hline V_{C C}=1.8 \mathrm{~V}, \\ \mathrm{ISINK}^{2}=1 \mathrm{~mA} \end{array}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 55 | 200 | mV |
|  |  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 300 |  |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}, \\ & \mathrm{I}_{\mathrm{SINK}}=6 \mathrm{~mA} \end{aligned}$ | $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$ | 190 | 350 |  |
|  |  |  | $\mathrm{T}_{\text {A }}=\mathrm{T}_{\text {MIN }}$ to $\mathrm{T}_{\text {MAX }}$ |  | 450 |  |
| Output Leakage Current (MAX9020 Only) | ILEAK | $\mathrm{V}_{\text {CC }}=5.5 \mathrm{~V}, \mathrm{~V}_{\text {OUT }}=5$ |  | 0.001 | 1 | $\mu \mathrm{A}$ |
| Output Short-Circuit Current | IsC | Sourcing, VOUT = VEE (MAX9019 only) | $V_{C C}=1.8 \mathrm{~V}$ | 3 |  | mA |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ | 35 |  |  |
|  |  | Sinking, VOUT $=\mathrm{V}_{\text {CC }}$ | $\mathrm{V}_{C C}=1.8 \mathrm{~V}$ | 3 |  |  |
|  |  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ | 33 |  |  |
| High-to-Low Propagation Delay (Note 4) | tpD- | $\mathrm{V}_{C C}=1.8 \mathrm{~V}$ |  | 7 |  | $\mu \mathrm{s}$ |
|  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ |  | 6 |  |  |
| Low-to-High Propagation Delay (Note 4) | tPD+ | $V_{C C}=1.8 \mathrm{~V}$ | MAX9019 | 11 |  | $\mu \mathrm{s}$ |
|  |  |  | MAX9020, RPULLUP = $100 \mathrm{k} \Omega$ to $\mathrm{V}_{\mathrm{CC}}$ | 12 |  |  |
|  |  | $\mathrm{V}_{\mathrm{CC}}=5.0 \mathrm{~V}$ | MAX9019 | 28 |  |  |
|  |  |  | MAX9020, RpulLup = $100 \mathrm{k} \Omega$ to $\mathrm{V}_{\mathrm{CC}}$ | 31 |  |  |

# SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference 

## ELECTRICAL CHARACTERISTICS—MAX9019/MAX9020 (Duals without REF) (continued)

$\left(\mathrm{V}_{C C}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=0 \mathrm{~V}, \mathrm{~T}_{\mathrm{A}}=-40^{\circ} \mathrm{C}\right.$ to $+85^{\circ} \mathrm{C}$, unless otherwise noted. Typical values are at $\mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$.) (Note 1)

| PARAMETER | SYMBOL | CONDITIONS | MIN TYP | MAX | UNITS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rise Time | trise | $C_{L}=15 \mathrm{pF}$ (MAX9019 only) | 1.6 |  | us |
| Fall Time | tFALL | $C \mathrm{~L}=15 \mathrm{pF}$ | 0.2 |  | $\mu \mathrm{s}$ |
| Power-Up Time | ton |  | 1.2 |  | ms |

Note 1: All devices are $100 \%$ tested at $T_{A}=+25^{\circ} \mathrm{C}$. Specifications over temperature ( $T_{A}=T_{\text {MIN }}$ to $T_{M A X}$ ) are guaranteed by design, not production tested.
Note 2: VOS is defined as the center of the hysteresis band at the input.
Note 3: The hysteresis-related trip points are defined as the edges of the hysteresis band, measured with respect to the center of the band (i.e., VOS) (Figure 1).
Note 4: Specified with an input overdrive (VOVERDRIVE) of 100 mV , and a load capacitance of $C L=15 \mathrm{pF}$. Voverdrive is defined above and beyond the offset voltage and hysteresis of the comparator input.

## Typical Operating Characteristics

$\left(V_{C C}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=0 \mathrm{~V}, \mathrm{CL}_{\mathrm{L}}=15 \mathrm{pF}\right.$, VOVERDRIVE $=100 \mathrm{mV}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}$, unless otherwise noted. $)$


## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference

## Typical Operating Characteristics (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=0 \mathrm{~V}, \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF}, \mathrm{V}_{\text {OVERDRIVE }}=100 \mathrm{mV}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted. $)$


## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference

## Typical Operating Characteristics (continued)

$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=\mathrm{OV}, \mathrm{CL}=15 \mathrm{pF}, \mathrm{V}_{\mathrm{OVERDRIVE}}=100 \mathrm{mV}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted. $)$



REFERENCE VOLTAGE
vs. REFERENCE SOURCE CURRENT



REFERENCE VOLTAGE
vs. TEMPERATURE


REFERENCE VOLTAGE
vs. REFERENCE SINK CURRENT


REFERENCE VOLTAGE DISTRIBUTION


REFERENCE VOLTAGE
vs. SUPPLY VOLTAGE


REFERENCE VOLTAGE vs. REFERENCE SINK CURRENT AND TEMPERATURE


## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference



PROPAGATION DELAY (tpd.) vs. CAPACITIVE LOAD


PROPAGATION DELAY (tpD + )
vs. INPUT OVERDRIVE


Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=0 \mathrm{~V}, \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF}, \mathrm{V}_{\text {OVERDRIVE }}=100 \mathrm{mV}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted. $)$

PROPAGATION DELAY (tpd-)
vs. TEMPERATURE


PROPAGATION DELAY (tpd+) vs. CAPACITIVE LOAD


PROPAGATION DELAY (tpd-)


PROPAGATION DELAY (tpd + ) vs. TEMPERATURE


PROPAGATION DELAY (tpd-) vs. INPUT OVERDRIVE


PROPAGATION DELAY (tpd + ) vs. PULLUP RESISTANCE


## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference

Typical Operating Characteristics (continued)
$\left(\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}, \mathrm{~V}_{\mathrm{EE}}=0 \mathrm{~V}, \mathrm{C}_{\mathrm{L}}=15 \mathrm{pF}, \mathrm{V}_{\text {OVERDRIVE }}=100 \mathrm{mV}, \mathrm{T}_{\mathrm{A}}=+25^{\circ} \mathrm{C}\right.$, unless otherwise noted. $)$

$10 \mu \mathrm{~s} / \mathrm{div}$

$2 \mu \mathrm{~s} / \mathrm{div}$



$2 \mu \mathrm{~s} / \mathrm{div}$


$10 \mu s / d i v$


20 $\mu \mathrm{s} / \mathrm{div}$

## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference

| PIN |  |  | NAME |  |
| :---: | :---: | :---: | :---: | :--- |
| MAX9015/ <br> MAX9016 | MAX9017/ <br> MAX9018 | MAX9019/ <br> MAX9020 |  |  |
| 1 | - | - | REF | 1.24V Reference Output |
| 2 | - | - | IN- | Comparator Inverting Input |
| 3 | - | - | IN+ | Comparator Noninverting Input |
| 4 | 4 | 4 | VEE | Negative Supply Voltage |
| 5,8 | - | - | N.C. | No Connection. Not internally connected. |
| 6 | - | - | OUT | Comparator Output |
| 7 | 8 | 8 | VCC | Positive Supply Voltage |
| - | 1 | 1 | OUTA | Comparator A Output |
| - | 3 | 3 | INA+ | Comparator A Noninverting Input |
| - | 5 | 5 | INB+ | Comparator B Noninverting Input |
| - | 6 | 6 | INB- | Comparator B Inverting Input |
| - | 7 | 7 | OUTB | Comparator B Output |
| - | - | 2 | INA- | Comparator A Inverting Input |
| - | 2 | - | REF/ <br> INA- | 1.24V Reference Output. Internally connected to the inverting input of <br> comparator A (MAX9017/MAX9018 only). |



# SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference 

## Detailed Description

The MAX9015-MAX9018 feature an on-board 1.24 V $\pm 0.5 \%$ ( $\pm 1.45 \%$ for the B grade) reference, yet draw an ultra-low supply current. The MAX9019/MAX9020 (duals without reference) consume just 850nA of supply current. All devices are guaranteed to operate down to 1.8 V supply. Their common-mode input voltage range extends 200 mV beyond-the-rails. An internal 4 mV hysteresis ensures clean output switching, even with slowmoving input signals. Large internal output drivers swing rail-to-rail with up to $\pm 6 \mathrm{~mA}$ loads (MAX9015/ MAX9017/MAX9019).
The output stage employs a unique design that minimizes supply-current surges while switching, which virtually eliminates the supply glitches typical of many other comparators. The MAX9015/MAX9017/MAX9019 have a push-pull output stage that sinks as well as sources current. The MAX9016/MAX9018/MAX9020 have an open-drain output stage that can be pulled beyond VCC up to 5.5 V above VEE. These open-drain versions are ideal for implementing wire-ORed output logic functions.

## Input Stage Circuitry

The input common-mode voltage ranges extend from VEE -0.2 V to $\mathrm{VCC}+0.2 \mathrm{~V}$. These comparators operate at any differential input voltage within these limits. Input bias current is typically $\pm 150 \mathrm{pA}$ at the trip point, if the input voltage is between the supply rails. Comparator inputs are protected from overvoltage by internal ESD protection diodes connected to the supply rails. As the input voltage exceeds the supply rails, these ESD protection diodes become forward biased and begin to conduct increasing input bias current (see the Input Bias Current vs. Input Bias Voltage graph in the Typical Operating Characteristics).

## Output Stage Circuitry

The MAX9015-MAX9020 feature a unique break-before-make output stage capable of driving $\pm 8 \mathrm{~mA}$ loads rail-to-rail. Many comparators consume orders of magnitude more current during switching than during steady-state operation. However, with the MAX9015MAX9020 family of comparators, the supply-current change during an output transition is extremely small. In the Typical Operating Characteristics, the Supply Current vs. Output Transition Frequency graphs show the minimal supply-current increase as the output switching frequency approaches 1 kHz . This characteristic reduces the need for power-supply filter capacitors to reduce glitches created by comparator switching currents. In battery-powered applications, this characteristic results in a substantial increase in battery life.

Reference (MAX9015-MAX9018) The MAX9015-MAX9018s' internal +1.24V reference has a typical temperature coefficient of $40 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$ over the full $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ temperature range. The reference is a very-low-power bandgap cell, with a typical $35 \mathrm{k} \Omega$ output impedance. REF can source and sink up to 100 nA to external circuitry. For applications needing increased drive, buffer REF with a low input-bias current op amp such as the MAX4162. Most applications require no REF bypass capacitor. For noisy environments or fast transients, connect a 1 nF to 10nF ceramic capacitor from REF to GND.

## Applications Information

## Low-Voltage, Low-Power Operation

The MAX9015-MAX9020 are ideally suited for use with most battery-powered systems. Table 1 lists a variety of battery types, capacities, and approximate operating times for the MAX9015-MAX9020, assuming nominal conditions.

## Table 1. Battery Applications Using the MAX9015-MAX9020

| BATTERY <br> TYPE | RECHARGEABLE | VRESH <br> (V) | VEND-OF- <br> LIFE (V) | CAPACITY, <br> AA SIZE <br> (mA-hr) | MAX9015A/ <br> MAX9016A | MAX9017/ <br> OPERATING <br> TIME (hr) | MAX9018 <br> OPERATING <br> TIME (hr) |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Alkaline (2 cells) | No | 3.0 | 1.8 | 2000 | 2000 k | 1540 k | MAX9019/ <br> OPERATING <br> TIME (hr) |
| Nickel-cadmium <br> (2 cells) | Yes | 2.4 | 1.8 | 750 | 750 k | 570 k | 500 k |
| Nickel-metal-hydride <br> $(2$ cells) $)$ | Yes | 2.4 | 1.8 | 1000 | 1000 k | 770 k | 660 k |
| Lithium-ion (1 cell) | Yes | 3.6 | 2.9 | 1000 | 1000 k | 770 k | 660 k |

# SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference 

## Internal Hysteresis

Many comparators oscillate in the linear region of operation because of noise or undesired parasitic feedback. Oscillations can occur when the voltage on one input is equal or very close to the voltage on the other input. The MAX9015-MAX9020 have internal 4 mV hysteresis to counter parasitic effects and noise.
The hysteresis in a comparator creates two trip points: one for the rising input voltage ( $\mathrm{V}_{\text {THR }}$ ) and one for the falling input voltage (VTHF) (Figure 1). The difference between the trip points is the hysteresis (VhB). When the comparator's input voltages are equal, the hysteresis effectively causes one comparator input to move quickly past the other, thus taking the input out of the region where oscillation occurs. Figure 1 illustrates the case in which the comparator's inverting input has a fixed voltage applied, and the noninverting input is varied. If the inputs were reversed, the figure would be the same, except with an inverted output.

## Additional Hysteresis (MAX9015/MAX9017/MAX9019) (Push-Pull Outputs)

 The MAX9015/MAX9017/MAX9019 feature a built-in 4 mV hysteresis band (VHB). Additional hysteresis can be generated with three resistors using positive feedback (Figure 2). Use the following procedure to calculate resistor values:1) Select R3. Input bias current at $I_{N_{-}}+$is less than 2nA, so the current through R3 should be at least $0.2 \mu \mathrm{~A}$ to minimize errors caused by input bias current. The current through R3 at the trip point is (VREF - VOUT)/R3. Considering the two possible output states in solving for R3 yields two formulas: R3 $=\mathrm{V}_{\text {REF }} / I R 3$ or $\mathrm{R} 3=\left(\mathrm{V}_{\mathrm{CC}}-\mathrm{V}_{\mathrm{REF}}\right) / \mathrm{I}_{\text {R3 }}$. Use the smaller of the two resulting resistor values. For example, when using the MAX9017 (VREF $=1.24 \mathrm{~V})$ and $\mathrm{VCC}_{\mathrm{C}}$ $=5 \mathrm{~V}$, and if we choose $\mathrm{IR} 3=0.2 \mu \mathrm{~A}$, then the two resistor values are $6.2 \mathrm{M} \Omega$ and $19 \mathrm{M} \Omega$. Choose a $6.2 \mathrm{M} \Omega$ standard value for R3.
2) Choose the hysteresis band required (VHB). For this example, choose 50 mV .
3) Calculate R1 according to the following equation:

$$
\mathrm{R} 1=\mathrm{R} 3\left(\frac{\mathrm{~V}_{\mathrm{HB}}}{\mathrm{~V}_{\mathrm{CC}}}\right)
$$

For this example, insert the values:

$$
\mathrm{R} 1=6.2 \mathrm{M} \Omega\left(\frac{50 \mathrm{mV}}{5 \mathrm{~V}}\right)=12 \mathrm{k} \Omega
$$



Figure 1. Threshold Hysteresis Band


Figure 2. MAX9015/MAX9017/MAX9019 Additional Hysteresis
4) Choose the trip point for $V_{I N}$ rising ( $V_{T H R}$ ) such that:

$$
\mathrm{V}_{\mathrm{THR}}>\mathrm{V}_{\mathrm{REF}}\left(1+\frac{\mathrm{V}_{\mathrm{HB}}}{\mathrm{~V}_{\mathrm{CC}}}\right)
$$

where $V_{\text {THR }}$ is the trip point for $V_{I N}$ rising. This is the threshold voltage at which the comparator switches its output from low to high as VIN rises above the trip point. For this example, choose 3V.
5) Calculate R2 as follows:

$$
\mathrm{R} 2=\frac{1}{\left[\left(\frac{V_{T H R}}{V_{R E F} \times R 1}\right)-\left(\frac{1}{R 1}\right)-\left(\frac{1}{R 3}\right)\right]}
$$



For this example, choose a $44.2 \mathrm{k} \Omega$ standard value.

# SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference 

6) Verify the trip voltages and hysteresis as follows:

VIN rising: $=2.992 \mathrm{~V}$, which is equivalent to REF times R1 divided by the parallel combination of R1, R2:

$$
\mathrm{V}_{\mathrm{THR}}=\mathrm{V}_{\mathrm{REF}} \times \mathrm{R} 1\left[\left(\frac{1}{\mathrm{R} 1}\right)+\left(\frac{1}{\mathrm{R} 2}\right)+\left(\frac{1}{\mathrm{R} 3}\right)\right]
$$

and R3.
VIN falling: $=2.942 \mathrm{~V}$ :

$$
\mathrm{V}_{\mathrm{THF}}=\mathrm{V}_{\mathrm{THR}}-\left(\frac{\mathrm{R} 1 \times \mathrm{V}_{\mathrm{CC}}}{\mathrm{R} 3}\right)
$$

Hysteresis $=$ VTHR - VTHF $=50 \mathrm{mV}$.

## Additional Hysteresis (MAX9016/MAX9018/MAX9020) (Open-Drain Outputs)

The MAX9016/MAX9018/MAX9020 feature a built-in 4mV hysteresis band. These devices have open-drain outputs and require an external pullup resistor (Figure 3). Additional hysteresis can be generated using positive feedback, but the formulas differ slightly from those of the MAX9015/MAX9017/MAX9019. Use the following procedure to calculate resistor values:

1) Select R3. Input bias current at $I_{-}+$is less than $2 n A$, so the current through R3 should be at least $0.2 \mu \mathrm{~A}$ to minimize errors caused by input bias current. The current through R3 at the trip point is (VREF - VOUT)/R3. Considering the two possible output states in solving for R3 yields two formulas: R3 $=V_{\text {REF }} / I_{R 3}$ or R3 $=\left[\left(V_{C C}-V_{\text {REF }}\right) / I_{R 3}\right]$ - R4. Use the smaller of the two resulting resistor values. For example, when using the MAX9018 (VREF $=1.24 \mathrm{~V})$ and $\mathrm{V}_{\mathrm{CC}}=5 \mathrm{~V}$, and if we choose $\mathrm{I}_{\mathrm{R} 3}=0.2 \mu \mathrm{~A}$, and $R 4=1 \mathrm{M} \Omega$, then the two resistor values are $6.2 \mathrm{M} \Omega$ and $18 \mathrm{M} \Omega$. Choose a $6.2 \mathrm{M} \Omega$ standard value for R3.
2) Choose the hysteresis band required ( $\mathrm{V}_{\mathrm{HB}}$ ).
3) Calculate R1 according to the following equation. For this example, insert the values:

$$
\begin{gathered}
\mathrm{R} 1=(\mathrm{R} 3+\mathrm{R} 4)\left(\frac{V_{H B}}{V_{C C}}\right) \\
\mathrm{R} 1=(6.2 \mathrm{M} \Omega+1 \mathrm{M} \Omega)\left(\frac{50 \mathrm{mV}}{5 \mathrm{~V}}\right)=72 \mathrm{k} \Omega
\end{gathered}
$$

4) Choose the trip point for $V_{I N}$ rising $\left(V_{T H R}\right)$ such that:

$$
\mathrm{V}_{\mathrm{THR}}>\mathrm{V}_{\mathrm{REF}}\left(1+\frac{\mathrm{V}_{\mathrm{HB}}}{\mathrm{~V}_{\mathrm{CC}}}\right)
$$

( $V_{\text {THR }}$ is the trip point for $V_{\text {IN }}$ rising). This is the threshold voltage at which the comparator switches its output from low to high as VIN rises above the trip point. For this example, choose 3V:
5) Calculate R2 as follows:

$$
R 2=\frac{1}{\left[\left(\frac{V_{T H R}}{V_{R E F} \times R 1}\right)-\left(\frac{1}{R 1}\right)-\left(\frac{1}{R 3}\right)\right]}
$$

$\mathrm{R} 2=\frac{1}{\left[\left(\frac{3.0 \mathrm{~V}}{1.24 \mathrm{~V} \times 72 \mathrm{k} \Omega}\right)-\left(\frac{1}{72 \mathrm{k} \Omega}\right)-\left(\frac{1}{6.2 \mathrm{M} \Omega}\right)\right]}=51.1 \mathrm{k} \Omega$
For this example, choose a $49.9 \mathrm{k} \Omega$ standard value.
6) Verify the trip voltages and hysteresis as follows:

$$
\begin{aligned}
\mathrm{V}_{\mathrm{IN}} \text { rising: } \begin{aligned}
& \mathrm{V}_{\mathrm{THR}}=V_{\mathrm{REF}} \times \mathrm{R} 1\left(\left(\frac{1}{\mathrm{R} 1}\right)+\left(\frac{1}{\mathrm{R} 2}\right)+\left(\frac{1}{\mathrm{R} 3}\right)\right) \\
&=3.043 \mathrm{~V} \\
& \mathrm{~V}_{\mathrm{IN}} \text { falling: } \begin{aligned}
\mathrm{V}_{\mathrm{THF}} & =\mathrm{V}_{\mathrm{REF}} \times \mathrm{R} 1\left(\left(\frac{1}{\mathrm{R} 1}\right)+\left(\frac{1}{\mathrm{R} 2}\right)+\left(\frac{1}{\mathrm{R} 3}\right)\right) \\
& -\frac{\mathrm{R} 1}{\mathrm{R} 3+\mathrm{R} 4} \times \mathrm{V}_{\mathrm{CC}}=2.993 \mathrm{~V}
\end{aligned} \\
& \text { Hysteresis }=\mathrm{V}_{\text {THR }}-\mathrm{V}_{\mathrm{THF}}=50 \mathrm{mV} .
\end{aligned} .
\end{aligned}
$$



Figure 3. MAX9016/MAX9018/MAX9020 Additional Hysteresis

## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference

## Board Layout and Bypassing

The MAX9015-MAX9020 ultra-low supply current typically requires no power-supply bypass capacitors. However, when the supply has high output impedance, long lead lengths or excessive noise, or fast transients, bypass VCC to VEE with a $0.1 \mu \mathrm{~F}$ capacitor placed as close to the VCc pin as possible. Minimize signal trace lengths to reduce stray capacitance. Use a ground plane and surface-mount components for best performance. If REF is decoupled, use a low-leakage ceramic capacitor.

Window Detector
The MAX9018 is ideal for window detectors (undervoltage/overvoltage detectors). Figure 4 shows a window detector circuit for a single-cell Li+ battery with a 2.9 V end-of-life charge, a peak charge of 4.2 V , and a nominal value of 3.6 V . Choose different thresholds by changing the values of R1, R2, and R3. OUTA provides an active-low undervoltage indication, and OUTB provides an active-low overvoltage indication. ANDing the two open-drain outputs provides an active-high, powergood signal.

## The design procedure is as follows:

1) Select R1. The input bias current into INB- is normally less than 2nA, so the current through R1 should exceed 100 nA for the thresholds to be accurate. In this example, choose $\mathrm{R} 1=1.24 \mathrm{M} \Omega$ ( $1.24 \mathrm{~V} / 1 \mu \mathrm{~A}$ ).
2) Calculate R2 + R3. The overvoltage threshold should be 4.2 V when VIN is rising. The design equation is as follows:

$$
\begin{aligned}
R 2+R 3 & =R 1 \times\left[\left(\frac{V_{\mathrm{OTH}}}{V_{\mathrm{REF}}+V_{H B}}\right)-1\right] \\
& =1.24 \mathrm{M} \Omega \times\left[\left(\frac{4.2 \mathrm{~V}}{1.24 \mathrm{~V}+0.004}\right)-1\right] \\
& =2.95 \mathrm{M} \Omega
\end{aligned}
$$

3) Calculate R2. The undervoltage threshold should be 2.9 V when $\mathrm{V}_{\mathbb{I}}$ is falling. The design equation is as follows:

$$
\begin{aligned}
R 2 & =(R 1+R 2+R 3) \times\left(\frac{V_{\text {REF }}-V_{H B}}{V_{U T H}}\right)-R 1 \\
& =(1.24 \mathrm{M} \Omega+2.95 \mathrm{M} \Omega) \times \frac{(1.236)}{2.9}-1.24 \mathrm{M} \Omega \\
& =546 \mathrm{k} \Omega
\end{aligned}
$$



Figure 4. Window Detector Circuit
For this example, choose a $499 \mathrm{k} \Omega$ standard value $1 \%$ resistor.
4) Calculate R3:

$$
\begin{aligned}
R 3 & =(R 2+R 3)-R 2 \\
& =2.95 \mathrm{M} \Omega-546 \mathrm{k} \Omega \\
& =240 \mathrm{M} \Omega
\end{aligned}
$$

5) Verify the resistor values. The equations are as follows, evaluated for the above example:
Overvoltage threshold:
$V_{\text {OTH }}=\left(V_{\text {REF }}+V_{H B}\right) \times \frac{(R 1+R 2+R 3)}{R 1}=4.20 \mathrm{~V}$
Undervoltage threshold:
$V_{U T H}=\left(V_{R E F}-V_{H B}\right) \times \frac{(R 1+R 2+R 3)}{(R 1+R 2)}=2.97 V$
where the internal hysteresis band, $\mathrm{V}_{\mathrm{HB}}$, is 4 mV .

## Zero-Crossing Detector

Figure 5 shows a zero-crossing detector application. The MAX9015/MAX9016/MAX9019/MAX9020s' inverting input is connected to ground, and its noninverting input is connected to a 100 mV P-P signal source. As the signal at the noninverting input crosses zero, the comparator's output changes state.

## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference



Figure 5. Zero-Crossing Detector

## Logic-Level Translator

The open-drain comparators can be used to convert 5V logic to 3V logic levels. The MAX9020 can be powered by the 5 V supply voltage, and the pullup resistor for the MAX9020's open-drain output is connected to the 3 V supply voltage. This configuration allows the full 5 V logic swing without creating overvoltage on the 3V logic inputs. For 3 V to 5 V logic-level translations, connect the 3 V supply voltage to $\mathrm{V} C \mathrm{C}$ and the 5 V supply voltage to the pullup resistor.

Chip Information
TRANSISTOR COUNT: 349
PROCESS: BiCMOS
__Ordering Information (continued)

| PART | TEMP RANGE | PIN- <br> PACKAGE | TOP <br> MARK |
| :--- | :--- | :--- | :---: |
| MAX9018AEKA-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIR |
| MAX9018BEKA-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIT |
| MAX9019EKA-T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIU |
| MAX9020EKA- T | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | 8 SOT23-8 | AEIV |

Typical Application Circuit


Pin Configurations

TOP VIEW


## SOT23, Dual, Precision, 1.8V, Nanopower Comparators With/Without Reference

Package Information
(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to www.maxim-ic.com/packages.
 implied. Maxim reserves the right to change the circuitry and specifications without notice at any time.
$\qquad$

